

Sunfield Developments Limited

ADDENDUM GEOTECHNICAL ASSESSMENT REPORT

Sunfield Landholding, Ardmore

Project Reference: J01627 October 10, 2025

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This report constitutes an addendum to a previous Geotechnical Assessment Report carried out by LDE Limited for and in accordance with instructions received from Sunfield Developments Limited with regard to a consent application for the Sunfield Landholding, Ardmore.

If you have any queries or you require any further clarification on any aspects of this report, please do not hesitate to contact the engineers listed above.



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PROJECT BRIEF AND SCOPE

This addendum report has been prepared for Sunfield Developments Limited to accompany a substantive application under the Fast Tract Approvals Act 2024. It should be read in conjunction with our previous Geotechnical Assessment Report (GAR; ref. J01627, dated 6 December 2024) prepared for this development (refer Section 2.1 below).

Our 2024 GAR outlined the site description, development proposal, our investigation findings, and our initial analysis results and recommendations. Based on the appended client supplied drawings (Appendix A), it is apparent that the proposed earthworks scheme has changed from the time of the 2024 GAR. We have also been provided with additional testing data undertaken by Initia (refer Section 2.2 below).

This report represents our analysis results and recommendations updated to incorporate these earthworks scheme changes and additional testing data.

PROJECT DATA

2.1 Related Reports

In preparing this report we have reviewed the following existing geotechnical report prepared by this consultancy:

LDE Limited. Geotechnical Assessment Report (GAR) for Sunfield Landholding Ardmore, Reference J01627, Revision 0, Dated 6 December 2024.

This addendum report should be read in conjunction with our 2024 report. All recommendations of our 2024 report remain applicable unless specifically superseded in this addendum report.

We have also reviewed the following existing memorandum prepared by this consultancy:

LDE Limited, Trial Preload Design and Settlement Monitoring for Sunfield Landholding Phase 1 Ardmore, Reference J01627, Dated 7 July 2025.

That memorandum detailed trial preload design and settlement monitoring protocols for this development.

Further, we have reviewed the following groundwater dewatering report completed by Earthtech Consulting Limited:

Earthtech Consulting Limited, Groundwater Dewatering and Ground Settlement Effects Assessment Report, Reference R10015-1, Revision B, Dated 13 June 2024.



2.2 Additional Test Data

In addition to the test data included in our 2024 report (refer Section 2.1 above), we have been provided with data from 45 Cone Penetrometer Tests (CPTs) undertaken by Initia. These tests are attached (refer Appendix F), and comprise the 100, 200 and 300 series shown on Figure 1.1 (Appendix B). We have incorporated this test data into our analyses below.

GEOTECHNICAL HAZARD ASSESSMENTS

3.1 Risk Register

In accordance with section 2.4 of Auckland Council Code of Practice (ACCoP), we have undertaken a qualitative sitespecific geohazards risk assessment for the proposed development. The risks we have assessed include the geohazards outlined in section 2.5 of ACCoP as well as any additional geotechnical hazards for the site that we have identified as being relevant using Table 1: risk classification

		Consequence					
		Insignificant 1	Minor 2	Moderate 3	Major 4	Extreme 5	
D	Almost Certain 5	Medium 5	High 10	Very high 15	Extremely high 20	Extremely hig 25	
	Likely 4	Low 4	Medium 8	High 12	Very high 16	Extremely hig 20	
Likelihood	Moderate 3	Low 3	Medium 6	Medium 9	High 12	Very high 15	
Ęķ	Unlikely 2	Very low 2	Low 4	Medium 6	Medium 8	High 10	
	Rare 1	Very low	Very low	Low 3	Low 4	Medium 5	

table (as per insert right) and also their guidance on how to assess both likelihood (Table 2: likelihood classification) and consequence (Table 3: consequence classification) scores.

Table 1 presents the assessed risk register for the proposed development. In summary, it is considered that a residual risk level (i.e., following implementation of the proposed engineering mitigation measures or design solutions) of very low to low can be achieved which is deemed an acceptable risk level for the end owner as per ACCoP's guidance. We also confirm that the proposed development therefore also fulfils Section 106 of the Resource Management Act. Regional hazards are beyond the scope of this report.

Table 1. Risk Register (risk rating score in accordance with Section 2.4.3 of ACCoP)

Seismic Hazards	Untreated Risk	Residual Risk	Risk Owner				
Seismic Hazards	2 (Very Low)	1 (Very Low)	Building Designer				
Potential Susceptibility	otential Susceptibility The site is approximately 10km from the nearest active fault (the Wairoa North Fault).						
Mitigation Measures	Refer to Section 7.8.1 of our 2024 GAR.						
Liquefoction	Untreated Risk	Untreated Risk Residual Risk					
Liquefaction	9 (Medium) 4 (Low) Contractor and Foundation Designer						
Potential Susceptibility We have updated the liquefaction analyses undertaken as part of our 2024 GAR, and liquefaction susceptibility assessed in Section 3.3 below.							
Mitigation Measures	Refer to Section 7.4.7 of our 2024 GAR and Section 3.3 below.						



	Untreated Risk	Residual Risk	Risk Owner					
Compressible Soils	12 (High)	4 (Low)	Contractor and Foundation Designer					
Potential Susceptibility	We have updated the settlement an susceptibility is assessed in Section	alyses undertaken as part of our 202	4 GAR, and consolidation settlement					
Mitigation Measures	Refer to Section 7.3.1 of our 2024 GAR and Section 3.4 below.							
Evnanciva Saila	Untreated Risk	Residual Risk	Risk Owner					
Expansive Soils	12 (High)	4 (Low)	Foundation Designer					
Potential Susceptibility	Laboratory testing found that the so 3604 on account of soil expansivity.	•	the definition of 'Good Ground' in NZS					
Mitigation Measures	Refer to Section 8.2 of our 2024 GA	ıR.						
Sensitive Soils	Untreated Risk	Residual Risk	Risk Owner					
Sensitive Sons	6 (Medium)	3 (Low)	Contractor					
Potential Susceptibility	Zone 1 soils are relatively sensitive	to disturbance, and Zone 2 soils may	also be sensitive to disturbance.					
Mitigation Measures	Refer to Section 8.4 of our 2024 GA	ıR.						
Collansible Soils	Untreated Risk	Residual Risk	Risk Owner					
Collapsible Soils	1 (Very Low)	1 (Very Low)	N/A					
Potential Susceptibility	No evidence of collapsible soils was	s encountered on this site.						
Mitigation Measures	Nil							
Landslide Susceptible	Untreated Risk	Residual Risk	Risk Owner					
Ground	2 (Very Low)	2 (Very Low)	N/A					
Ground Potential Susceptibility	The prevailing topography on site so other than shallow seated movemer our 2024 GAR, the primary area of conveyance channel incised within	slopes at less than 1(v) in 4(h), with nts within localised over steepened gu concern is the proposed 1(v) in 4(h) Zone 1 soils.	no obvious evidence of slope instability illy flanks. As discussed in Section 7.2 of flanks forming the proposed stormwater					
	The prevailing topography on site so other than shallow seated movemer our 2024 GAR, the primary area of conveyance channel incised within the	slopes at less than 1(v) in 4(h), with nts within localised over steepened gu concern is the proposed 1(v) in 4(h) Zone 1 soils.	no obvious evidence of slope instability illy flanks. As discussed in Section 7.2 of flanks forming the proposed stormwater					
Potential Susceptibility Mitigation Measures	The prevailing topography on site so other than shallow seated movemer our 2024 GAR, the primary area of conveyance channel incised within. We have updated the stormwater of slope stability of this channel is asset	slopes at less than 1(v) in 4(h), with nts within localised over steepened gu concern is the proposed 1(v) in 4(h) Zone 1 soils.	N/A no obvious evidence of slope instability ully flanks. As discussed in Section 7.2 of flanks forming the proposed stormwater undertaken as part of our 2024 GAR, and Risk Owner					
Potential Susceptibility	The prevailing topography on site so other than shallow seated movemer our 2024 GAR, the primary area of conveyance channel incised within. We have updated the stormwater of slope stability of this channel is asso.	slopes at less than 1(v) in 4(h), with ats within localised over steepened guardines to the proposed 1(v) in 4(h). Zone 1 soils. Sonveyance channel stability analysis usessed in Section 3.5 below.	no obvious evidence of slope instability illy flanks. As discussed in Section 7.2 of flanks forming the proposed stormwater undertaken as part of our 2024 GAR, and					
Potential Susceptibility Mitigation Measures Stream Instability and	The prevailing topography on site of other than shallow seated movemer our 2024 GAR, the primary area of conveyance channel incised within the We have updated the stormwater of slope stability of this channel is assolited. Untreated Risk 1 (Very Low) There are several artificial watercouproposed stormwater conveyance of	slopes at less than 1(v) in 4(h), with ats within localised over steepened gu concern is the proposed 1(v) in 4(h). Zone 1 soils. Proveyance channel stability analysis usessed in Section 3.5 below. Residual Risk 1 (Very Low) rses present on site, however these achannel) as part of the proposed device ion design stage by the Civil Engire	no obvious evidence of slope instability illy flanks. As discussed in Section 7.2 of flanks forming the proposed stormwater undertaken as part of our 2024 GAR, and					



Coastal Instability and	Untreated Risk	Residual Risk	Risk Owner		
Erosion	1 (Very Low)	1 (Very Low)	N/A		
Potential Susceptibility	The nearest coastline is located app	proximately 2.5km to the west of the s	site.		
Mitigation Measures	Nil				
Geothermal Issues	Untreated Risk	Residual Risk	Risk Owner		
Geothermanissues	1 (Very Low)	1 (Very Low)	N/A		
Potential Susceptibility	There is no evidence of geothermal	activity on this site.			
Mitigation Measures	Nil				
Soil Erosion	Untreated Risk	Residual Risk	Risk Owner		
Son Erosion	4 (Low)	2 (Very Low)	Contractor		
Potential Susceptibility & Mitigation Measures					
Rockfall or Falling	Untreated Risk	Residual Risk	Risk Owner		
Debris	1 (Very Low)	1 (Very Low)	N/A		
Potential Susceptibility	There is no ground elevated steeply above the site.				
Mitigation Measures	Nil				
Uncontrolled Fill	Untreated Risk	Residual Risk	Risk Owner		
Gilcontrolled I III	4 (Low)	2 (Very Low)	Contractor and Geotechnical Engineer		
Potential Susceptibility	An area of uncontrolled fill was encountered during site works in July 2024 (likely associated with an old rubbish pit). The presence of rubbish pits elsewhere should never be discounted in farm environments.				
Mitigation Measures	Refer to Section 8.3 of our 2024 GA	.R.			
Groundwater	Untreated Risk	Residual Risk	Risk Owner		
Drawdown	4 (Low)	4 (Low)	N/A		
Drawdown	+ (LOW)	. (2311)			
Potential Susceptibility	The proposed cuts are up to approx		table was measured at up to 0.2m depth		

3.2 Groundwater Drawdown: AUP Section E7 Assessment

As part of our 2024 report, groundwater measurements were undertaken in machine borehole piezometers across the site over the course of a seasonal year. These groundwater measurements are shown in Table 2 below.



Table 2: Machine Borehole Piezometer Groundwater Measurements

Machine	Proposed Cut Depth at Borehole	Groundwater Measurements (mBEGL)					
Borehole	Location (m)	30.04.21	30.07.21	27.10.21	17.01.22	09.02.23	
MH01	2.0	1.66	1.05	1.61	1.73	-	
MH02	2.0	1.57	0.50	-	0.92	-	
MH04	0.5	3.37	0.60	2.92	3.30	-	
MH05	-	1.46	0.50	0.52	1.00	-	
MH06	6.0	7.17	3.50	4.26	5.68	-	
MH07	-	1.87	0.60	0.56	0.72	-	
MH08	-	3.23	3.45	3.39	3.37	-	
MH09	-	1.55	0.40	0.39	0.91	-	
MH10	-	2.69	1.00	0.97	2.43	-	
MH11	2.0	2.54	0.20	0.32	1.28	-	
MH12	-	1.30	1.20	1.17	1.44	-	
MH13	2.0	1.26	0.60	0.63	1.03	-	
MH14	-	-	-	-	-	1.15	
MH15	-	-	-	-	-	1.16	

The highest groundwater measurements in each piezometer have been conservatively taken as the assumed 'natural' groundwater level for the purposes of our AUP E7 assessment. As such, the maximum expected potential drawdown as a result of the proposed cuts/earthworks is approximately 2.5m (at the location of MH06). This is generally consistent with the Earthtech Consulting Limited groundwater dewatering report (refer Section 2.1).

Table 3 assesses the compliance of the proposed excavations to the AUP E7 groundwater guidelines, rules E.7.6.1.6 and E7.6.2.10:

Table 3: AUP E7 Assessment

	Activity	Applicability to Site			
	(1) The water take must not be geothermal water.	Complies: There is no evidence of geothermal activity at the site.			
E7.6.1.6	(2) The water take must not be more than 10 days (peat), or 30 days (other soils).	Does Not Comply: Groundwater take will be permanent.			
	(3) The water take must only occur during construction.	Does Not Comply: Groundwater take will be permanent.			



	Activity	Applicability to Site		
	(2) Any excavation that extends below natural groundwater level must not exceed 1ha and 6m depth below the natural ground level	Does Not Comply: Excavations in the eastern corner of the site are shown to be more than 1ha and will extend more than 6m below the natural ground level.		
	(3) The natural groundwater level must not be reduced by more than 2m on the boundary of any adjoining site.	Complies: The maximum expected potential drawdown resulting from the proposed excavations is approximately 2.5m.		
E7.6.1.10	4) Any structure, excluding sheet piling remaining in place no more than 30 days, that physically impedes the flow of groundwater must not impede the flow of groundwater over a length of more than 20m or extend more than 2m below the natural groundwater level	Complies: No structure that physically impedes the flow of groundwater is proposed.		
	(5a) The distance to any existing neighbouring structure (excluding timber fences and small structures) from the edge of any excavation extending below natural groundwater level must be at least equal to the depth of the excavation	Complies: The proposed excavations are generally centralized in the site (i.e., excavations extending below natural groundwater level are positioned well away from site boundaries). The point of maximum expected potential drawdown (MH13) is located more than 25m from the nearest site boundary, and the point of maximum proposed cut anywhere on site is located approximately 200m from the nearest site boundary.		

Our assessment has found that a permanent groundwater drawdown of up to 2.5m can be anticipated based on the proposed cuts. The excavation therefore does not comply to rule E7.6.1.6 (2) and (3) or rule E7.6.1.10 (2).

The anticipated potential drawdowns as a result of the proposed cuts/earthworks are up to 1.5m in the Zone 1 'peat' soils (at the location of MH02) and up to 2.5m in the Zone 2 East Coast Bays Formation (ECBF) soils (at the location of MH06). Consolidation settlement as a result of groundwater drawdown based on typical coefficient of compressibility values of $1.2x10^{-3}$ m² kN⁻¹ for the 'peat' soils and $3.0x10^{-5}$ m² kN⁻¹ for the ECBF soils (based on the findings of our 2024 report) is calculated to be less than 30mm, as outlined below.



- Zone 1 'Peat' Soils:
 - Coefficient of compressibility (Mv) = 1.2×10^{-3} m² kN⁻¹ (refer Appendix 3.1 from our 2024 report)
 - Thickness of affected soil (d) = 1.5m
 - Change in stress ($\Delta \sigma$) = unit weight of water x depth of drawdown = 15kNm⁻²
 - Total settlement = Mv x d x $\Delta \sigma$ = <30mm
- Zone 2 ECBF Soils:
 - o Coefficient of compressibility (Mv) = 3.0x10⁻⁵ m² kN⁻¹ (refer Appendix 3.1 from our 2024 report)
 - Thickness of affected soil (d) = 2.5m
 - Change in stress ($\Delta \sigma$) = unit weight of water x depth of drawdown = 25kNm⁻²
 - Total settlement = Mv x d x $\Delta \sigma$ = <5mm

Further to this, all excavations extending below natural groundwater level are positioned well away from site boundaries, with the point of maximum expected potential drawdown located more than 25m from the nearest site boundary. As such, we consider that the anticipated groundwater drawdowns will have a negligible effect on any neighbouring structures. A programme of preloading is also proposed following bulk earthworks, which will allow any settlements induced by groundwater drawdown to attenuate prior to construction of end use structures. Groundwater drawdown should therefore be dismissed as a geotechnical issue and a Consent (if deemed necessary) issued for this proposed development.

No retaining walls are proposed as part of the development (i.e., retaining structures proposed are limited to box culverts, bridge abutments, etc.), and as such mechanical settlement resulting from retaining structures is dismissed as a geotechnical issue. Based on this consideration and the above drawdown assessment, a Groundwater Settlement Monitoring & Contingency Plan (GSMCP) is not considered necessary for the proposed development.

3.3 Liquefaction

3.3.1 Computer Liquefaction Analysis

We have updated the liquefaction assessment undertaken in Section 7.4 of our 2024 GAR to incorporate the additional CPT data provided to us (refer Section 2.2) as well as the latest earthworks plans.

Our liquefaction assessment has been completed using GeoLogismiki CLiq v.3.5.2.5 software and in accordance with the parameters and assumptions used in our previous assessment, with the following exceptions:

- The proposed cuts and fills have been modelled for both SLS (Case 1) and ULS (Case 2) scenarios.
- For the additional CPTs, clay-like cyclic softening was applied where the CPTs / nearby boreholes indicate Undifferentiated Holocene Alluvium (i.e., we have followed the same assumptions used in our previous assessment for the geological zoning of all previously assessed CPTs).

Detailed summary tables and full output results from our computer liquefaction analyses are presented in Appendix D.



No vertical settlements were calculated under SLS seismic conditions for any CPT, with the exception of CPT131 where theoretical vertical settlements of up to 90mm were calculated. Under ULS seismic conditions, theoretical vertical settlements of up to 150mm were calculated, again with the exception of CPT131 where theoretical vertical settlements of up to 430mm were calculated.

However, these vertical settlement values do not take into account non-liquefiable crust thickness overlying the liquefiable layers, nor do they account for the Liquefaction Severity Number (LSN) for each analysis or the geological age and fabric of the soils. The geological age and soil fabric criteria are outlined in Sections 7.4.3 and 7.4.4 of our 2024 GAR (these factors remaining unchanged), and the non-liquefiable crust thickness and LSN criteria are outlined in Sections 3.3.2 and 3.3.3 below. Further, assessed vertical settlements following consideration of these factors are presented in Section 3.3.4 below.

3.3.2 Liquefaction Severity Number

MBIE Module 3 Table 5.1 (inset right) indicates expected performance levels for liquefied deposits based on the Liquefaction Severity Number (LSN). The potential for ground surface damage as a result of the computer liquefaction settlements has therefore been evaluated using LSNs for each CPT assessed.

As shown in Appendix D, the calculated LSN value for SLS ground shaking in CPT131 (the only CPT where liquefaction was calculated under SLS conditions) is 15, indicating insignificant to mild effects

Table 5.1: General performance levels for liquefied deposits

	PORE WATER PRESSURE AND LIQUEFACTION	CHARACTERISTICS OF LIQUEFACTION AND ITS CONSEQUENCES	CHARACTERISTIC
Lo	Insignificant	No significant excess pore water pressures (no liquefaction).	F _L > 1.4 LPI=0 LSN <10
Lı	Mild	Limited excess pore water pressures; negligible deformation of the ground and small settlements.	F _L > 1.2 LPI = 0 LSN = 5 - 15
L2	Moderate	Liquefaction occurs in layers of limited thickness (small proportion of the deposit, say 10 percent or less) and lateral extent; ground deformation results in relatively small differential settlements.	F _L ≈ 1.0 LPI < 5 LSN 10 - 25
L3	High	Liquefaction occurs in significant portion of the deposit (say 30 percent to 50 percent) resulting in transient lateral displacements, moderate-to-large differential movements, and settlement of the ground in the order of 100 mm to 200 mm.	F _L < 1.0 LPI = 5 - 15 LSN = 15 - 35
14	Severe	Complete liquefaction develops in most of the deposit resulting in large lateral displacements of the ground, excessive differential settlements and total settlement of over 200 mm.	F _L << 1.0 LPI > 15 LSN > 30
L5	Very severe	Liquefaction resulting in lateral spreading (flow), large permanent lateral ground displacements and/or significant ground distortion (lateral strains/stretch, vertical offsets and angular distortion).	

Inset 1: MBIE Module 3 Table 5.1

as a result of liquefaction. The LSN values for ULS ground shaking are typically less than 10 with almost all of the remaining values in excess of 10 but still less than 15. This indicates insignificant to mild effects as a result of liquefaction across all but six of the analysed CPTs as per MBIE Module 3 Table 5.1. However, CPT102, 123, 202, and 302 have calculated LSNs between 25 and 35 (moderate to high effects as a result of liquefaction), while CPT131 and CPT206 have calculated LSNs in excess of 35.

The average LSN for the Zone 1 soils for the ULS case is approximately 8.3, while the average LSN for the Zone 2 soils is approximately 7.7. This indicates insignificant to mild liquefaction effects generally prevail under ULS shaking across both of these zones, resulting in limited excess pore water pressures, negligible deformation of the ground and small settlements only.



3.3.3 Surface Manifestation Criteria

MBIE Module 3 provides guidance around consideration of crust thickness. A non-liquefiable crust thickness of 3m is generally deemed thick enough to suppress surface manifestation of deep liquefaction occurrence for earthquakes with a PGA of 0.2g or less.

Research completed by Bowen & Jacka (2013)¹ has compared this theory to the damage recorded during the 2010 and 2011 Canterbury earthquake sequence which also found that where the crust thickness of 3m or more is present (for a PGA of 0.2g), liquefaction was considered unlikely to occur as the crust thickness was considered too thick for the underlying liquefied soils to 'break through', for example in the case of sand boils. The research also suggests that the thickness of the underlying liquefied layer is a less important factor except in instances where a liquefied layer of between 0.5m and 2.0m were present within the upper 3m.

The results of our computer liquefaction analysis have considered the thickness of non-liquefiable crust layers, and these demonstrate that the non-liquefiable crust thickness was between 1.0m and 6.3m under ULS seismic conditions (refer Appendix D). For SLS seismic conditions in CPT131 (the only CPT where liquefaction was calculated under SLS conditions), the non-liquefiable crust was 8.0m thick.

A significant number of CPTs in Zone 1 (18 out of 33) have non-liquefiable crusts less than 3m thick under ULS seismic conditions, while out of the Zone 2 CPTs, only 14 out of 49 have non-liquefiable crusts less than 3m thick. Based on this, the Zone 1 soils could result in more surface manifestation of liquefaction during a ULS earthquake, while the Zone 2 soils are generally not expected to show surface manifestation based on crust thickness criteria.

3.3.4 Assessed Vertical Settlements

Based on the criteria assessed above, the Zone 1 soils are possibly susceptible to liquefaction only under ULS shaking with calculated settlements of up to 430mm, while the Zone 2 soils are considered to be less susceptible to liquefaction. Recommendations around development on liquefaction-prone (Zone 1) soils are provided in Section 7.4.7 of our 2024 report. Our recommendations remain unchanged in this regard.

3.4 Consolidation Settlement

We have updated the consolidation settlement assessment undertaken in Section 7.3 of our 2024 report to incorporate the additional CPT data provided to us (refer Section 2.2) as well as the latest earthworks plans.

Our consolidation assessment has been completed using CPeT-IT v3.9.4.11 software (for the CPT data) and DMT Settlements v1.1.2.0 software (for the DMT data) and in accordance with the parameters and assumptions used in our previous assessment, with the following exceptions:

¹ Bowen, H. & Jacka, M. (2013) "Liquefaction induced ground damage in the Canterbury earthquakes: predictions vs reality" Proc. 19th NZGS Geotechnical Symposium.



- Three cases have been modelled. Case 1 has been modelled with the proposed earthworks loads only, Case 2 has been modelled with the proposed end use loads only, and Case 3 has been modelled with both proposed earthworks loads and end use loads. Case 3 settlement values have been calculated from Case 1 plus Case 2 settlement values except where total earthworks plus end use surcharge yields higher settlement values in the software analyses.
- A nominal 10m x 20m rectangular building footprint has been used for proposed residential end use areas, along with a nominal 180m x 360m footprint for proposed commercial or industrial end use areas. For proposed end use loads, a rigid footing (i.e., stiffened pod-raft) is used.
- The end use loads applied to our analyses have been determined from the delivery standard we
 understand is to be used for the development.

Detailed summary tables and full output results from our computer settlement analyses are presented in Appendix E.

Based on the results of our settlement analyses, total settlement beneath the proposed loads are summarised for Case 1 (earthworks surcharge), Case 2 (end use surcharge) and Case 3 (earthworks plus end use surcharge), respectively, as follows:

Zone 1:

- Up to 345mm, 180mm and 460mm (using the DMT data).
- Up to 920mm, 230mm and 1,010mm (using the CPT data)

Zone 2:

- Up to 0mm, 85mm and 85mm (using the DMT data).
- Up to 240mm, 690mm and 690mm (using the CPT data).

It should be noted that there is a reasonable disparity between CPT and DMT settlement estimations. DMT methods are widely regarded as a more accurate in-situ test for estimating settlements due to the direct measurement of the soil constraint modulus (M). Notwithstanding, trial preloading (as discussed in Section 7.3.1 of our 2024 report and in our trial preload design memorandum referenced in Section 2.1 above) will help assess actual response of the ground to surcharge application, as opposed to reliance on widely varying theoretical estimations.

Our settlement analyses do not encompass the proposed recreational areas, as we understand they are proposed to comprise generally permeable areas with low loadings (e.g. playgrounds). For these recreational areas, consolidation and groundwater drawdown settlements are considered unlikely to present geotechnical risk, however the subdivision design should allow for groundwater recharge as is usual in peat soils, further limiting any risk.



3.5 Slope Stability

We have updated the slope stability assessment undertaken in Section 7.2 of our 2024 report, which assesses the stability of the 1(v) in 4(h) and approximately 3.5m high (measured vertically) flanks of the proposed stormwater conveyance channel. Our slope stability assessment has been completed using Slide2 and in accordance with the parameters and assumptions used in our previous assessment, with the following exceptions:

• For the seismic scenario, a factor of safety (FoS) of 1.0 and ULS seismic load of 0.19g was used as specified in the NZGS Earthquake Geotechnical Engineering Practice Module 1, 2022.

Full output results from our computer settlement analyses are presented in Appendix C.

The existing groundwater and elevated groundwater scenarios both returned satisfactory FoS in our analyses. However, the ULS seismic FoS was not achieved, and a Newmark analysis was performed to estimate the permanent slope displacement. Estimated displacements for existing conditions using the displacement-based Jibson (2007) method estimates that limited (50th percentile permanent) lateral displacement of up to 3mm could occur at this site. Therefore, lateral displacement from the analysed earthquake event is considered insignificant.

Nevertheless, as discussed in our 2024 report, the proposed channels are subject to detailed design and it is recommended that further geotechnical assessments are completed once the final channel locations and geometries have been confirmed.

4 LIMITATIONS

This addendum report should be read and reproduced in its entirety including the limitations to understand the context of the opinions and recommendations given.

This report has been prepared exclusively for Sunfield Developments Limited in relation to the specific project described herein, in accordance with the brief given to us or the agreed scope. Sunfield Developments Limited will be deemed the exclusive owner on full and final payment of the invoice.

Information, opinions, and recommendations contained within this report can only be used for the purposes with which it was intended. LDE accepts no liability or responsibility whatsoever for any use or reliance on the report by any party other than the owner or parties working for or on behalf of the owner, such as local authorities, and for purposes beyond those for which it was intended. All future owners of this property should seek professional geotechnical advice to satisfy themselves as to its ongoing suitability for their intended use.

This report was prepared in general accordance with current standards, codes and best practice at the time of this report. These may be subject to change.

Factual evidence, opinions, recommendations and comments given in this report result from the application of normal methods of site investigation and are based on visual methods and subsurface investigations at discrete



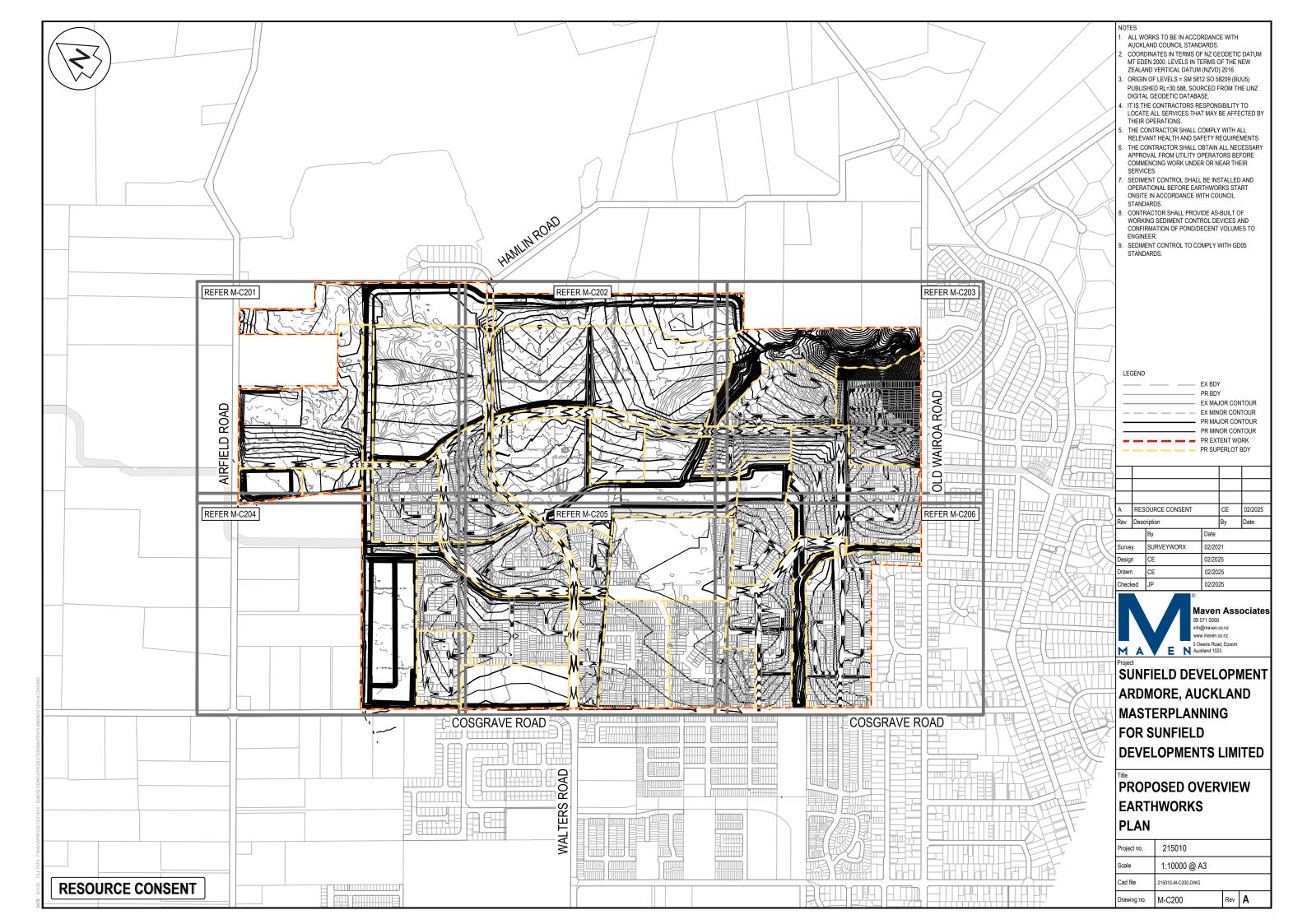
locations and are designed to the constraints of the project scope to provide the best assessment of the environment. By their nature these methods only provide information about a relatively small volume of subsoils and it must be appreciated that the nature and continuity of the subsurface materials between these locations are inferred and that actual conditions could vary from that described herein. There may therefore be special conditions pertaining to this site which have not been disclosed by the investigation and which have not been taken into account in the report.

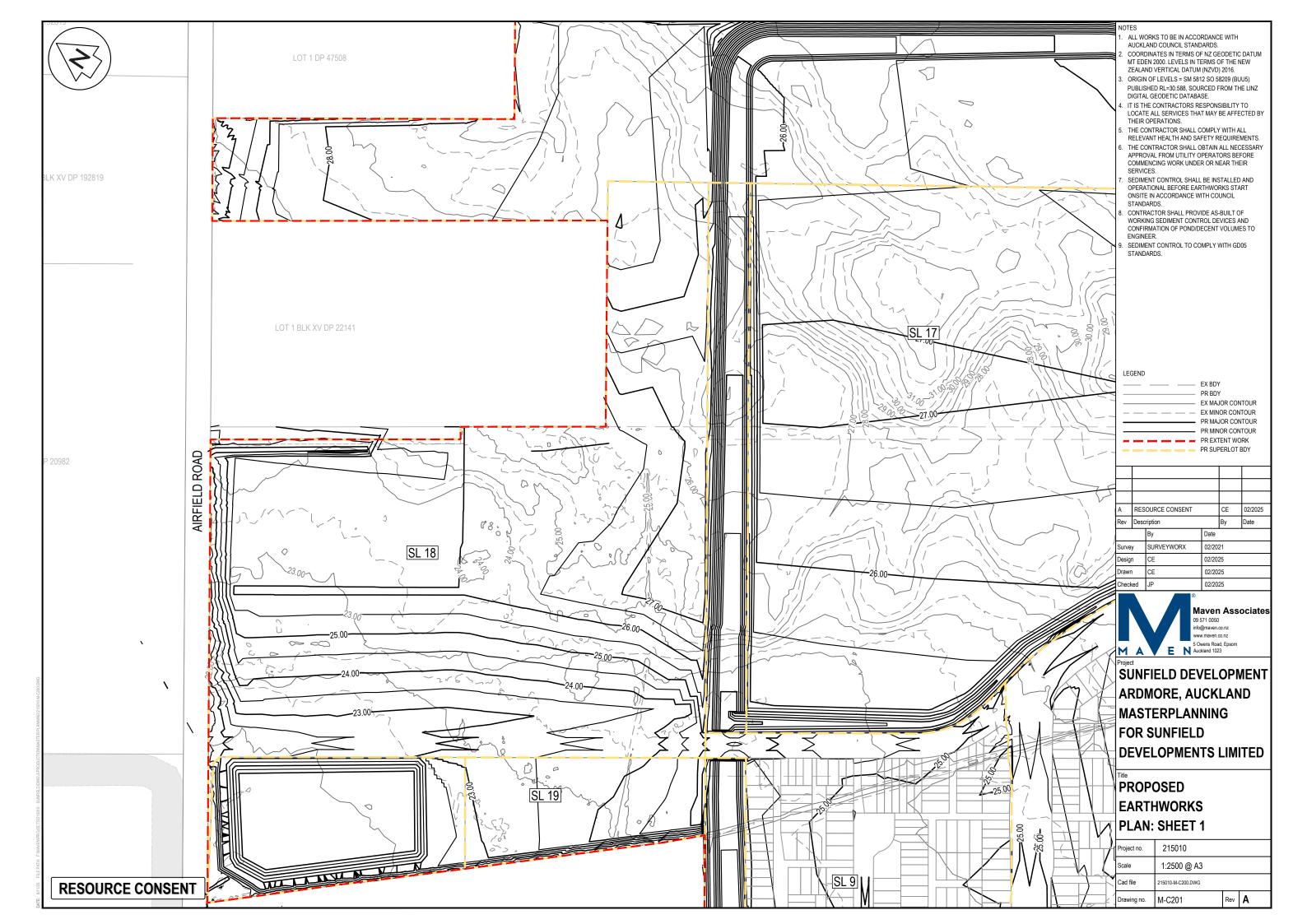
We should be contacted immediately if the conditions are found to differ from those described or assumed to exist in this report.



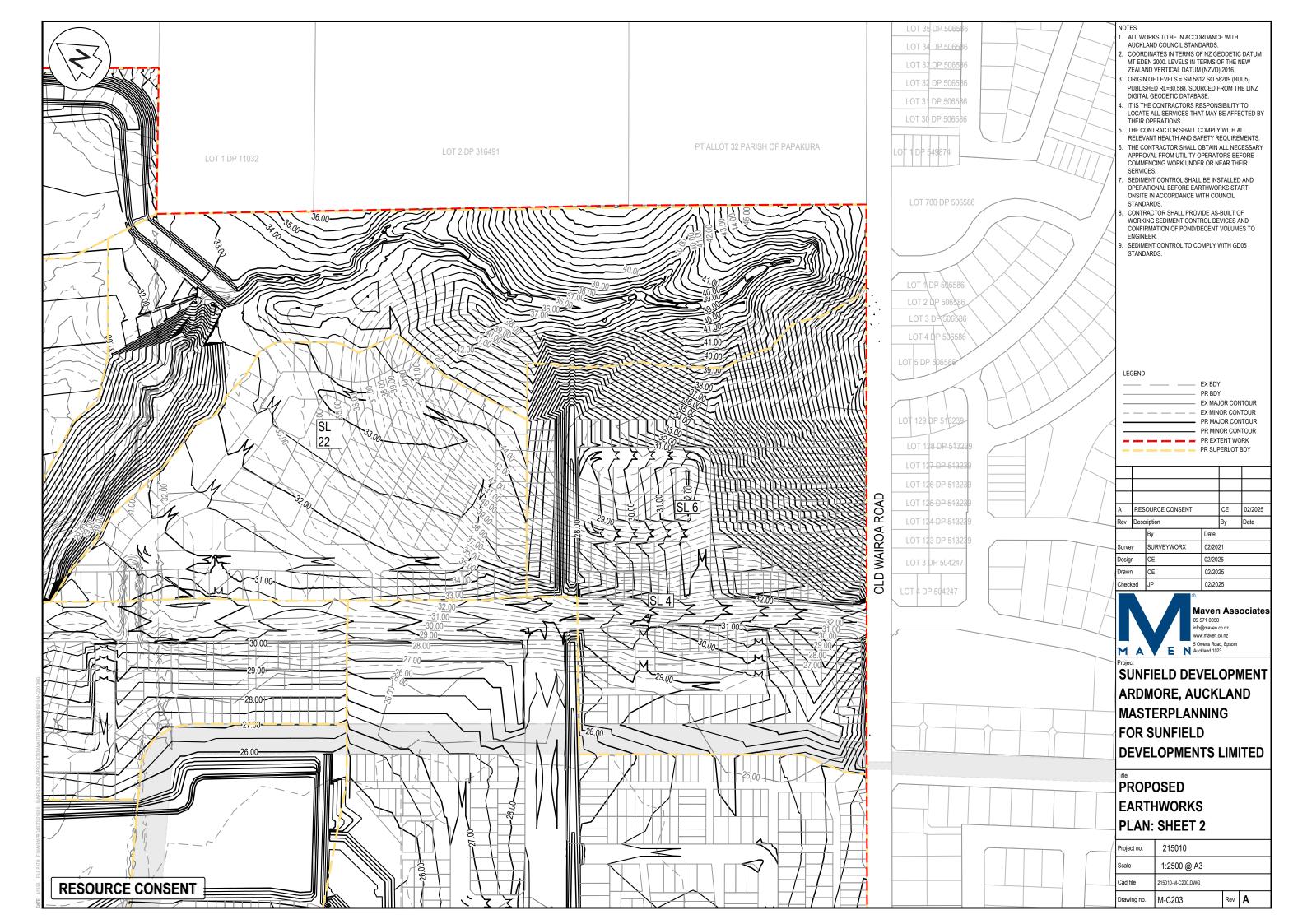
APPENDIX A CLIENT SUPPLIED DRAWINGS

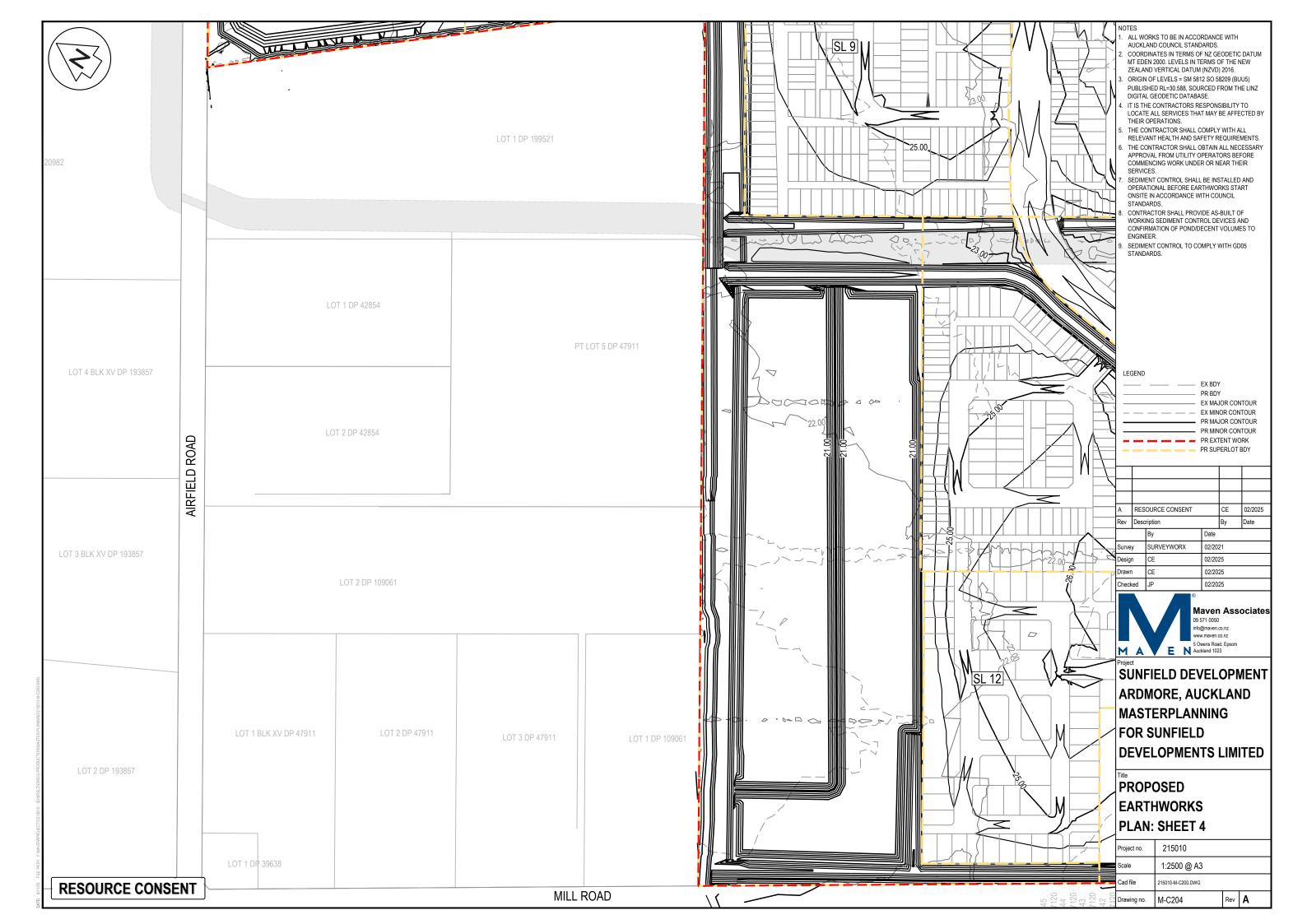


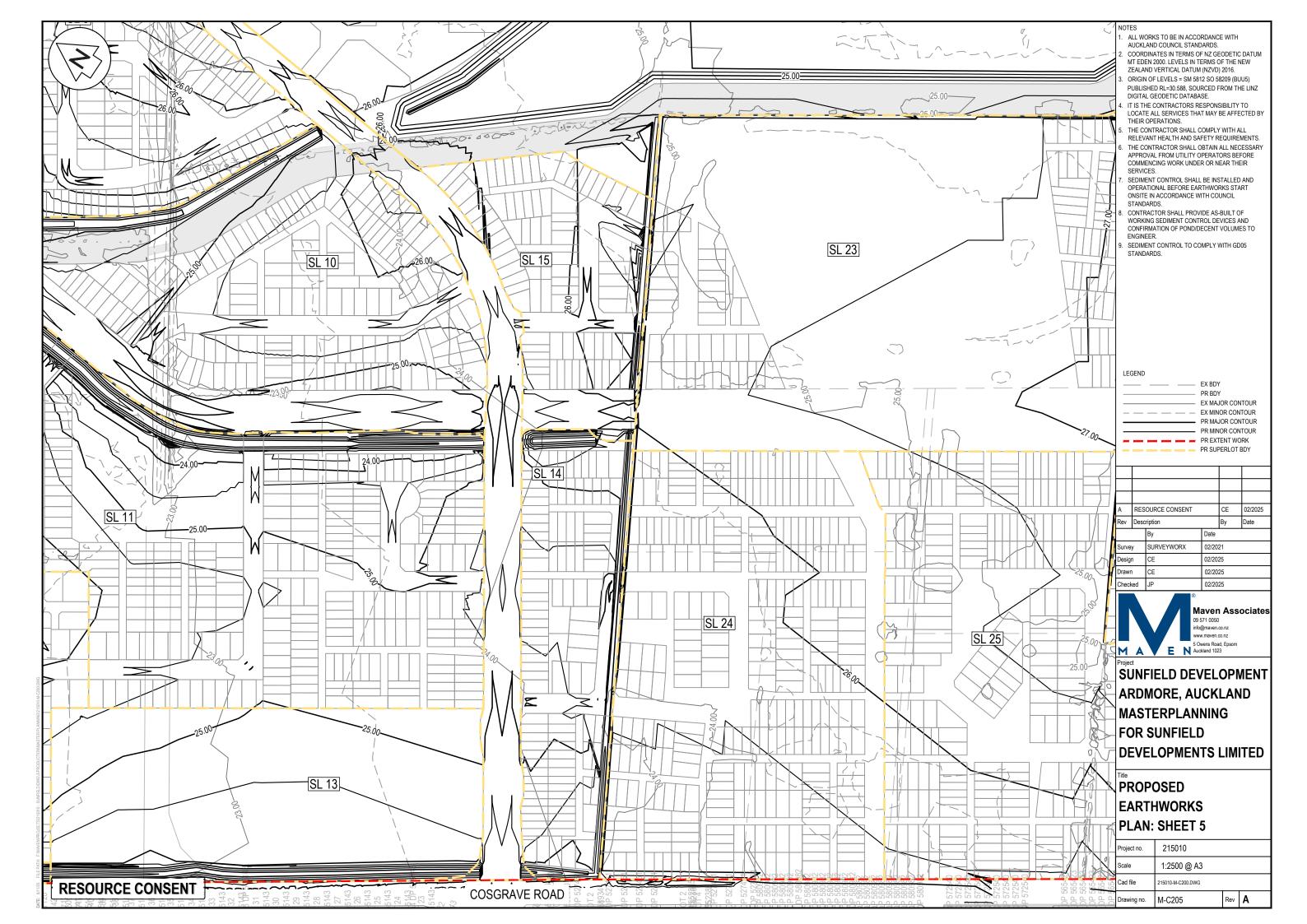


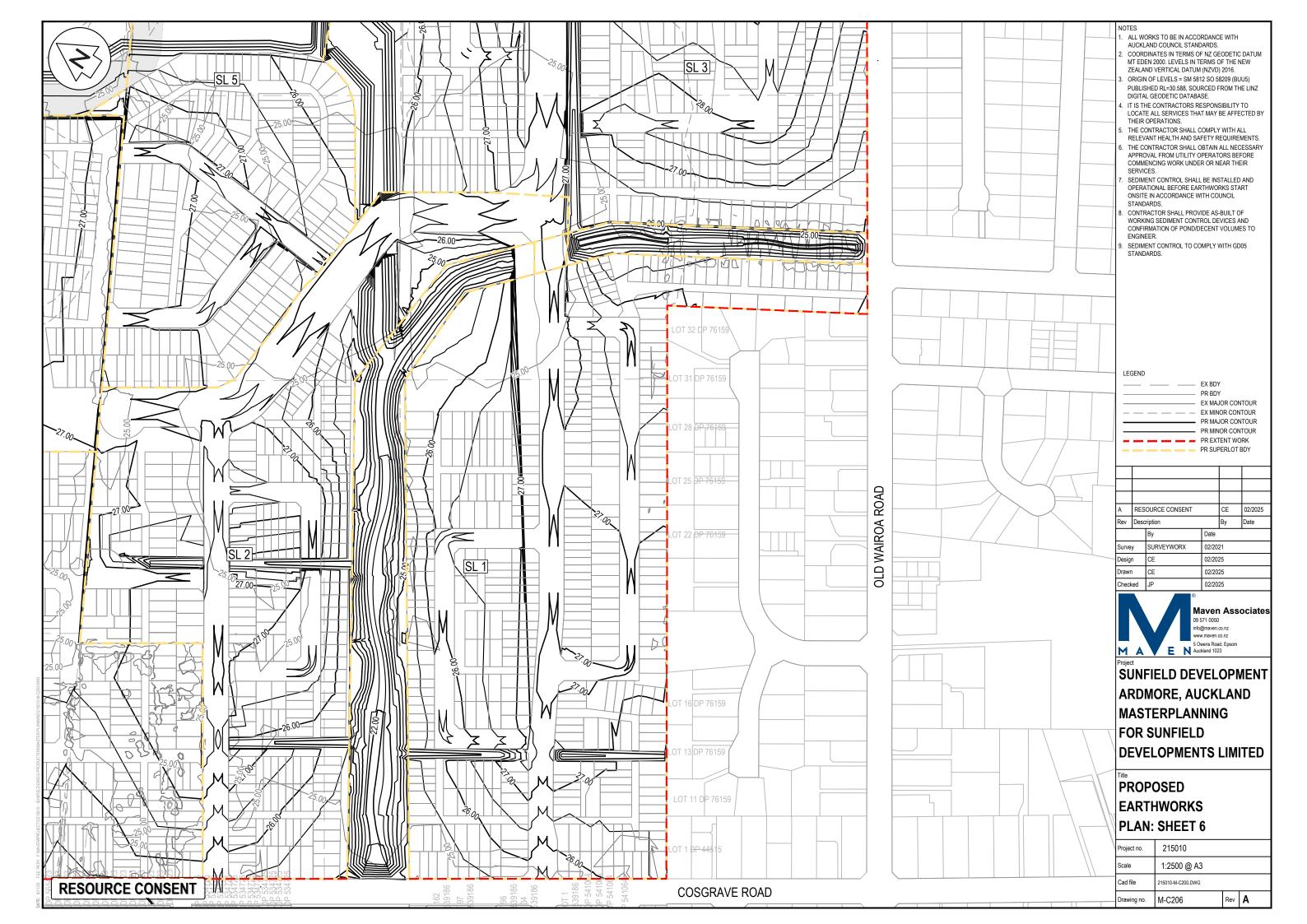




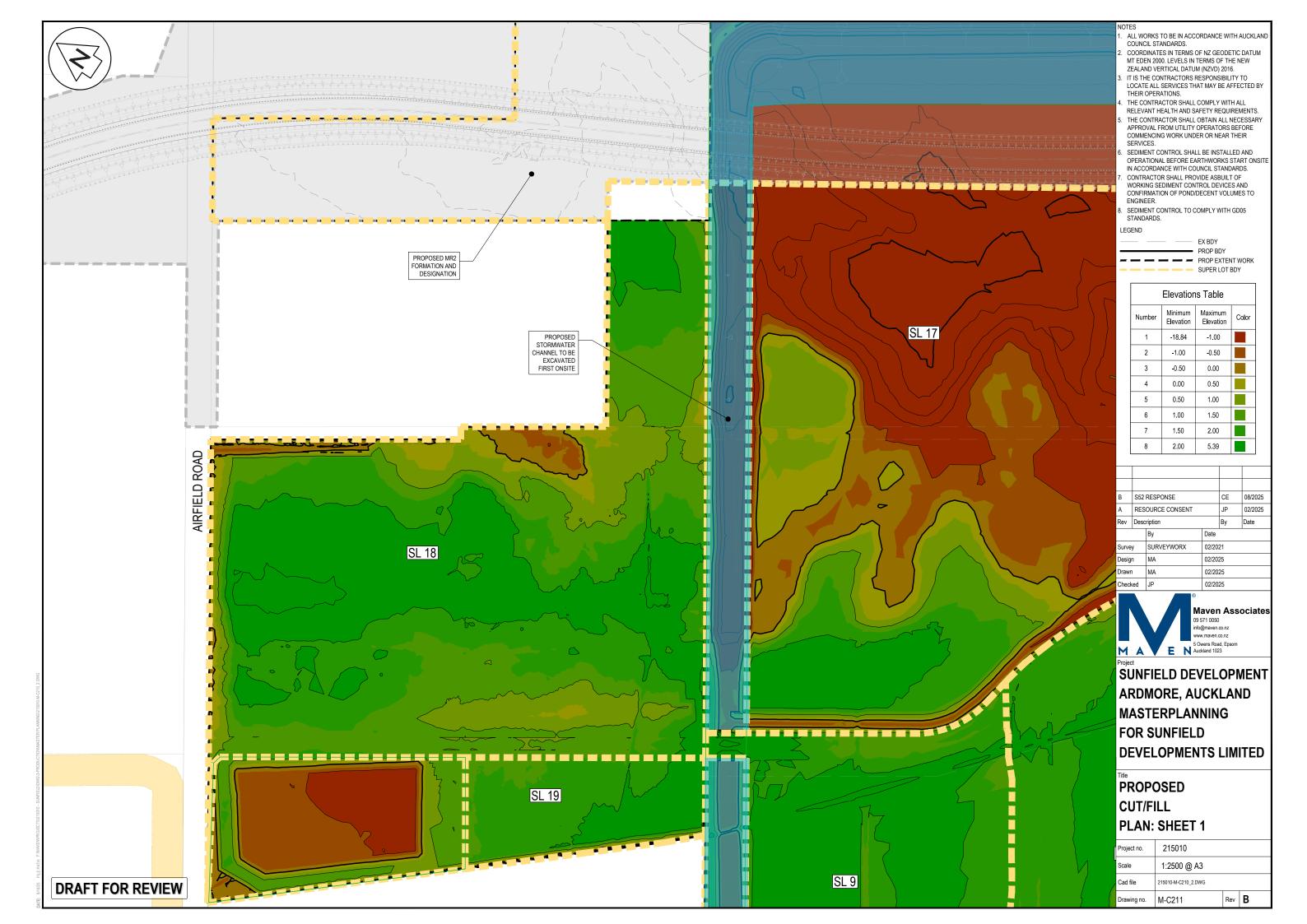


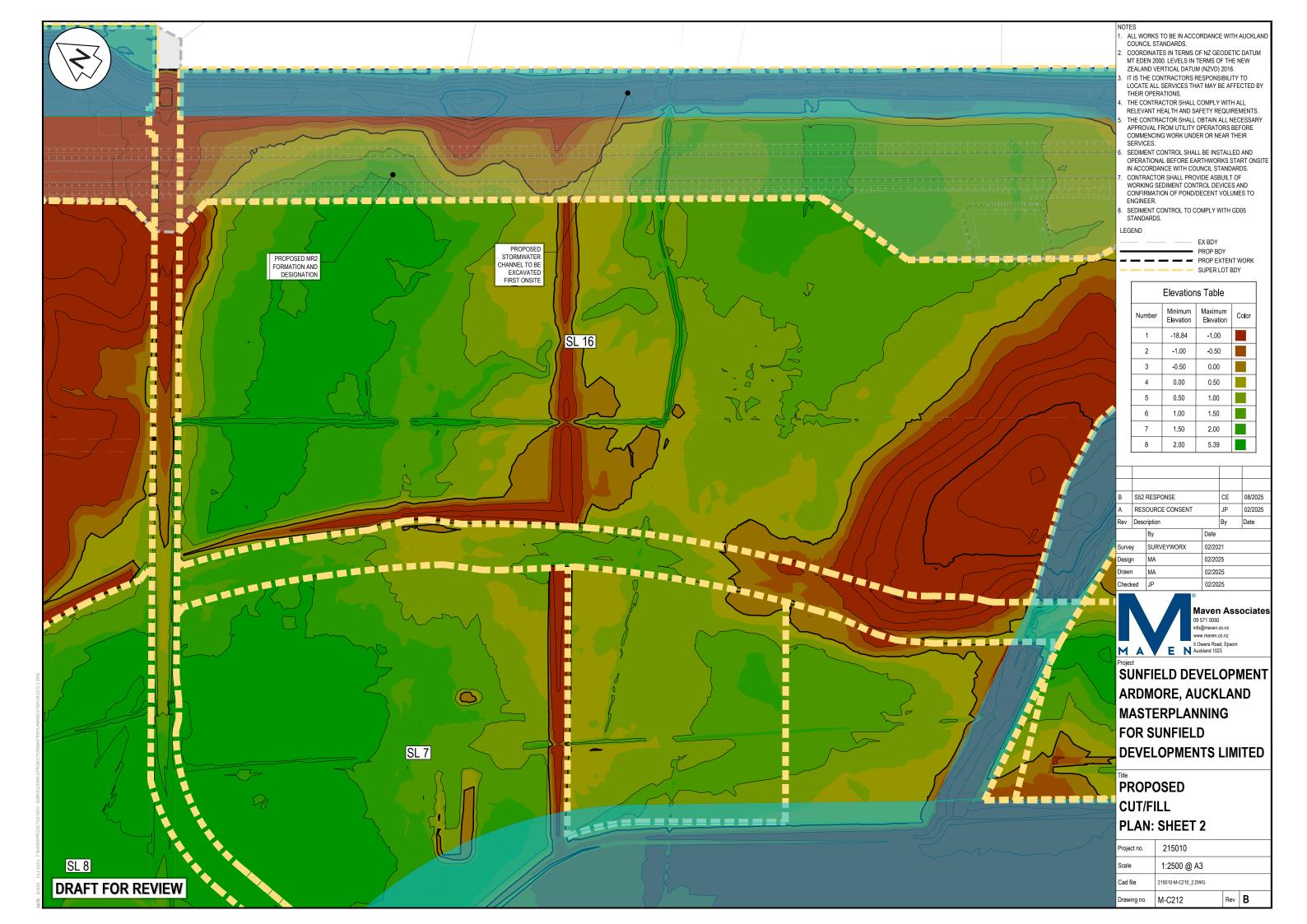


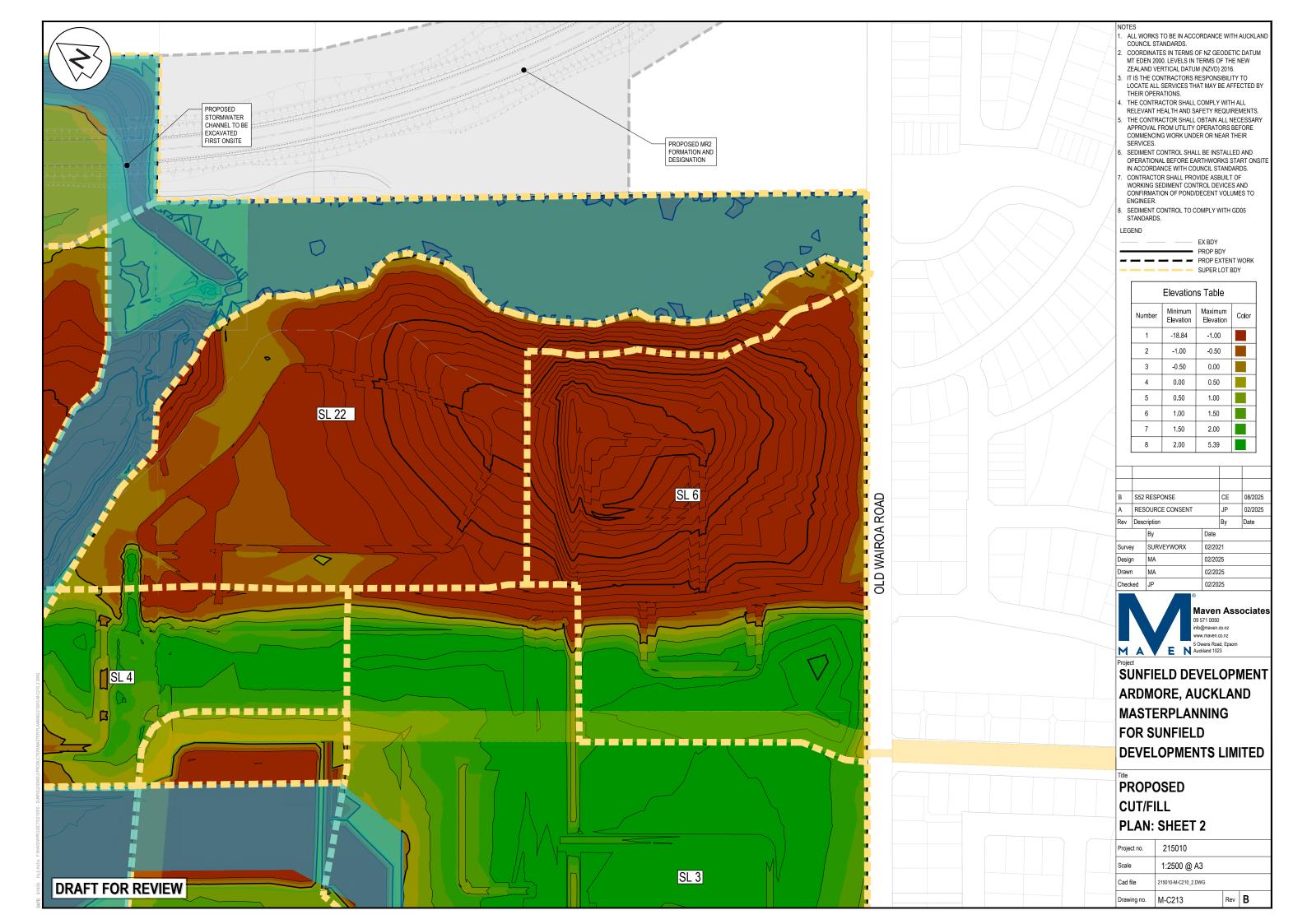


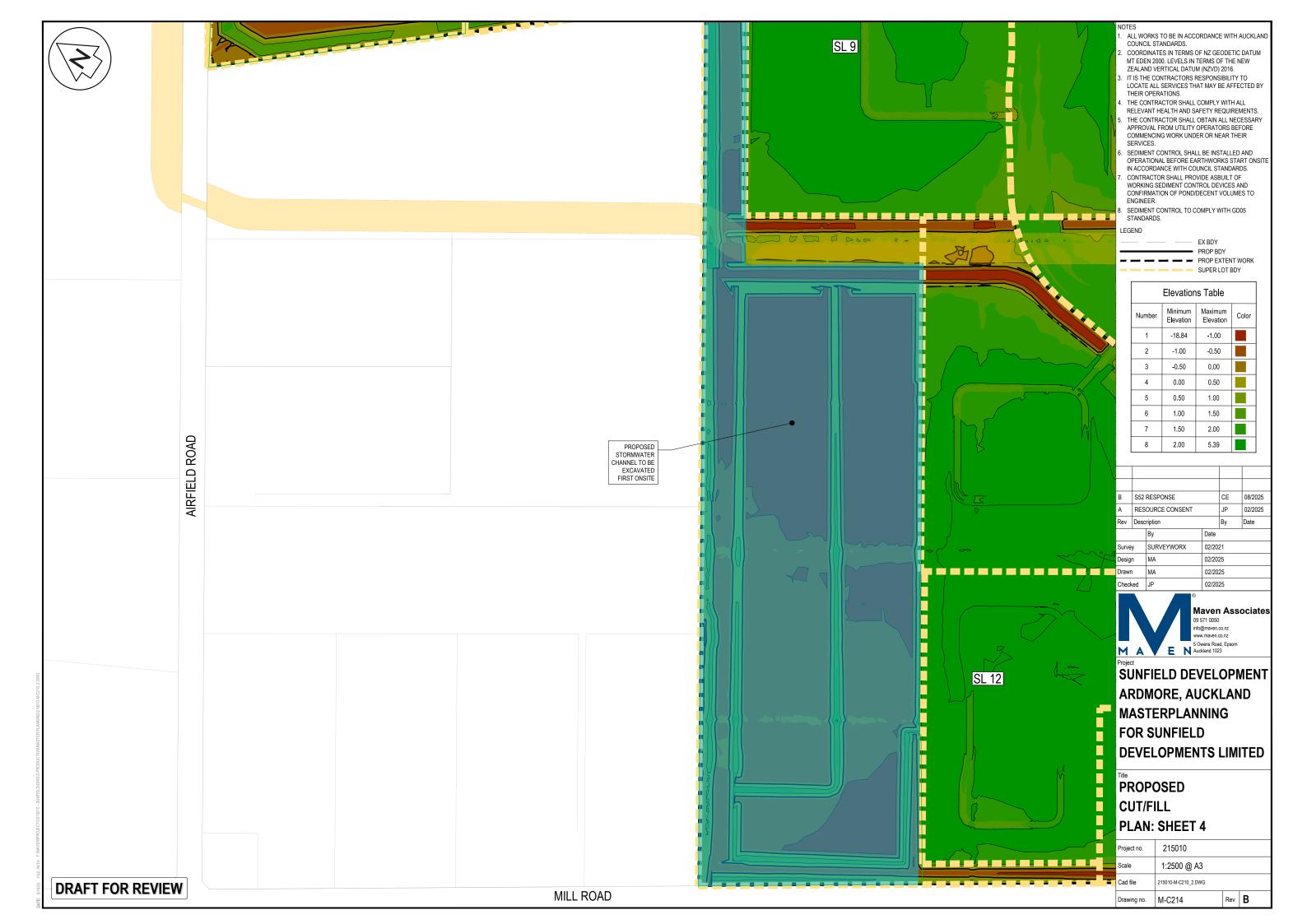






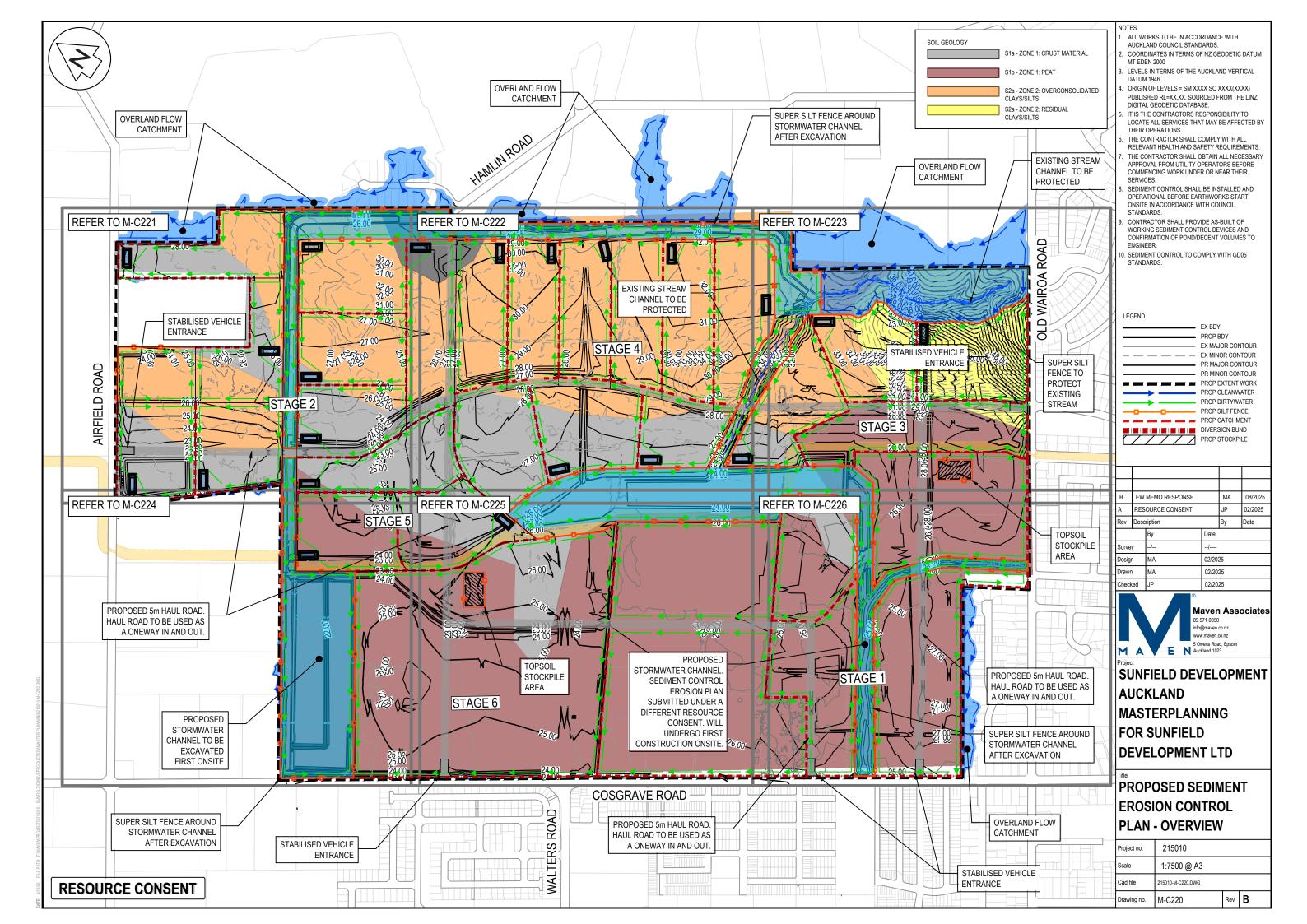


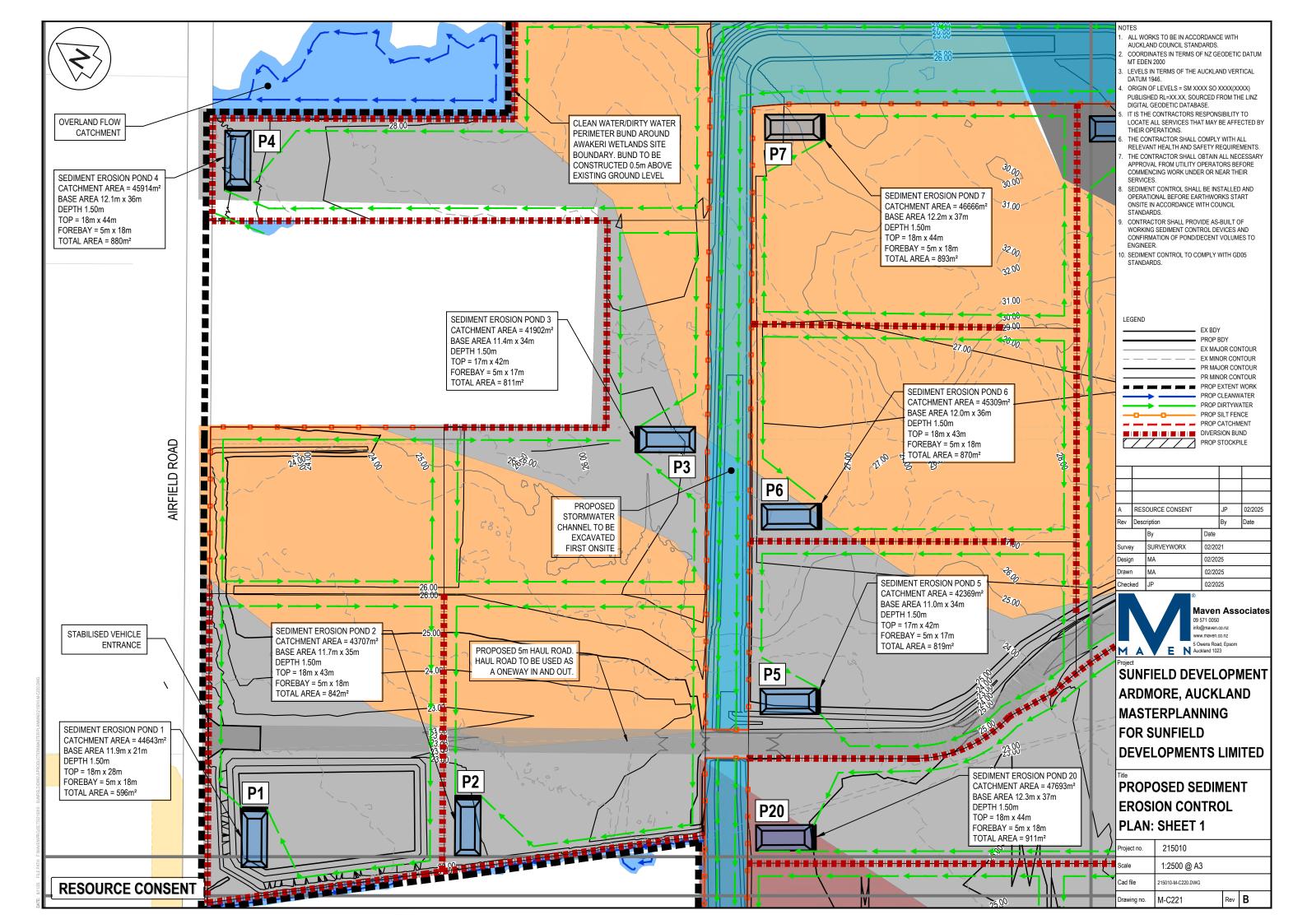


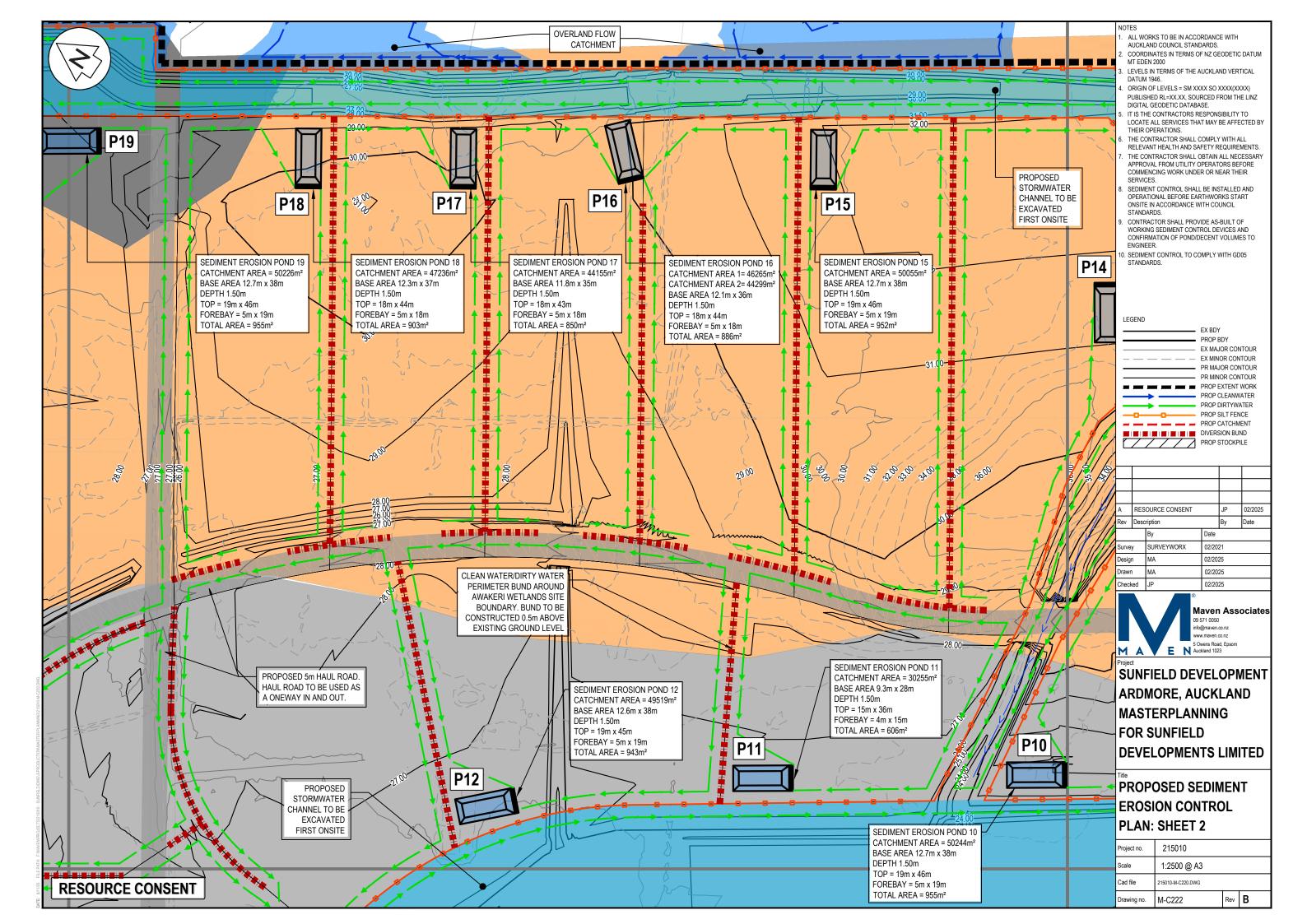


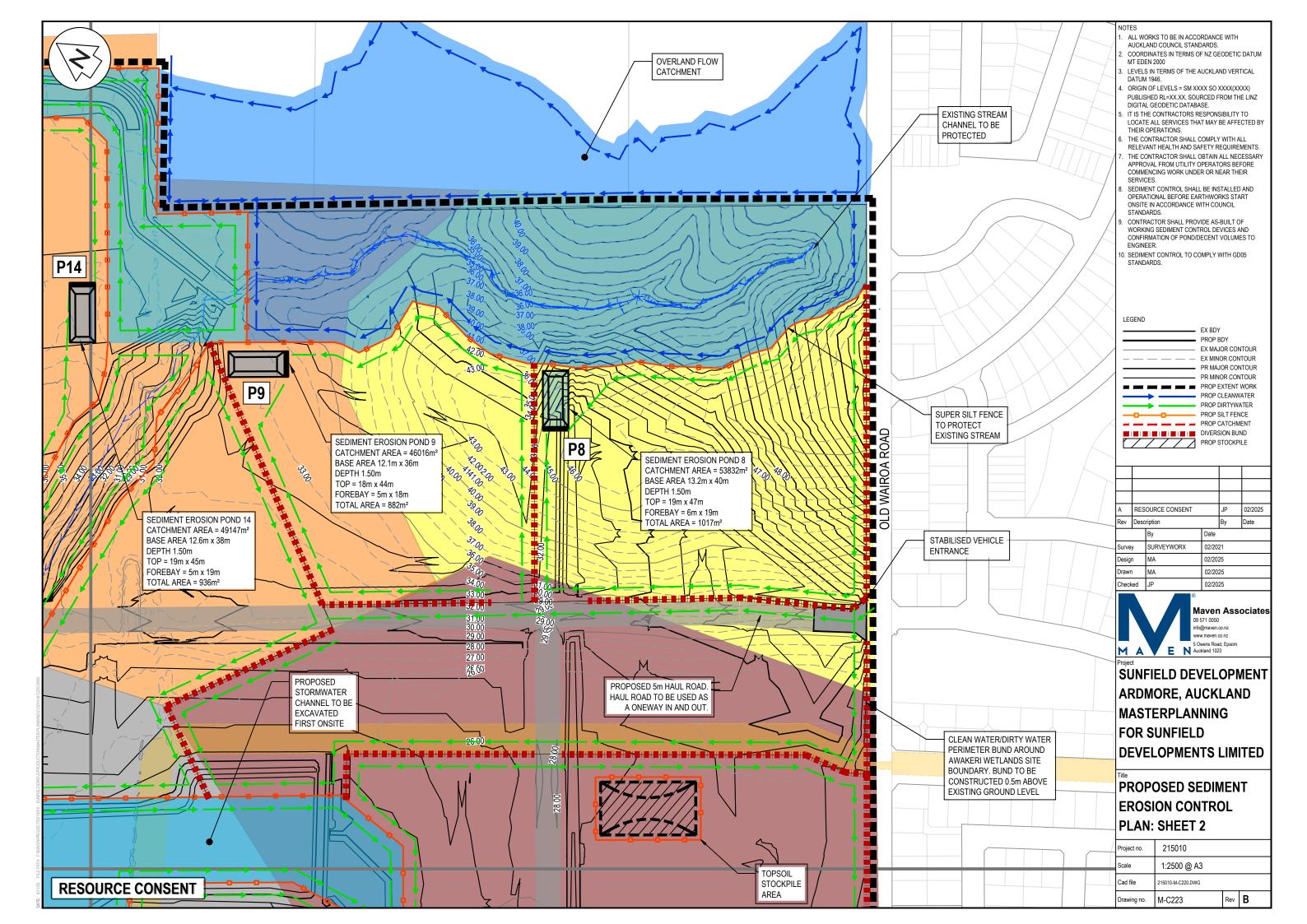


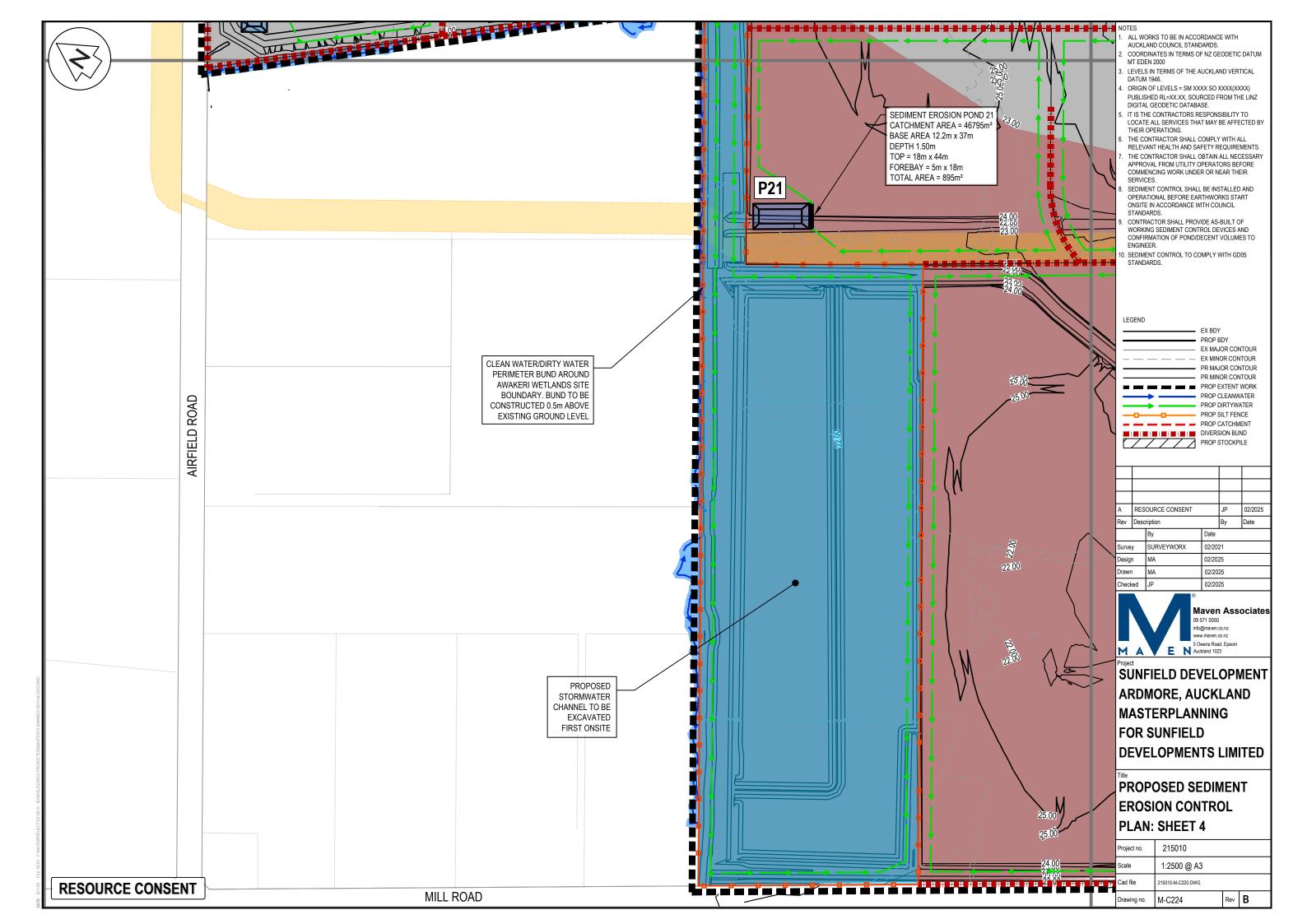


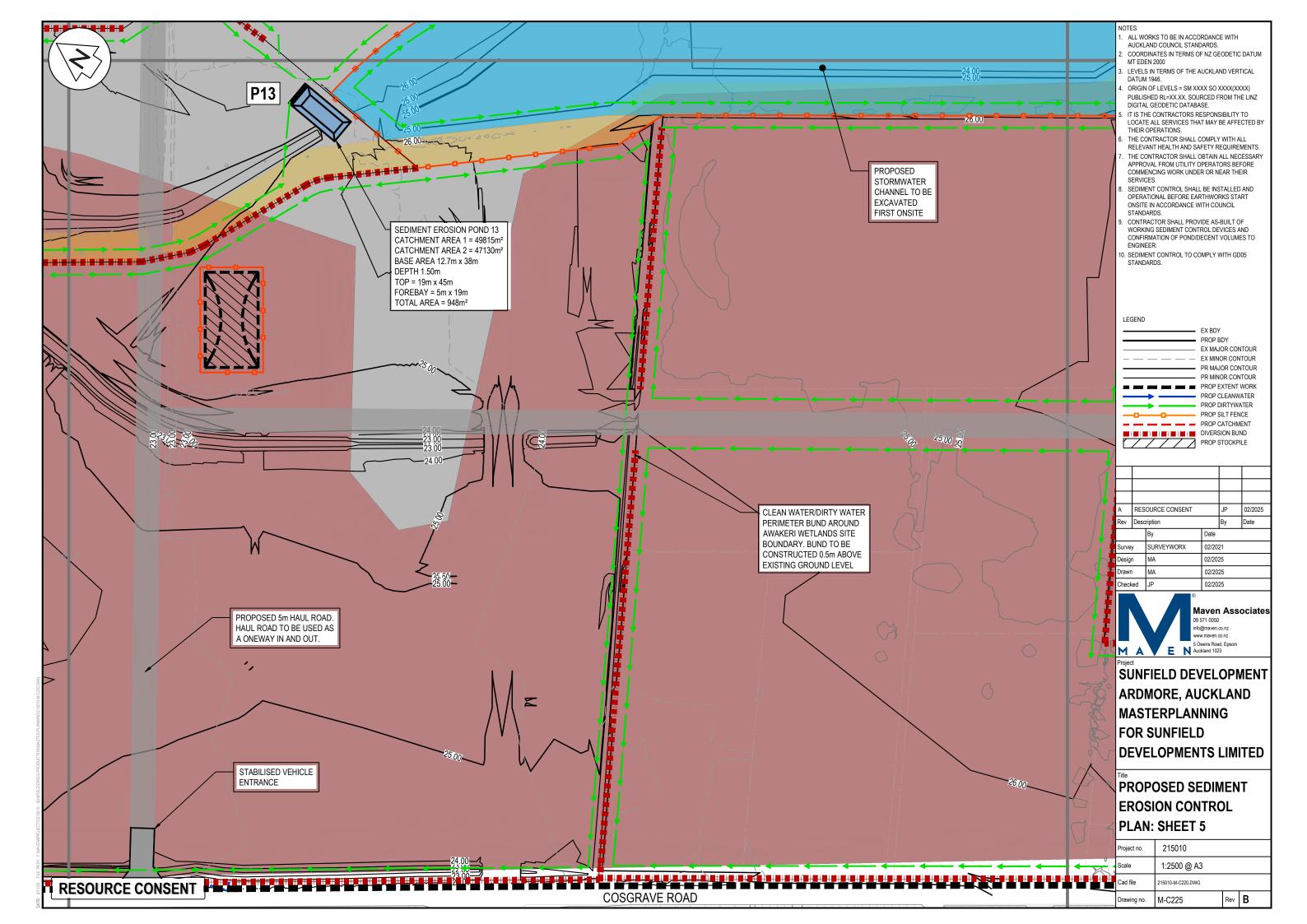


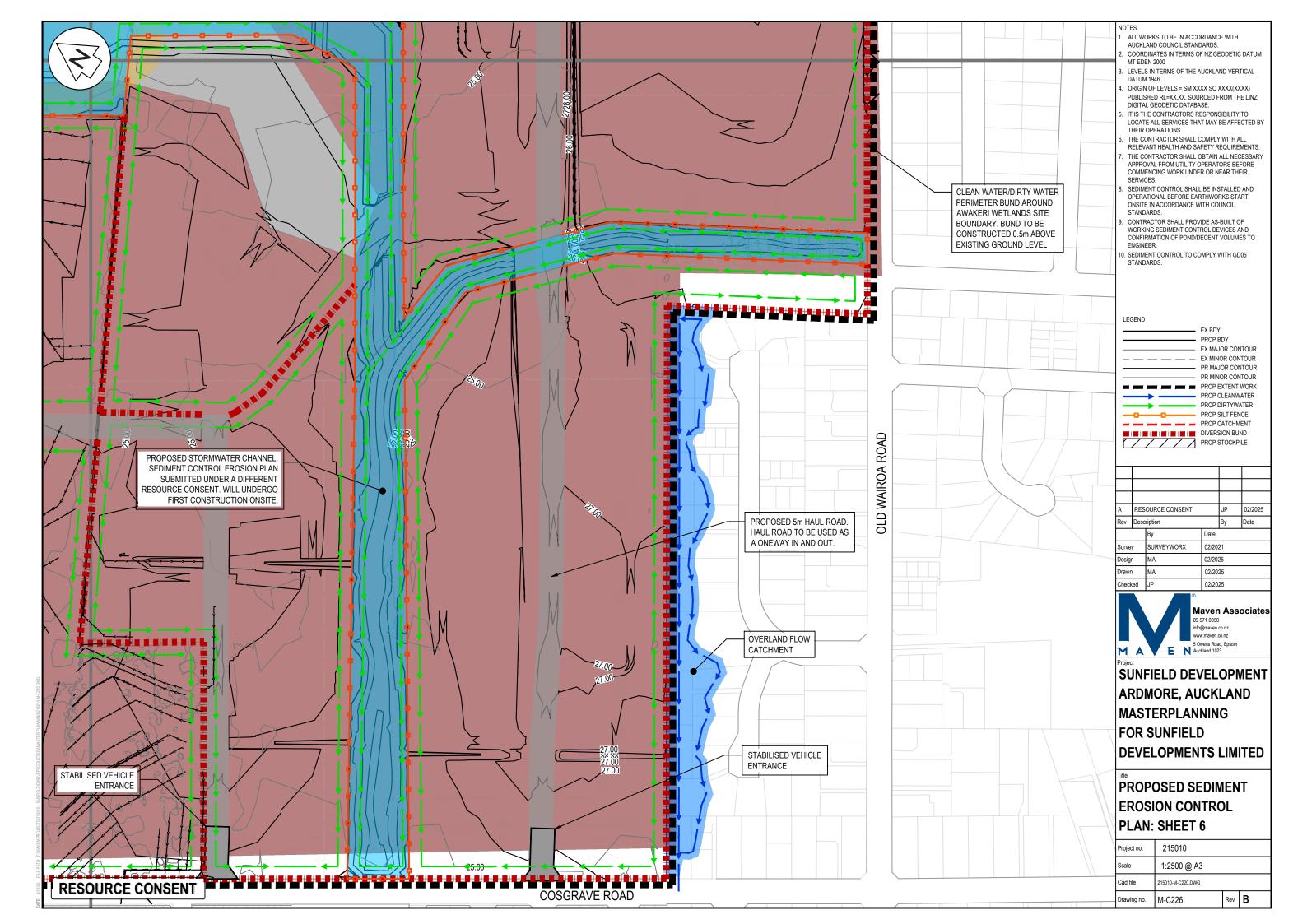


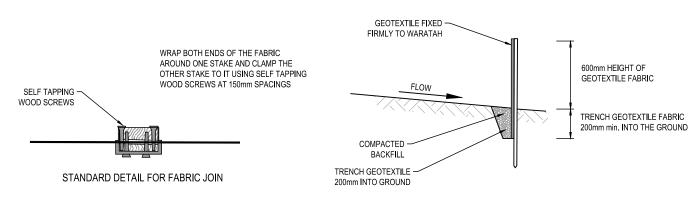






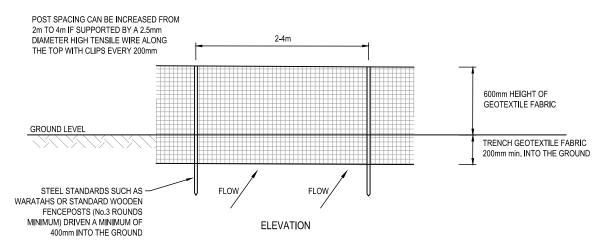


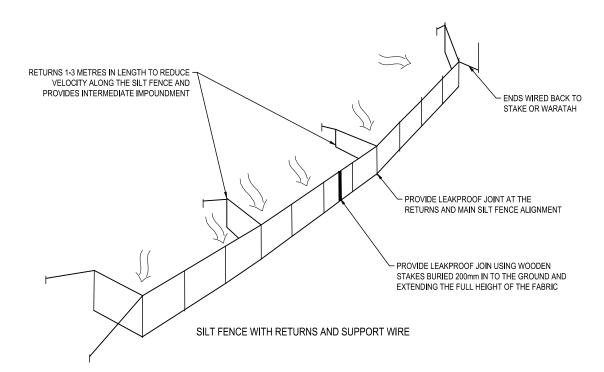




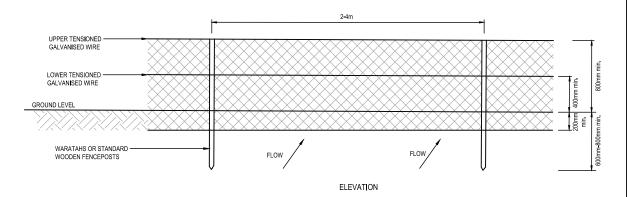
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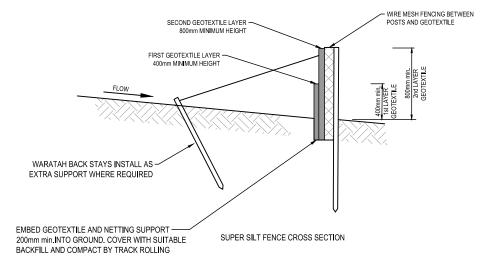
STANDARD DETAIL FOR SILT FENCE





SUPER SILT FENCE DETAIL





NOTES

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- SEDIMENT CONTROL TO COMPLY WITH GD05 STANDARDS.

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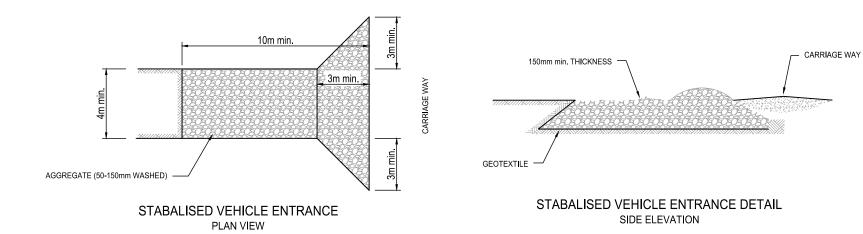
SUNFIELD DEVELOPMENT
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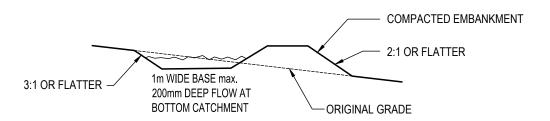
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PROPOSED SEDIMENT EROSION CONTROL DETAILS: SHEET 1

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Scale	N.T.S				
Cad file	215010-M-C230.DWG				
Drawing no.	M-C230 Rev A				

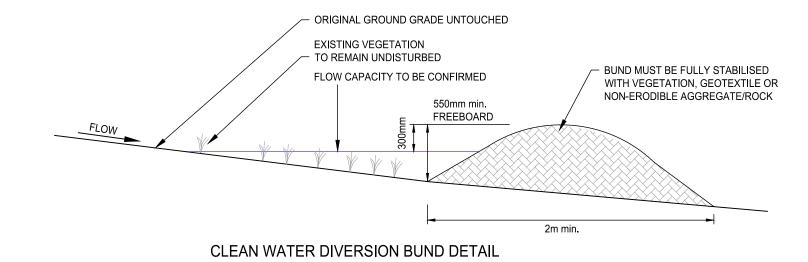
RESOURCE CONSENT





TYPICAL CROSS SECTION OF A RUNOFF DIVERSION

TYPICAL DIMENSIONS UNLESS OTHERWISE NOTED



RESOURCE CONSENT

- . ALL WORKS TO BE IN ACCORDANCE WITH AUCKLAND COUNCIL STANDARDS.
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- SEDIMENT CONTROL TO COMPLY WITH GD05

STANDARDS.

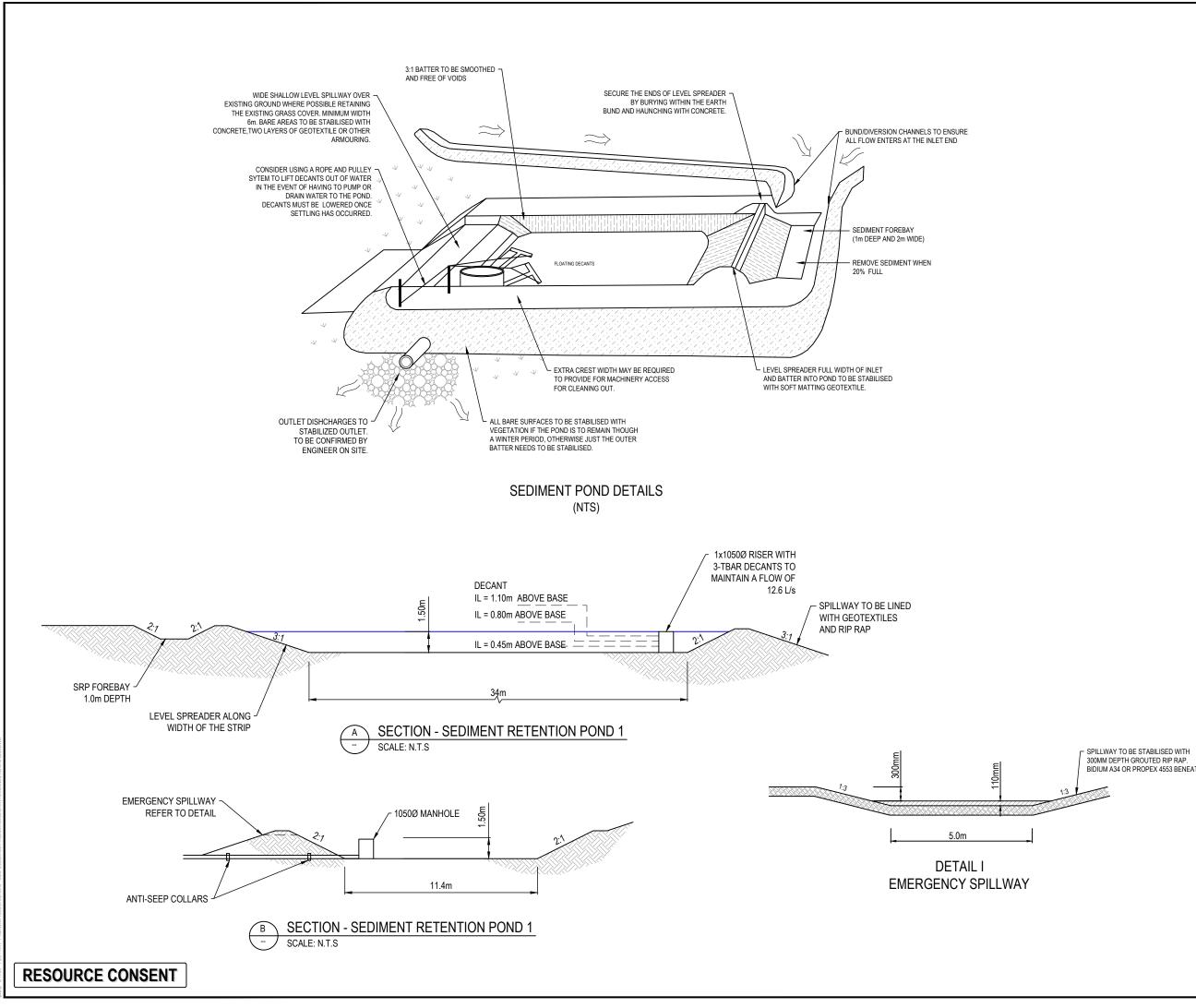
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PROPOSED SEDIMENT **EROSION CONTROL DETAILS: SHEET 2**

Project no.	215010			
Scale	N.T.S			
Cad file	215010-M-C230.DWG			
Drawing no.	M-C231	Rev	Α	



NOTES

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- 7. SEDIMENT CONTROL TO COMPLY WITH GD05 STANDARDS.

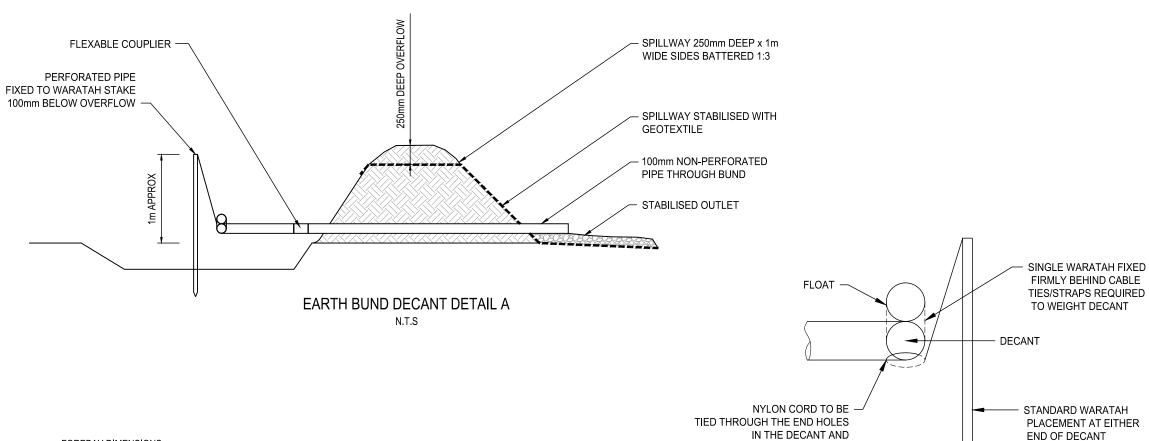
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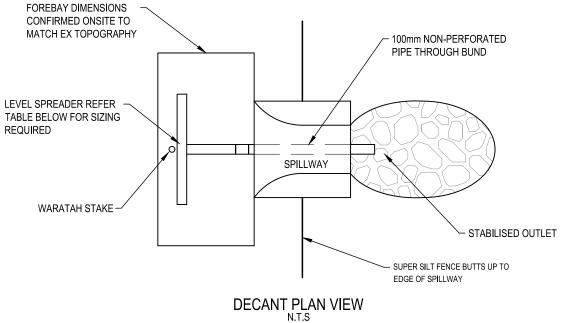


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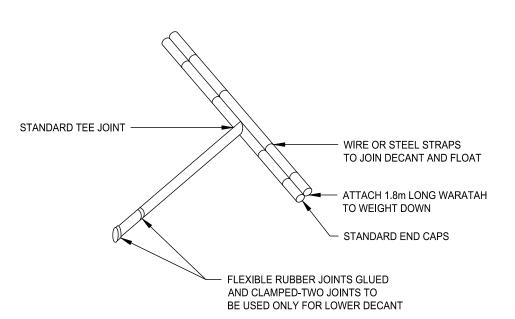
PROPOSED SEDIMENT
EROSION CONTROL
DETAILS: SHEET 3

Project no.	215010		
Scale	N.T.S		
Cad file	215010-M-C230.DWG		
Drawing no.	M-C232	Rev	Α





LEVEL SPREADER DESIGN CRITERIA (20 YEAR STORM EVENT)						
DESIGN FLOW (m³/sec) INLET WIDTH (m) DEPTH (m) END WIDTH (m) LENGTH (mm)						
0-0.3	3	150	1	3		
0.3-0.6	5	180	1	7		
0.6-0.9	7	220	1	10		



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NOTES

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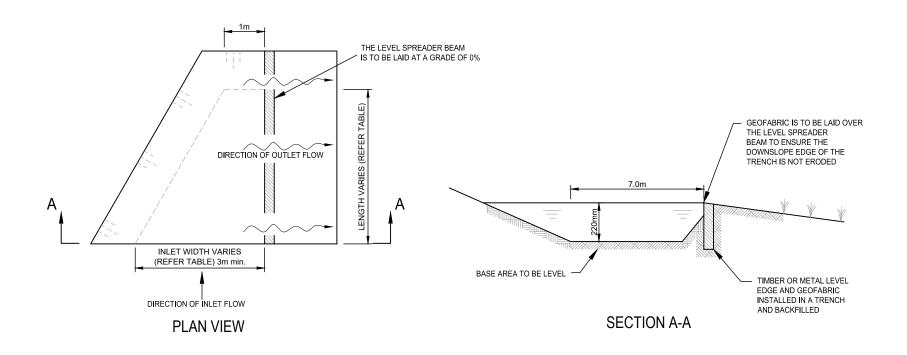
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PROPOSED SEDIMENT EROSION CONTROL

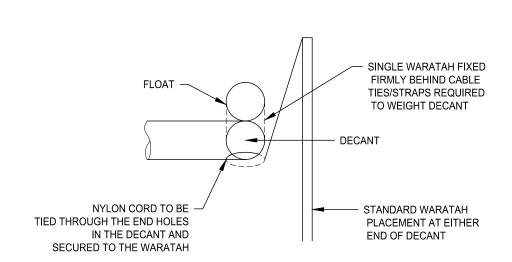
DETAILS: SHEET 4

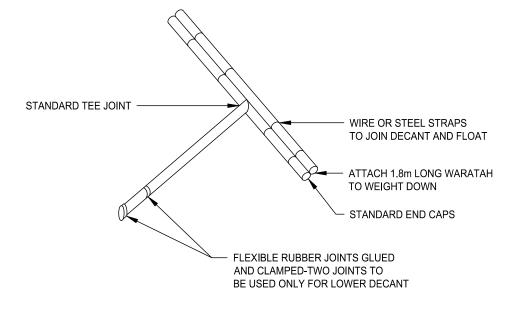
Project no.	215010		
Scale	N.T.S		
Cad file	215010-M-C230.DWG		
Drawing no.	M-C233	Rev	Α

RESOURCE CONSENT



LEVEL SPREADER DESIGN CRITERIA (20 YEAR STORM EVENT)					
DESIGN FLOW (m³/sec) INLET WIDTH (m) DEPTH (m) END WIDTH (m) LENGTH (n)					
0-0.3	3	150	1	3	
0.3-0.6	5	180	1	7	
0.6-0.9	7	220	1	10	





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- SEDIMENT CONTROL TO COMPLY WITH GD05 STANDARDS.

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PROPOSED SEDIMENT EROSION CONTROL DETAILS: SHEET 5

	Drawing no.	M-C234	Rev	Α
	Cad file	215010-M-C230.DWG		
	Scale	N.T.S		
	Project no.	215010		
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RESOURCE CONSENT

