

REVISION DETAILS				YED	
			DESIG	ĒD	
	144	1	DRAV		
7 7 7	<b>ביו</b>		CHEC	D	
			APPR	ΈD	



BUILDING B, LEVEL 1
8 NUGENT ST, GRAFTON,
AUCKLAND 1023
+64 9 308 9229

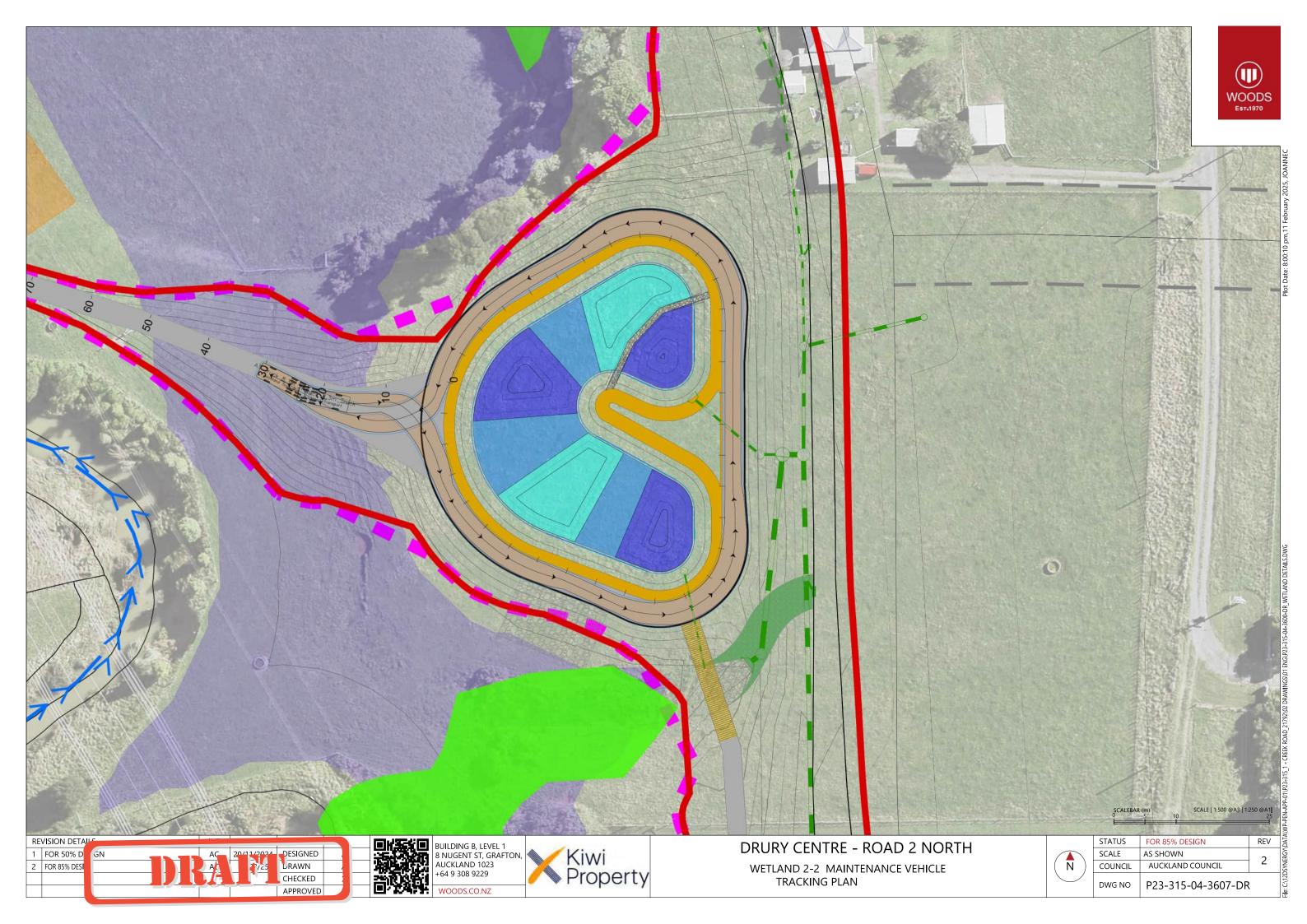
WOODS.CO.NZ



#### DRURY CENTRE - ROAD 2 NORTH

WETLAND MAINTENANCE ACCESS LONG-SECTION DETAIL

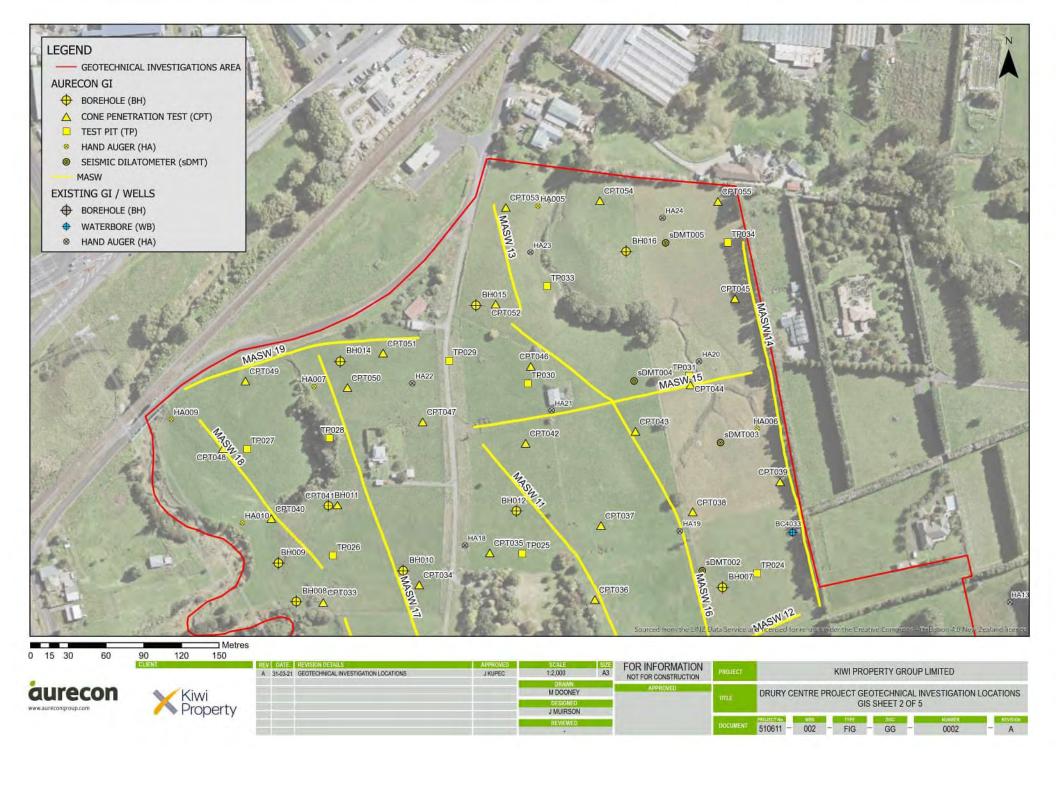
	STATUS	FOR 85% DESIGN
	SCALE	AS SHOWN
$\overline{N}$ )	COUNCIL	AUCKLAND COUNCIL
	DWG NO	P23-315-04-3606-DR





# **APPENDIX C**

Previous Investigations/ Logs





Hand Shear Vane Serial No: DR4938 Correction Factor: 1.519

Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

**BH008** 

Sheet 1 of 6

Met Equ	hod: ipm	: F ent: <sup>-</sup>	INFOR Rotary Tracked Perry G	Core d Rig	Wireline	CO-ORDINATES Easting: Northing: Reduced level:	5: <b>Mt Eden 2000</b> 416451.000m 774474.000m 8.000m (NZVD2016)		Date sta Date co Inclinati Azimuth	mple on:		: 1 9		/2020 /2020		Logged by Input by: Reviewed Verified by	BGW by: GO		
Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	M	aterial Descript	ion	Weathering/USC	Testing		TCR (%)	SCR (%)	RQD (%)	wws ws Fracture cs Log		Defect [	igraphy Descriptio nal Notes		Installation
	_	- - - -	7 77	Т	Om: SILT with minor of Very stiff, moist, low p subangular, fine to mo	lasticity. Gravel is	ce rootlets; brown. weathered,	ML							0m: TA	NURANGA GR	OUP		
HQ3	7	1		TAx							13								
	_	- - -	×		<b>1.5m:</b> Fine to medium orange and light brow				1.5m: SPT 0// 0,0,0,0 N = 0										
SPT	6	2	× × × ×	TAs	<b>1.85m to 2.15m</b> :ligh	t brown, mottled o	range.	SM			22								
НФЗ	_	-  -  -  -	× × ×		2.5m: PUSH TUBE Y	ET TO BE EXTRA	CTED				100								
N54	5	3		TAx	<b>3m:</b> Sandy CLAY with Firm, moist, high plas	ı some silt; light bro ticity. Sand is fine t	own mottled orange. o medium.		3m: SPT 2//		100								
SPT	_	-  -  -		TAc				СН	1,2,1,1 N = 5		100								
НФЗ	4	4	<u>X</u>	TAx	3.6m to 3.68m:Iron weathered, fine sands 3.68m: Silty CLAY wit high plasticity. Sand is \3.85m: Silty CLAY; gr 3.9m: CORE LOSS	stone gravel.  h trace sand; light s fine to medium	brown. Firm, moist,	СН			57								-
SPT	3		X x x x x	TAc	<b>4.5m:</b> Silty CLAY; gre	yish green. Stiff, m	oist, high plasticity.	СН	4.45m: IBHSV 76 kPa 4.5m: SPT 2// 1,1,1,1 N = 4	,	100								
REM 1) B	MARI H008	KS: 3 back	dilled up	on co	mpletion.			•		,					Water I Date Ti No wat	Level Reading ime   Hole Dep ter level record	gs: oth   Water Le ded	evel	



BOREHOLE INFORMATION

Hand Shear Vane Serial No: DR4938 Correction Factor: 1.519

Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

CO-ORDINATES: Mt Eden 2000

**BH008** 

Logged by: BGW

Sheet 2 of 6

BOREH Method Equipm Contrac	l: [ nent: <sup>-</sup>	Rotary Tracke	Core	Wireline Easting: 416451.000m Northing: 774474.000m		Date starte Date comp Inclination: Azimuth:	leted	: 1 g		/2020 /2020	Logged by: BGW Input by: BGW Reviewed by: GO Verified by: JM	
Method R.L. (m)	Length (m)	Graphic Log	Layer Code	Material Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	wws wws Fracture cs Log	Stratigraphy Defect Description Additional Notes	Installation
HQ3	- - - - -	X X X X X X X X X X X X X X X X X X X	TAZ	4.5m: Silty CLAY; greyish green. Stiff, moist, high plasticity.  5.1m: Clayey SILT; grey. Firm, moist, high plasticity. Contains ancient shell impressions, approximately <20mm in size.	CH		100					
Lds -	6	X X X X X X X X X X X X X X X X X X X	TAC	5.85m: Silty CLAY; grey. Very stiff, moist, highly plastic.  6.15m: Clayey SILT with trace organics; grey. Firm, moist, high plasticity. Organics are fibrous <10mm in size. Contains ancient shell impressions, approximately <20mm in size.	СН	5.95m: IBHSV UTP 6m: SPT 1// 1,1,1,1 N = 4	100					
T 103	7	× × × × × × × × × × × × × × × × × × ×					100					
SPT	- - - - 8	× × × × × × × × × × × × × × × × × × ×	TAz		МН	7.5m: SPT 1// 1,0.1,1 N = 3	93				7.92m to 7.95m: No recovery	
HQ3	- - - - -	× × × × × × × × × × × × × × × × × × ×					100					
-1 Ids	9	× × × × × × × × × × × × × × × × × × ×				8.95m: IBHSV UTP 9m: SPT 1// 1,1,1,1 N = 4	100					
-2		*					100					
REMAR 1) BH00	KS: 18 back	kfilled up	on co	empletion.							Water Level Readings: Date Time J Hole Depth   Water Level No water level recorded	

Date started:

15/12/2020



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

Sheet 3 of 6

**BH008** 

Met Equ	nod: ipme	F ent: 1	INFOR Rotary Tracked Perry G	Core d Rig	Wireline	CO-ORDINATES: Easting: Northing: Reduced level:	: <b>Mt Eden 2000</b> 416451.000m 774474.000m 8.000m (NZVD2016)		Date starte Date comp Inclination: Azimuth:	leted	l: 1 9	5/12 5/12 00° I/A	/202 /202	0	Logged by: Input by: Reviewed by Verified by:	BGW BGW C GO JM		
Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	N	Material Description	on	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)		cs vcs Ecs	Stratigr Defect De Additiona	scription	Installation	
HQ3		- - -	×	TAz	<b>6.15m:</b> Clayey SILT wigh plasticity. Organ ancient shell impress	ics are fibrous <10m	nm in size. Contains	мн	10.45m: IBHSV UTP 10.5m: SPT	100								
SPT	-3	_ _ _ _ _ 11	× × × × × × × × × × × × × × × × × × ×	TAx	<b>10.68m:</b> NO RECOV <b>10.95m:</b> Clayey SILT		arov Firm moint		10.5m: SP1 2// 0,0,0,1 -N = 1	40							- - -	
НДЗ		- - - - - -			low plasticity. Organic low plasticity. Organic ancient shell impress	cs are fibrous <10mr	m in size. Contains			100							-	
SPT	-4		× × × × × × × × × × × × × × × × × × ×						12m: SPT 2// 1,0,1,1 N = 3 12m: IBHSV UTP	100				                         			- - - -	
HQ3	-5		<pre></pre>	TAz	13.1m:Trace unwervolcaniclastic gravel.		, fine to medium	МН		100				111			-	
SPT	-6		(		13.5m:Organics are	e fibrous and <50mn	n in length.		13.5m: SPT 1// 1,1,1,1 N = 4	100							- - - -	
HQ3	-7		*							97								
REM 1) B	MARK H008	S: back	dilled up	on co	mpletion.									Wate Date	er Level Readings: Time   Hole Depth vater level recorded	Water Level		



Hand Shear Vane Serial No: DR4938 Correction Factor: 1.519

Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

**BH008** 

Sheet 4 of 6

Me Eq	thod: uipm	ent: -	I <b>NFO</b> F Rotary Fracked Perry G	Core d Rig	Wireline	CO-ORDINATES: Mt Eden 2000 Easting: 416451.000m Northing: 774474.000m Reduced level: 8.000m (NZVD2016)		Date start Date com Inclination Azimuth:	pleted	: (		/2020 /2020		Logged by: Input by: Reviewed by Verified by:	BGW BGW : GO JM	
Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	V	Material Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	wws ws Fracture cs Log	ECS	Stratigr Defect Des Additiona	scription	Installation
SPT	_	-	X X X [X X X	TAc	15m: Silty CLAY with brown. Firm, moist, h <50mm in length.	n minor organics; greyish green mottled nigh plasticity. Organics are fibrous and	СН	15m: SPT 2// 1,0,1,1 N = 3	100				14.97	m to 15m: No reco	very	-
НОЗ	-8	16	で	TAp TAz	high plasticity. Organ ancient shell impress 15.9m: Fibrous PEA 15.96m to 15.99m:	F with trace organics; grey. Firm, moist, lics are fibrous, <10mm in size. Contains sions, approximately <20mm in size.  T; brown. Firm, moist.  Silty Sand inclusion  PEAT; brown. Very stiff, moist, low	MH PT	- 16.3m: IBHSV	100							- - - -
SPT	9	_ _ _ _ _ _ _		TAo	plasticity. \16.3m to 16.33m:F 16.4m: Organic CLA' high plasticity. Sand	Y with trace sand; brown. Firm, moist,	ОН	128/24 kPa 16.5m: SPT 2// 1.1.1.1 N = 4	100							- - - -
HQ3	_	- - - -	x x x x x x x x x x x x x x x x x x x	TAZÍA₽	17.57m: Sandy clayer stiff, moist, low plastion fibrous, <40mm in lea		PT ML		100							-
SPT	-10	18		TAs	17.60m: Clayey, Silty banded brown. Loos length.	r SAND with some organics; light green, e, moist. Organics are fibrous, <40mm in	sc	18m: SPT 3// 21,1,1,1 N = 5	82				18.37	m to 18.45m: No re	ecovery	
НОЗ	<u>-11</u>	19	₹ × *	TAC	green. Firm, moist, h  18.75m: Pumiceous organics; brownish g	with trace sand and organics; brown and igh plasticity. Sand is fine to medium.  SAND with some silt and minor rey. Loose, moist. Sand is fine to medium. and <30mm in length.	СН		100							-
		_ _ _ _		TAs			SM	19.5m: SPT 2// 2,2,2,1 N = 7								
	-12 MARI		-CII		moist, homogeneous	lium SAND with minor silt; green. Loose, s. Sand is predominantly mica and quartz.	SM	. ,	100				Water	Level Readings:	I Wotar !	
1)	3H008	s back	tilled up	on co	mpletion.								No wa	Time   Hole Depth ater level recorded	water Level	



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Hand Shear Vane Serial No: DR4938 Correction Factor: 1.519

Client: **Kiwi Properties Ltd** Project: Drury Development

Location: 108 Flanagan Road, Drury Project Reference: 510611

**BH008** 

Sheet 5 of 6

Library file: AURECON\_AKL\_20201012.GLB Template: AURECON\_AKL\_20170201.GDT\_Report File:

CO-ORDINATES: Mt Eden 2000 **BOREHOLE INFORMATION** Date started: 15/12/2020 BGW Logged by: 15/12/2020 Method: Rotary Core Wireline Easting: 416451.000m Date completed: Input by: **BGW** Equipment: Tracked Rig Contractor: Perry Geotech Northing: 774474.000m Inclination: 90° Reviewed by: GO 8.000m JM Reduced level: Azimuth: N/A Verified by: (NZVD2016) Weathering/USC Code Fracture Log Graphic Log ength (m) Installation R.L. (m) TCR (%) RQD (%) Stratigraphy SCR (%) Testing Method Defect Description Material Description Layer Additional Notes WWS WWS CS CS VCS 19.72m: Fine to medium SAND with minor silt; green. Loose, moist, homogeneous. Sand is predominantly mica and quartz.  $\Pi\Pi\Pi$  $\Pi\Pi\Pi$ 11111 $\Pi \Pi \Pi \Pi$  $\Pi\Pi\Pi$ HQ3  $\Box$ 100 11111 20.54m to 20.68m:...Very thin, undulating laminae, <1mm,  $\Pi\Pi\Pi$ with minor specks of weathered pumice. 11111 SM  $\prod$  $\Pi\Pi\Pi$  $\Pi\Pi\Pi$ -13 21 21m: SPT 5// 1,2,2,2 N = 7  $\Pi\Pi\Pi$  $\Box$  $\Pi\Pi\Pi$ SPT 100 11111 $\Pi \Pi \Pi$ 11111 11111**21.5m:** Fine to medium SAND with minor silt; green. Very dense, moist, moderately cemented, homogeneous. Sand is 11111 11111predominantly mica and quartz. 11111 $\square$  $\Pi\Pi\Pi$ TAs SM 11111НОЗ -14 22 100  $\Box\Box\Box$  $\Pi\Pi\Pi$  $\Pi\Pi\Pi\Pi$ 11111  $\square$ 22.3m: Fine to medium SAND with minor silt; greyish green. 11111 Very dense, moist, uncemented, homogeneous. Sand is predominantly mica and quartz. 1111122.5m: SPT 23// 50 for 20mm N = 50+ 11111 SPT 100 11111 $\Pi\Pi\Pi$  $\square$  $\square$  $\Pi\Pi\Pi\Pi$ -15 23  $\Box$ SM  $\Pi\Pi\Pi$  $\Pi\Pi\Pi$  $\Pi\Pi\Pi$  $\square$ HÖ3 85 1111111111 11111  $\Pi\Pi\Pi$  $\Pi\Pi\Pi$ | | | | | | |23.8m: CORE LOSS 11111ΤĀΧ  $\Pi\Pi\Pi$ -16 24 **24m:** Fine to medium SAND with minor silt; green. Very dense, moist, uncemented. Indistinctly, laminated to very 24m: SPT 17// 31,19 for 25mm N = 50+ 11111 SPT 100  $\Pi \Pi \Pi$ thinly, subhorizontally bedded. Sand is predominantly mica  $\Pi\Pi\Pi$ and quartz.  $\square$ 11111TAs  $\Pi\Pi\Pi$ SM 11111 HQ3  $\Pi\Pi\Pi$ 5 IIIII| | | | | | |11111 $\Pi\Pi\Pi$ 24.9m: CORE LOSS -17 25 Water Level Readings: Date Time | Hole Depth | Water Level No water level recorded REMARKS: BH008 backfilled upon completion.



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

**BH008** 

Sheet 6 of 6

Me Eq	thod: uipme	F ent: T	INFOR Rotary ( racked erry G	Core d Rig	Wireline	CO-ORDINATES: Mt Eden 2000 Easting: 416451.000m Northing: 774474.000m Reduced level: 8.000m (NZVD2016)		Date starte Date comp Inclination: Azimuth:	letec	d: (	15/12/ 15/12/ 90° N/A		Logged by: BGW Input by: BGW Reviewed by: GO Verified by: JM	
Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	٨	Material Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	wws Fracture cs Log vcs Log	Stratigraphy Defect Description Additional Notes	Installation
- ноз		- - - -		ТАх	24.9m: CORE LOSS	um SAND with minor silt; green. Very		25.5m: SPT	52					-
SPT		_		TAs	dense, moist, uncem thinly, subhorizontally pumice. Sand is pred	nented. Indistinctly, laminated to very y bedded. Contains minor, weathered, fine dominantly mica and quartz. 5.76m (Target Depth)	SM	18// 12,38 for 30mm N = 50+	100					

REMARKS:
1) BH008 backfilled upon completion.

Hand Shear Vane Serial No: DR4938 Correction Factor: 1.519

Water Level Readings: Date Time | Hole Depth | Water Level No water level recorded

Database File: 510611 V3.GPJ Library file: AURECON AKL\_20201012 GLB Template: AURECON AKL\_20170201.GDT Report File: AURECON DH LOG V3.9 UDP Date Generated: 8/03/2021



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

**BH009** 

Sheet 1 of 6

	Met Equ	hod: ipme	ent:	INFOR Rotary Tracke Perry G	Core d Rig	e Wireline J	CO-ORDINATES: Mt Eden 2000 Easting: 416437.000m Northing: 774505.000m Reduced level: 8.000m (NZVD2016)		Date starte Date comp Inclination: Azimuth:	letec	d: :		//2020 //2020	Logged by: BGW Input by: BGW Reviewed by: GO Verified by: JM
	Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	N	laterial Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	wws ws Fracture cs Log	Stratigraphy Defect Description Additional Notes
	НДЗ	_	- - - - -	× ; × ; X = - X X = - X X = - X	TAc	Very stiff, moist, low purely subangular, fine to make to make to make to make the total version of the stiff of the total version of t	clay, trace gravel and organics; brown. plasticity. Gravel is weathered, edium sandstone. Organics are fibrous in trace rootlets; yellowish brown, mottled high plasticity.	ML		60				Om: TAURANGA GROUP
	SPT	7	1		TAx	0.9m: NO RECOVER	PY		1.5m: SPT 0// 0.0,0,0 N = 0	0				
Box 1	HQ3	6		X	TAZ	speckled bluish grey, fine, completely weat 2.55m to 2.77m:Iro inclined, laminated to	n oxide staining on indistinct, gently very thin beds.	мн		100				
	SPT	5	3		TAc	brown. Very stiff, moi	rith some silt; light brown mottled orange st, high plasticity. Sand is fine to medium.	СН	2.95m: IBHSV UTP 3m: SPT 3// 3.2,2,3 N = 10	100				- - - -
	НОЗ	4	4	× × × × × × ×	TAc TAs	brown mottled grey, sto medium, complete  4.1m: Sandy CLAY w	edium SAND with trace gravel; orange speckled black. Loose, wet. Gravel is fine ly weathered sandstone.  with some silt; light brown mottled orange igh plasticity. Sand is fine to medium.	SM		81				
2	SPT	_	_ _ _ _	 x x	TAx	4.3m: CORE LOSS 4.5m: Silty CLAY with	n minor sand and trace organics; grey. sticity. Sand is fine to medium. Organics		4.3m: IBHSV 28 kPa 4.5m: SPT 2// 0,1,1,1 N = 3	100				
Box	REN 1. In	3 //ARK vesti 0m g	gation	L Collar is	s reco	orded to an accuracy of ±1 stand installed.	0.0 m horizontal and ±1.0 m vertical.	СН		100	-			Water Level Readings: Date Time   Hole Depth   Water Level No water level recorded



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

**BH009** 

Sheet 2 of 6

Metl Equ	hod: ipme	ent: <sup>-</sup>	INFOF Rotary Fracked Perry G	Core d Ria	Wireline Easting: 416437.000m Northing: 774505.000m		Date starte Date comp Inclination: Azimuth:	letec	1:	16/12 16/12 90° N/A	2/2020 2/2020	Logged by: BGW Input by: BGW Reviewed by: GO Verified by: JM	
Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	Material Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	ws ws mws Fracture cs Log vcs Log	Stratigraphy Defect Description Additional Notes	Installation
НQ3			XX-X-X-X-X-X-X-X-X-X-X-X-X-X-X-X-X-X	TAc	4.5m: Silty CLAY with minor sand and trace organics; grey. Firm, moist, high plasticity. Sand is fine to medium. Organics are fibrous, <5mm in length.  5.9m: Silty CLAY with some organics, gravel and trace sand;	СН		100				3	
SPT	2	6 - - - -		1	grey speckled light green. Firm, moist, high plasticity. Organics are fibrous, <20mm in length. Gravel is fine to medium, completely weathered, subrounded siltstone. Sand is fine to medium.	СН	5.95m: IBHSV 50/12 kPa 6m: SPT 1// 0,1,1,1 N = 3	100					
НОЗ	1	- - 7 - - -			<b>6.85m</b> : Clayey SILT with some gravel, trace sand and organics; grey speckled green. Firm, moist, high plasticity. Gravel is completely weathered, subrounded siltstone. Organics are fibrous, <25mm in length.			100	-				
SPT U54	0	- - 8 - - -	x   x   x   x   x   x   x   x   x   x	TAz		мн	8m: SPT 2// 1.1.1,1,1 N = 4	100					
НОЗ	-1		 				8.95m: IBHSV 44/10 kPa	100					
HQ3 SPT		- - - - -					9m: SPT 2/1 0,2,1,1 N = 4	100					
REM		gatior			rded to an accuracy of ±10.0 m horizontal and ±1.0 m vertical. tand installed.						Wat	ter Level Readings: e Time   Hole Depth   Water Level water level recorded	



Hand Shear Vane Serial No: DR4938 Correction Factor: 1.519

Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

**BH009** 

Sheet 3 of 6

	Metl Equ	hod: ipme	F ent: 1	INFOF Rotary Fracked Perry G	Core d Rig	Wireline	Northing: Reduced level:	Mt Eden 2000 416437.000m 774505.000m 8.000m (NZVD2016)		Date starte Date comp Inclination: Azimuth:	letec	d: 1	6/12 6/12 00° \/A	/2020 /2020		Logged by: Input by: Reviewed b Verified by:	BGW BGW y: GO JM	
	Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	N	laterial Descriptio	n	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	ws ws Fracture		Stratig Defect De Addition	escription	Installation
	НОЗ		_ _ _ _	×		<b>6.85m:</b> Clayey SILT v organics; grey speckl Gravel is completely organics are fibrous,	ed green. Firm, mois weathered, subround	t, high plasticity.		10.45m: IBHSV 38/8	100							-
	SPT	<b>-</b> 3		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \						kPa 10.5m: SPT 1// 1,0,1,1 N = 3	100							-
Box 3	HQ3		- - - - -	× × × × × × × × × × × × × × × × × × ×	TAz				МН		100							
	SPT	-4		× × × × × × × × × × × × × × × × × × ×		<b>12.45m</b> :Greyish gre	nen speckled brown			11.95m: IBHSV 44/10 kPa 12m: SPT 1// 1,1,1,1 N = 4	100							-
	ноз	-5	13	× × × × × × × × × × × × × × × × × × ×	TAc	12.85m: Silty CLAY w stiff, moist, high plasti	vith trace organics; gr	reyish green. Very	СН	13.45m: IBHSV UTP	100							-
Box 4	SPT	<b>-</b> 6		X X X [X  X		<b>13.85m:</b> brown <b>13.94m:</b> Fine to medi	um SAND with minor	r silt; green. Loose,		13.5m: SPT 2// 1,1,1,1 N = 4	100				             			- - - -
	НОЗ		  -  -  -  -  -		TAs	moist. Sand is predor	ninantly mica and qu	artz. edium sand.	SM		100					0 O	have all the state of the state	
		-7 MARK				14.6m: Fine to mediu light brown, speckled 14.77m to 14.86m: 14.86m: Pumiceous f light grey, mottled gre	green. Loose, moist. Clay ine to medium SANE en. Medium dense, I	) with minor silt; moist, uncemented.	SM							ter Level Readings:	hows slight plasticity.	-
	1. <b>I</b> n 2. 1.	vestig .0m g	gation alvan	i co <b>il</b> ar is ised ste	s reco el ups	rded to an accuracy of ±10 stand insta <b>ll</b> ed.	J.U m horizontal and ±1.	U m vertical.							No v	e Time   Hole Depti water level recorde	n   water Level d	



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

Sheet 4 of 6

**BH009** 

	v	vww.a	urecon	group.con	n	Projec	ct Reference: 510611								Sh	eet <b>4</b> of <b>6</b>	
	Met Eau	hod:	F ent: 1	INFOF Rotary Fracked Perry G	Core	Wireline	CO-ORDINATES: Mt Eden 2000 Easting: 416437.000m Northing: 774505.000m Reduced level: 8.000m (NZVD2016)			Date starte Date comp Inclination Azimuth:	pleted	l: 1		/2020 /2020	Logged by: Input by: Reviewed by Verified by:	BGW BGW : GO JM	
	Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	M	aterial Description	Weathering/USC		Testing	TCR (%)	SCR (%)	RQD (%)	wws ws wws Fracture cs Log	Stratigr Defect De Additiona	scription	Installation
Box 4	SPT	_	_ _ _				m SAND with minor silt; green. Medium cemented, homogeneous.	SM	15m: S 10// 7,5,6,7 N = 25	PT	100						- - - -
_	наз	-8									95						- - - - -
	SPT		_ _ _ _ _		TAs	16.5m:Uncemented		SM	16.5m: 6// 3,3,4,3 N = 13		82				16.45m to 16.5m: Core	loss.	- - - - -
	НОЗ	<u>-9</u>									100				16.87m to 16.95m: No r	ecovery.	- - - - -
Box 5	¥ —	-10	_ _ _ _ _ _ _ _ _ _						18m: S		100						- - - -
	SPT	_	_ _ _ _	X	TAx		um SAND with minor silt; green.		4,3,5,4 N = 16		67						-
	HQ3	<u>-11</u>	19		TAs	Medium dense, moist	, uncemented, homogeneous.	SM			100						
Box 6	SPT	-12			TAx	<b>19.81m</b> : NO RECOVI	ERY	SM	19.5m: 6// 3,5,4,4 N = 16		69						
	1. In	MARK Ivesti .0m g	gation	i co <b>ll</b> ar is ised ste	s reco el ups	rded to an accuracy of ±10 tand installed.	0.0 m horizontal and ±1.0 m vertical.								Water Level Readings: Date Time   Hole Depth No water level recorded	Water Level	



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

**BH009** 

Sheet 5 of 6

Met Equ	:hod: iipm	ent: 7	INFOI Rotary Fracke Perry G	Core	Wireline	CO-ORDINATES: Mt Eden 2000 Easting: 416437.000m Northing: 774505.000m Reduced level: 8.000m (NZVD2016)			Date starte Date comp Inclination: Azimuth:	leted	l: 1		/2020 /2020	Inpu Rev	ged by: it by: iewed by fied by:	BGW BGW : GO JM		
Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	N	laterial Description	Weathering/USC		Testing	TCR (%)	SCR (%)	RQD (%)	wws Fracture cs Log ecs Log	De	Stratigr fect Des dditiona	scription	Installation	100000000000000000000000000000000000000
НФЗ	-13	_ _ _ _ _ _ _ _ _		TAs	<b>19.95m:</b> Fine to med Medium dense, mois	um SAND with minor silt; greyish green. t, uncemented, homogeneous.	SM			100								-
SPT		- -		TAx	21m:loose 21.24m: NO RECOV	ERY		21m: SI 3// 2,1,2,1 N = 6	PT	53								
HQ3	-14	22			Medium dense, mois	ium SAND with minor silt; greyish green. t, uncemented, homogeneous. kled yellow. Trace fine completely				100								
SPT	1-15			TAs			SM	22.5m: 8// 6,4,5,7 N = 22	SPT	80				22.86m to 22	.95m: No re	ecovery.		
НФЗ				T						100				23.55m to 24 redrilled.	m: Core sli	pped out of barre	I,	See A TO SEE AND SEE A
SPT		_						24m: SI 6// 5,3,3,7 N = 18	PT	64								O TO Towns A IDE
HQ3	-17			TAx	24.45m: CORE LOS	3		-		0								POPOGO NA MOCHETA
1. li	MARk	(S: gatior	n collar i	s reco el ups	rded to an accuracy of ±1 tand installed.	0.0 m horizontal and ±1.0 m vertical.	1	•						Water Level I Date Time   H No water leve	lole Depth	Water Level		Cile: 640844 V/9 CD1 1.1



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 108 Flanagan Road, Drury
Project Reference: 510611

#### **BH009**

Sheet 6 of 6

Me Equ	thod: uipm	ent: <sup>-</sup>	INFOR Rotary Fracke Perry G	Core	Wireline	CO-ORDINATES: Easting: Northing: Reduced level:	Mt Eden 2000 416437.000m 774505.000m 8.000m (NZVD2016)			Date starte Date comp Inclination Azimuth:	oletec	l: 1		2/2020 2/2020	Logged by Input by: Reviewed Verified by	BGW by: GO	
Method	R.L. (m)	Length (m)	Graphic Log	Layer Code		Material Description						SCR (%)	RQD (%)	wws ws Fracture ws Log ecs	Defect D	igraphy Description nal Notes	Installation
HQ3		_		TAx	24.45m: CORE LOS				0								
SPT				TAs		m: Fine to medium SAND with minor silt; greenish grey. ium dense, moist, uncemented, homogeneous.					100						
	-18	26	× × × ×	non-plastic, dilatant.	; greenish grey. Medi	um dense, wet,	ML										
HQ3	_	_ _ _ _ _		TAs	<b>26.15m:</b> Fine to med Medium dense, mois	Fine to medium SAND with minor silt; greenish grey. dense, moist, uncemented, homogeneous.		SM			86						
	-19	27	Ż	ТАх	<b>26.85m:</b> CORE LOS												
SPT		_ _ _		TAs	27m: Fine to medium Medium dense, mois			SM	27m: S 13// 3,9,7,9 N = 28	ri	100						

End of borehole at 27.45m (Target Depth)

REMARKS:

N. Investigation collar is recorded to an accuracy of ±10.0 m horizontal and ±1.0 m vertical. 2. 1.0m galvanised steel upstand installed.

Hand Shear Vane Serial No: DR4938 Correction Factor: 1.519

Water Level Readings: Date Time | Hole Depth | Water Level No water level recorded

Database File: 510611\_V3.GPJ Library file: AURECON\_AKL\_20201012.GLB Tomplate: AURECON\_AKL\_20170201.GDT Report File: AURECON DH LOG V3.9 0DP Date Generated: 1203/2021



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 132 Flanagan Road, Drury
Project Reference: 510611

Sheet 1 of 6

**BH011** 

Con			rack iv Perry G		ed Drill Rig Northing: 774550.000m ch Ltd Reduced level: 18.000m (NZVD2016)	()	Inclination Azimuth:	1:		√A √A 1		Reviewed by: GO Verified by: JM
nollialvi	R.L. (m)	Length (m)	Graphic Log		Material Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	wws wws Fracture cs Log	Stratigraphy Defect Description Additional Notes
		_	34	_	<b>0m:</b> Silty SAND with some clay; dark brown. Firm, moist, high plasticity.	SM						0m: TOPSOIL
	_	- - -	X × × ×		O.3m: Silty CLAY with minor sand; reddish orange brown.  Firm, moist, high plasticity.  [Completely weathered, reddish orange brown, moderately vesicular BASALT; Extremely weak].							0.3m: SOUTH AUCKLAND VOLCANIC FIELD
		_ _ _	X X X			СН		100				
17	<u>1</u> - -	*	VRb	1m: Silty fine to coarse GRAVEL and COBBLES with some clay; greyish red and black. Medium dense, moist, well graded. Gravel, sub-angular to angular, completely weathered to highly weathered, moderately vesicular. BASALT. Silt is low plasticity.		_						
	_	- - -			[Completely weathered BASALT].	GM	1.5m: SPTC	N/A				1.5m: SPT hammer bouncing
		- - -					20 for 15mm// N = 50+					
	16	2			<b>1.95m</b> : Moderately weathered; grey BASALT. Moderately strong.	MW						
		- - -			2.15m: Highly weathered, reddish brown, slightly vesicular BASALT; extremely weak.  [Silty fine to coarse GRAVEL with minor sand; reddish brown.  Medium dense, moist,well graded. Gravel, sub-angular to langular, highly weathered, slightly vesicular basalt).	HW		100	27	27		2.15m: Recovered as broken basalt
	-			VWb	2.35m: Moderately weathered; grey BASALT. Moderately strong.  2.55m: Highly weathered, reddish brown, slightly vesicular BASALT; extremely weak.  [Fine to coarse GRAVEL with some silt and trace clay; reddish							2.55m: Recovered as gravels and cobbles.
	15	- - 3 -			brown. Medium dense, dry].	HW	3m: SPTC 6//					
		- -			3.2m: Highly weathered, dark brown mottled orange, slightly vesicular BASALT; extremely weak. [Clayey silty fine to coarse GRAVEL; dark brown mottled orange. Medium dense, moist, well graded. Gravel,		4,5,6,8 N = 23	N/A				
	_	 			sub-angular to angular, highly weathered, slightly vesicular BASALT, extremely weak. Clay is high plasticity].							
	14	- - 4						100				
		_ _ _		VRb		HW						
	_	-  -					4.5m: SPTC 12// 8,11,15,15 N = 49					
	12	- - - 5					- 40	N/A				
l'n		S: gation			ded to an accuracy of ±10 m horizontal and ±1 m vertical.	GM	<u> </u>	100	<u> </u>			Water Level Readings: Date Time   Hole Depth   Water Level (1) 15/01/21 00:00   m   7.1 m bgl



Hand Shear Vane Serial No: 359 Correction Factor: 1.503

Client: Kiwi Properties Ltd
Project: Drury Development
Location: 132 Flanagan Road, Drury
Project Reference: 510611

## **BH011**

Sheet 2 of 6

	Metho Equip	od: me	F ent: 1		Core Ioun	Wireline ted Drill Rig		6.000m 0.000m Im		Date started: 14/01/2021 Date completed: 15/01/2021 Inclination: 90° Azimuth: N/A					Logged by: STH Input by: STH Reviewed by: GO Verified by: JM				
	Method	K.L. (m)	Length (m)	Graphic Log	Layer Code	N	Material Description		Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	www. www. Fracture	ECS	Stratigi Defect De Additiona	scription	Installation	
	НОЗ		- - - -			black. Loose, saturat angular, completely viextremely weak. Slift i (Completely weathern 5.15m: Sifty clayey fir yellow and grey. Loosub-angular to angula sub-angular to angula basalt, extremely weathern	ed BASALT].  The to medium Gravel; brown  se, moist, poorly graded. Gra  ar, completely weathered, his  ak. Silt and clay is high plasti  ed BASALT].	GM GM		100								-	
Box 2	SPTC	2	- 6 - - - -			mottled yellow and greatly sub-angular to angular basalt, extremely weat [Completely weathered]	medium GRAVEL with minor rey. Loose, moist, poorly gra ar, completely weathered, hi ak. Clay is high plasticity. ed BASALT]. ır change, black mottled ye <b>l</b> k	ded. Gravel, ghly vesicular	GC	6m: SPTC 4// 2,2,2,2 N = 8	N/A								-
	P 103	1	- - - - 7 - -		VRb		red, brownish orange mottled	ł yellow,			100								- - - -
-	LdS1	0				highly vesicular BAS, [Clayey fine to coarse orange mottled yellov sub-angular to angul basalt, extremely we: 7.45m: Clayey fine to orange and yellow. L sub-angular to angular	e GRAVEL with minor silt; bn w. Loose; moist, well graded, ar, completely weathered, his ak. Clay and silt is high plastic medium GRAVEL; brown moose, moist, poorly graded. ( ar, completely weathered, memely weak. Clay is high pla	Gravel, ghly vesicular / icity] J nottled Gravel, oderately	GC	7.5m: SPT 3// 2.2.2.2 N = 8	100								5 V3 9 0DP Date Generated: 8/03/2021
Box 3	HQ3		- - - - -	× × × × × × × × × × × × × × × × × × ×			edium SAND with minor clay e, moist. Silt and clay is low p		SM		100				8.15m:	TAURANGA GR	OUP		20170201 GDT Report File: AURECON DH LOC
-	SPT	9	9	× × × × × ×	TAs	8.9m: Silty fine to me yellow. Medium dens 8.95m to 9.05m:Mi	dium SAND with some clay; e, moist. Silt and clay is low nor organics	brownish plasticity.	SM	9m: SPT 3// 2,2,3,3 N = 10	100								1. 20201012, GLB Template: AURECON AKL
Box 4	REMA 1. Inve	estig	gation	× × × × × × × × × × × × × × × × × × ×	s reco el ups	rded to an accuracy of ±1 tand installed.	0 m horizontal and ±1 m vertical.				100				Date Ti	.evel Readings: me   Hole Depth 01/21 00:00   m	Water Level   7.1 m bgl		File: 510611 V3.GPJ Library file: AURECON AK



Hand Shear Vane Serial No: 359 Correction Factor: 1.503

Client: Kiwi Properties Ltd
Project: Drury Development
Location: 132 Flanagan Road, Drury
Project Reference: 510611

## **BH011**

Sheet 3 of 6

I E	/leth Equi	nod: ipme	F ent: 1	INFOR Rotary Frack M Perry G	Core Ioun	TION  Wireline ted Drill Rig sch Ltd	CO-ORDINATES: Mt Eden 2000 Easting: 416476.000m Northing: 774550.000m Reduced level: 18.000m (NZVD2016)	Date start Date com Inclination Azimuth:	pleted	: ;		/2021 /2021	Logged by: STH Input by: STH Reviewed by: GO Verified by: JM		
	Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	N	/laterial Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	wws Fracture	Stratigraphy Defect Description Additional Notes	Installation
	HO3		- - - -	× × × ×		8.9m: Silty fine to me yellow. Medium dens	edium SAND with some clay; brownis se, moist. Silt and clay is low plasticit	sh y.	O.S. COT	100					
	니 시 시 시 시 시 시 시 시 시 시 시 시 시 시 시 시 시 시 시	7	- - - - 11	× × × ×		10.9m: Fine to mediu	um SAND with some silt and trace cla v. Medium dense, moist, uniformly gr	5/ 3, N	0.5m: SPT / 4,5,6 = 18	100					
Box 4	наз		- - -			Silt and clay is low pl	asticity.			100					
- B		6	_ _ _ _ 					12	≧m: SPT						
!	l ds		- - -		TAs			3, N	4,4,4 = 15	100					
	HO3	5						SP		100					
	I AS	4						6/3,	3.5m: SPT / 4,5,5 = 17	100					
Box 5	HQ3		- - - - -							100					
	REM	3 IARK	_  15 :S:			14.9m to 14.92m:N	Moderately cemented							ter Level Readings:	
- 1 -	1. In	vesti	gation	ı co <b>ll</b> ar i: ised ste	s reco el ups	orded to an accuracy of ±1 stand insta <b>ll</b> ed.	0 m horizontal and ±1 m vertical.						<b>Dat</b> (1)	te Time   Hole Depth   Water Level 15/01/21 00:00   m   7.1 m bgl	



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 132 Flanagan Road, Drury
Project Reference: 510611

## **BH011**

Sheet 4 of 6

www.aurecongroup.com Project Reference: 510611 Sheet 4 of 6											
Method: Equipment:	E INFORMA Rotary Core : Track Mour : Perry Geote	e Wireline nted Drill Rig	CO-ORDINATES: Mt Eden 2000 Easting: 416476.000m Northing: 774550.000m Reduced level: 18.000m (NZVD2016)	10	Date starte Date comp Inclination: Azimuth:	leted		5/01/ )°	/2021 /2021	Logged by: STH Input by: STH Reviewed by: GO Verified by: JM	
Method R.L. (m)	Graphic Log Layer Code	N	laterial Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	wws Fracture cs Log cs Log Ecs	Stratigraphy Defect Description Additional Notes	Installation
TPS -	X X X X	15m: Silty CLAY with plasticity. Sand is find	with trace sand; grey. Very stiff, moist, high s fine to medium.		15m: SPT 2// 1,1,1,1 N = 4 15m: IBHSV UTP	100					
	6 X X X X 			СН		100					- - -
	× × × × × × × × × × × × × × × × × × ×	dense, moist, well graden and the state of t	medium SAND; greyish green. Medium aded. inor clay; greyish green. Very stiff,	SM							
				ML	16.5m: SPT 2// 1,2,2,2 N = 7 16.5m: IBHSV UTP	100					- - - -
——————————————————————————————————————	*		greyish green. Very stiff, moist, high inor clay; greyish green. Very stiff,	СН		100					- - - - -
0 18	8 × × × × × × × × × × × × × × × × × × ×				18m: SPT 2// 2,2,2,2 N = 8 18m: IBHSV UTP	100					- - - -
- - - -	X X X X X X X X X X X X X X X X X X X			ML							- - - -
S -1 19	9 × × × × × × × × × × × × × × × × × × ×					100					
450	× × × × × × × × × × × × × × × × × × ×				19.5m: IBHSV UTP	100					
REMARKS:  1. Investigation collar is recorded to an accuracy of ±10 m horizontal and ±1 m vertical.  2. 1.0m galvanised steel upstand installed.  Water Level Readings: Date Time   Hole Depth   Water Level (1) 15/01/21 00:00   m   7.1 m bgl											



Client: Kiwi Properties Ltd
Project: Drury Development
Location: 132 Flanagan Road, Drury
Project Reference: 510611

**BH011** 

Sheet 5 of 6

Me Eq	thod: uipm	Fent: 1	rack N	Core ⁄loun	TION  Wireline ted Drill Rig ch Ltd	CO-ORDINATES: Mt Eden 2000 Easting: 416476.000m Northing: 774550.000m Reduced level: 18.000m (NZVD2016)		Date starte Date comp Inclination: Azimuth:	letec	l: 1	4/01  5/01  0°  /A			Logged by: STH Input by: STH Reviewed by: GO Verified by: JM	
Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	N	faterial Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	l	cs vcs Ecs	Stratigraphy Defect Description Additional Notes	not-oll otion
SPT		- - -	× × × × × × × × × × × × × × × × × × ×	TAZ	moist, low plasticity.	inor clay; greyish green. Very stiff,	ML	20m: SPT 4// 3,3,3,3 N = 12	100					5m: Washed out sand	
HQ3	-3	_ _ _ _ _ _ _		TAx	20.45m: CORE LOS				52						
SPT	-5		× × × × × × × × × × × × × × × × × × ×		20.95m: SILT with mi moist, low plasticity.	inor clay; greyish green. Very stiff,		21m: SPT 4// 3,3,2,3 N = 11 21m: IBHSV UTP	100						
HQ3	4_		× × × × × × × × × × × × × × × × × × ×				ML		100						
SPT	_	- - - - -	X X X X X X X X X X X X X X X X X X X		<b>22.6m</b> : SILT with son high plasticity.	ne clay; greyish green. Very stiff, moist,	МН	22.5m: SPT 5// 3.3,3,3 N = 12	100						
НФЗ	-5		× × × × × × × × × × × × × × × × × × ×	TAZ	23.1m: SILT with min low plasticity.	or clay; greyish green. Very stiff, moist,		23.5m: IBHSV UTP	100						
SPT	-6	24	×				ML	24m: SPT 5// 3,3,3,4 N = 13	100						
HQ3	_	_ _ _ _	× × × × × × × × × × × × × × × × × × ×						100						
1.1	REMARKS:  1. Investigation collar is recorded to an accuracy of ±10 m horizontal and ±1 m vertical.  2. 1.0m galvanised steel upstand installed.  Water Level Readings: Date Time   Hole Depth   Water Level (1) 15/01/21 00:00   m   7.1 m bgl														



Client: **Kiwi Properties Ltd** Project: Drury Development

Location: 132 Flanagan Road, Drury Project Reference: 510611

**BH011** 

Sheet 6 of 6

**BOREHOLE INFORMATION** Method: Rotary Core Wireline Equipment: Track Mounted Drill Rig Contractor: Perry Geotech Ltd CO-ORDINATES: Mt Eden 2000 416476.000m 774550.000m 18.000m Easting: Northing: Reduced level: (NZVD2016)

14/01/2021 Date started: Date completed: 15/01/2021 Inclination: 90° N/A Azimuth:

Logged by: STH Input by: STH Reviewed by: GO Verified by: JM STH STH

						(112102010)	(IVEVBEOTO)							_
	Method	R.L. (m)	Length (m)	Graphic Log	Layer Code	Material Description	Weathering/USC	Testing	TCR (%)	SCR (%)	RQD (%)	wws Fracture	Stratigraphy Defect Description Additional Notes	Installation
Box 8	SPT HQ3	_	- - - - - -	× × × × × × × × × × × × × × × × × × ×	TAz	23.1m: SILT with minor clay; greyish green. Very stiff, moist, low plasticity.	ML	25m: IBHSV UTP  25.5m: SPT 4// 2,2,3,3 N = 10	100					

End of borehole at 25.95m (Target depth reached)

REMARKS:

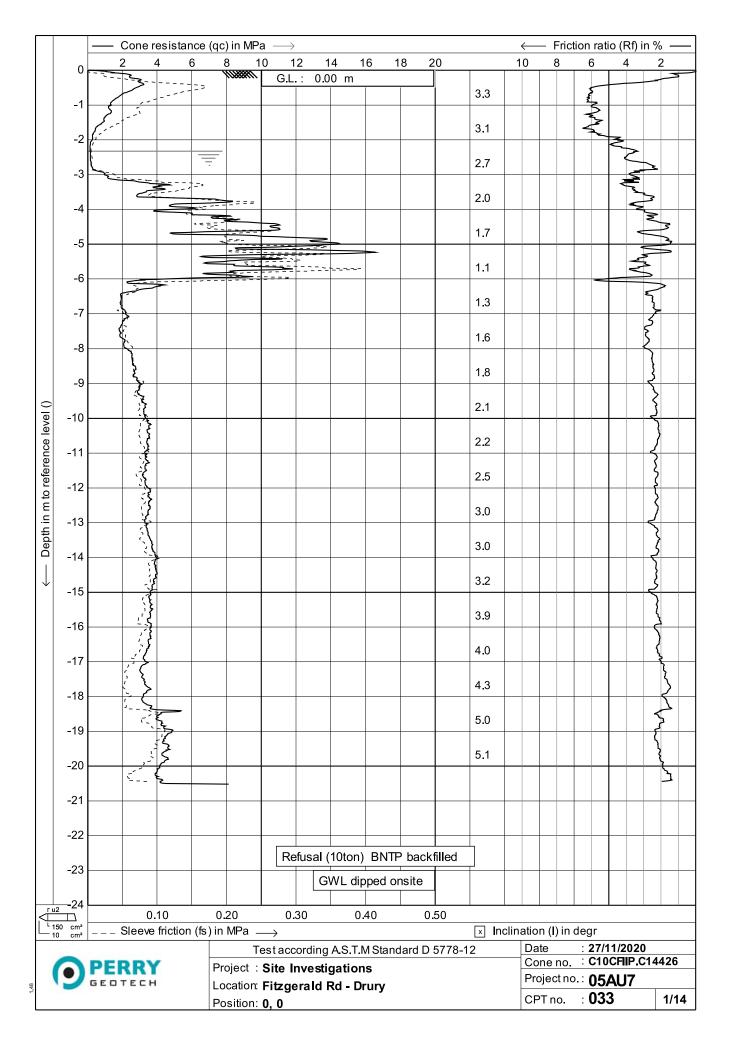
1. Investigation collar is recorded to an accuracy of ±10 m horizontal and ±1 m vertical.

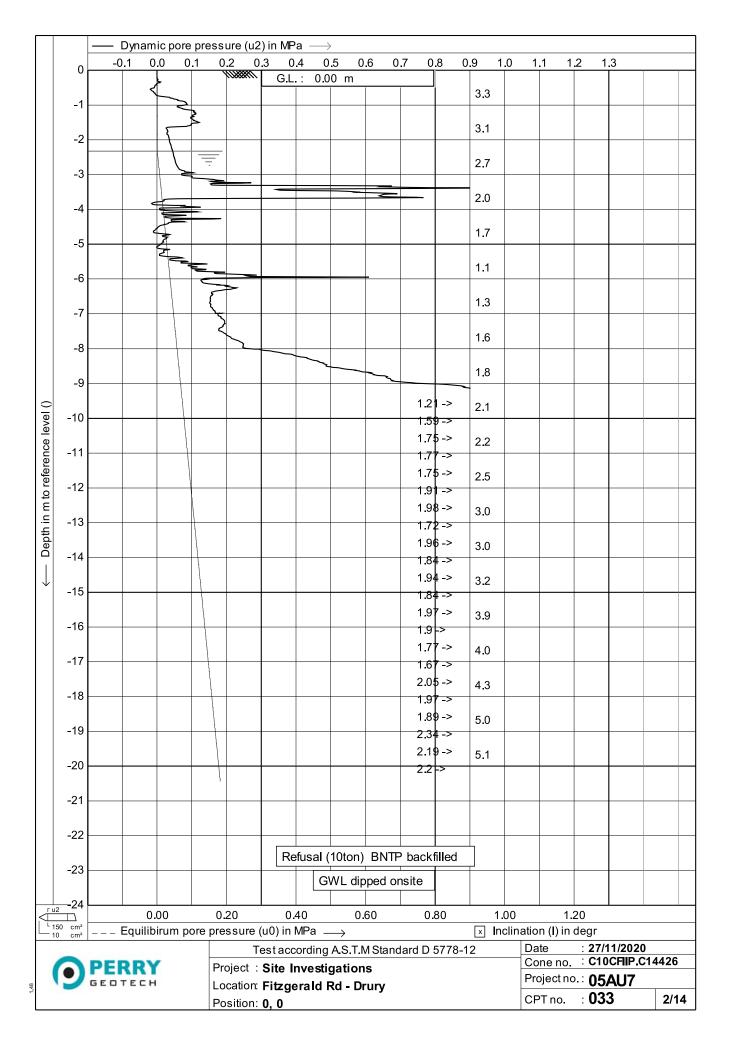
2. 1.0m galvanised steel upstand installed.

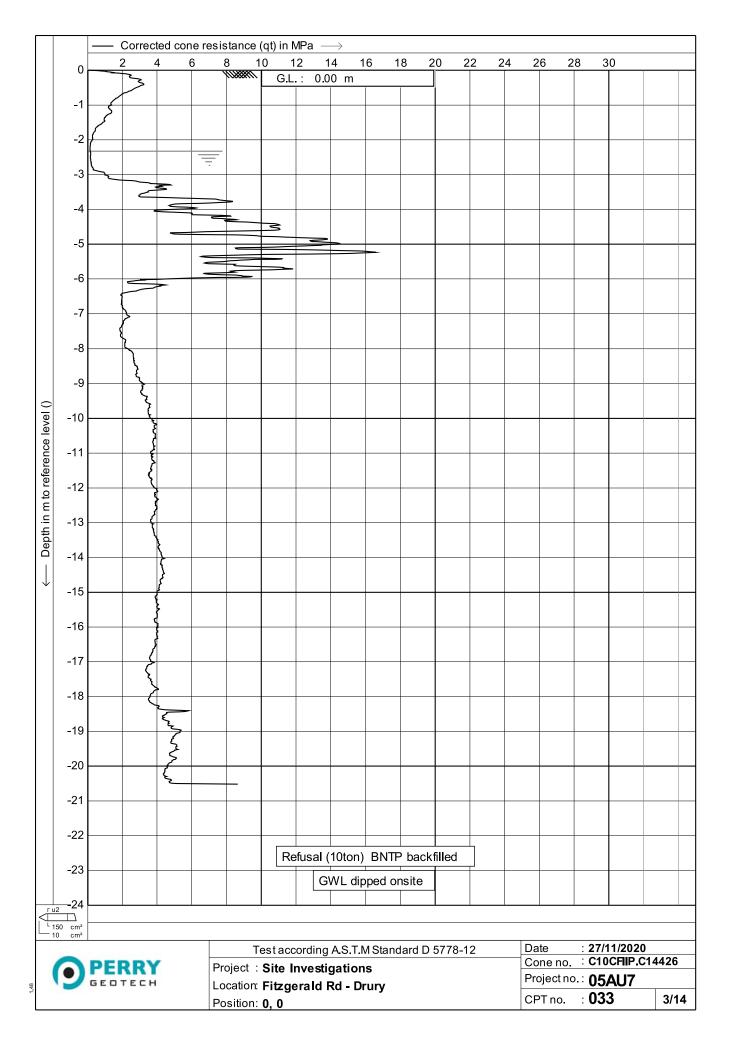
Hand Shear Vane Serial No: 359 Correction Factor: 1.503

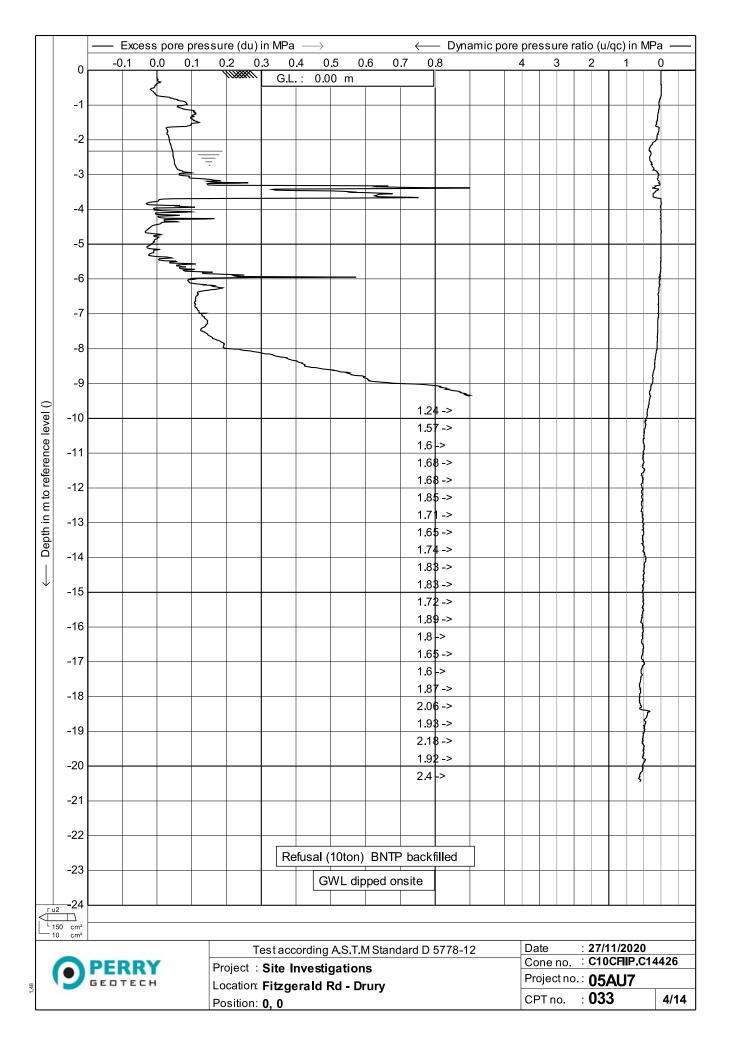
Water Level Readings: Date Time | Hole Depth | Water Level (1) 15/01/21 00:00 | m | 7.1 m bgl

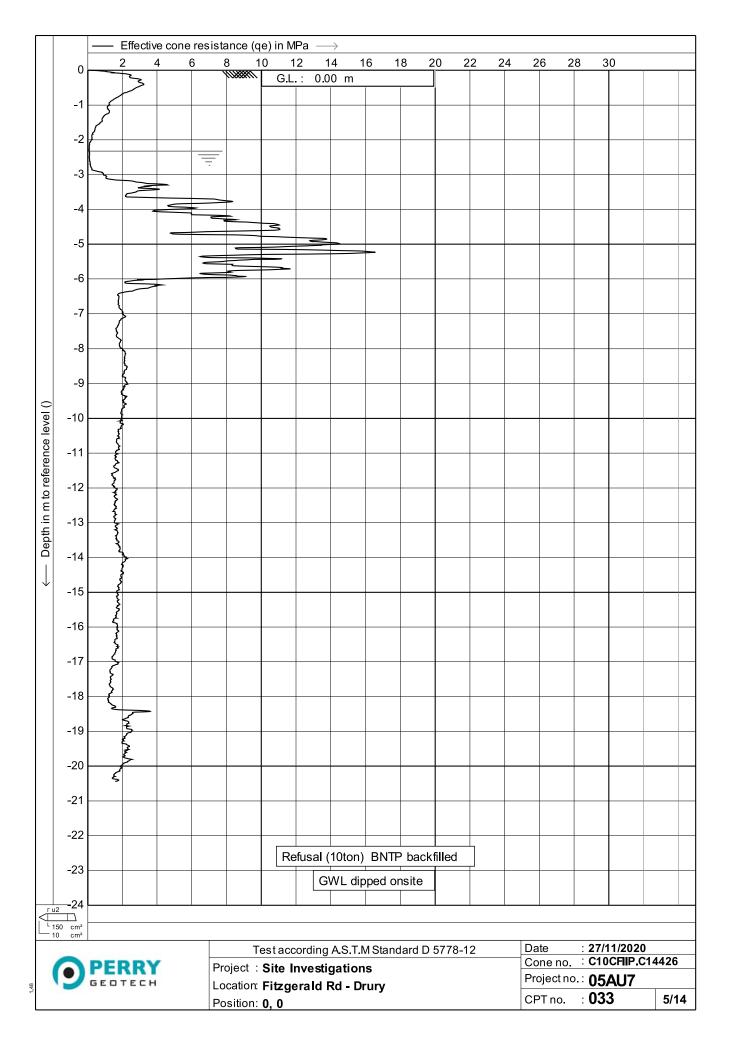
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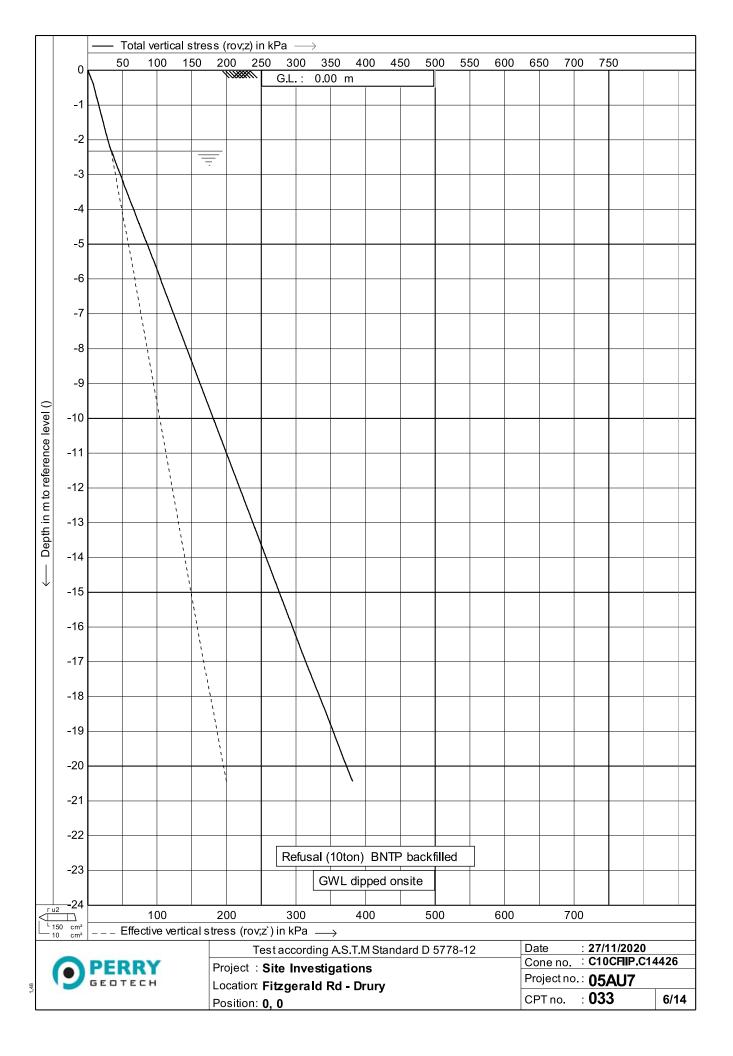


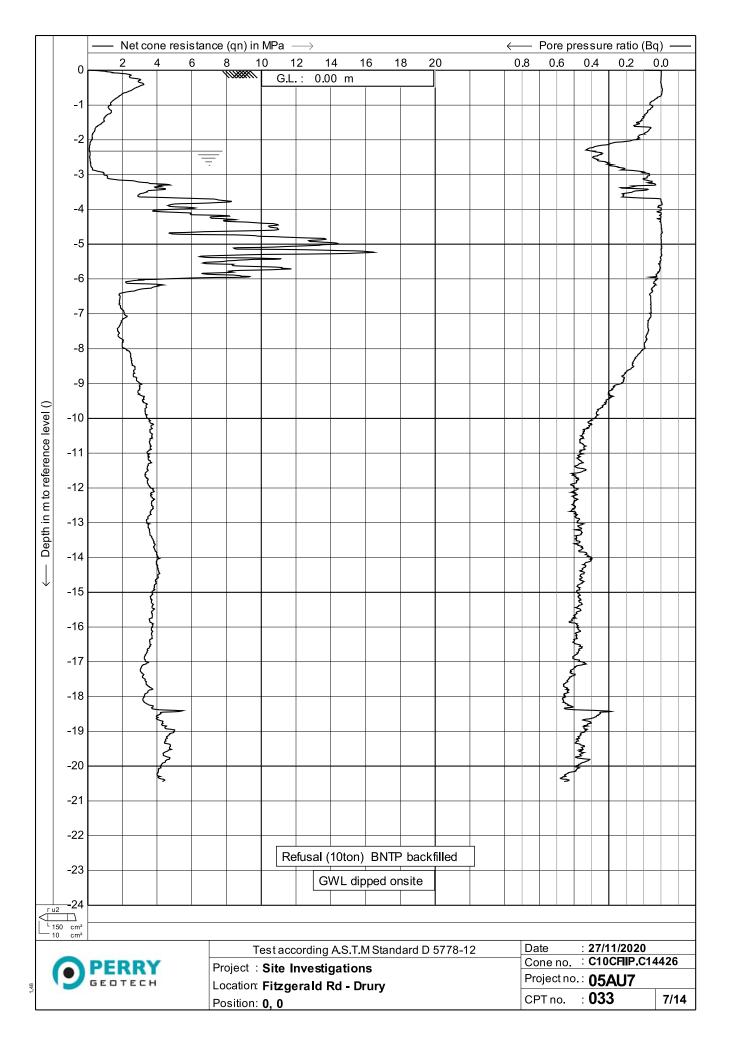


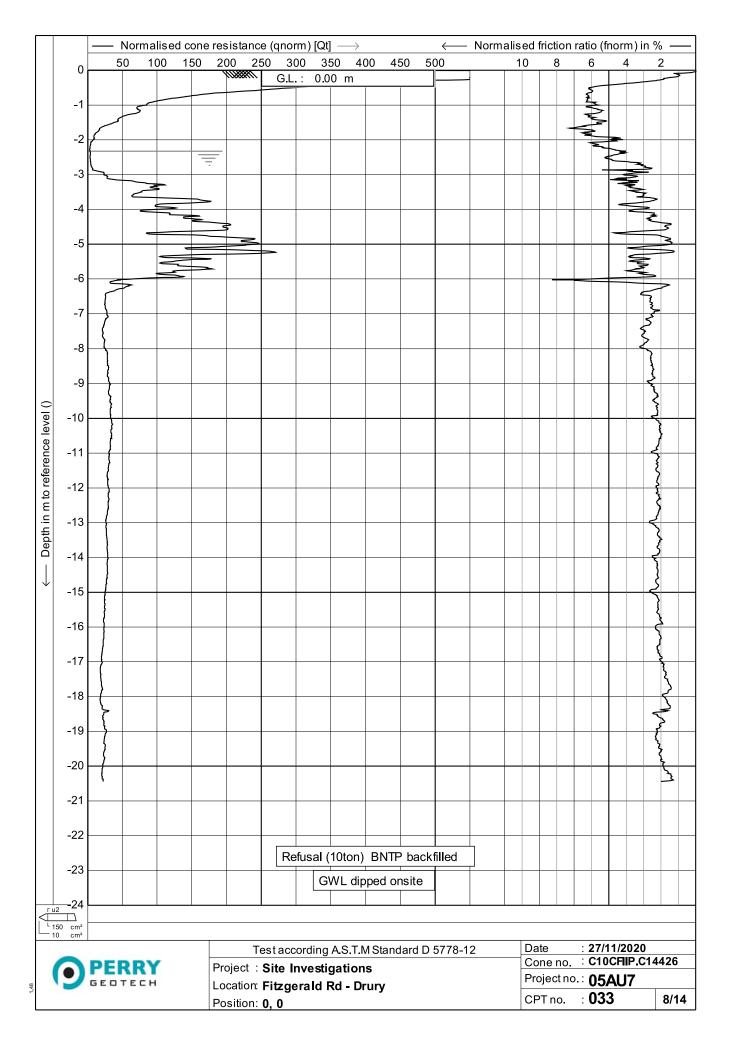


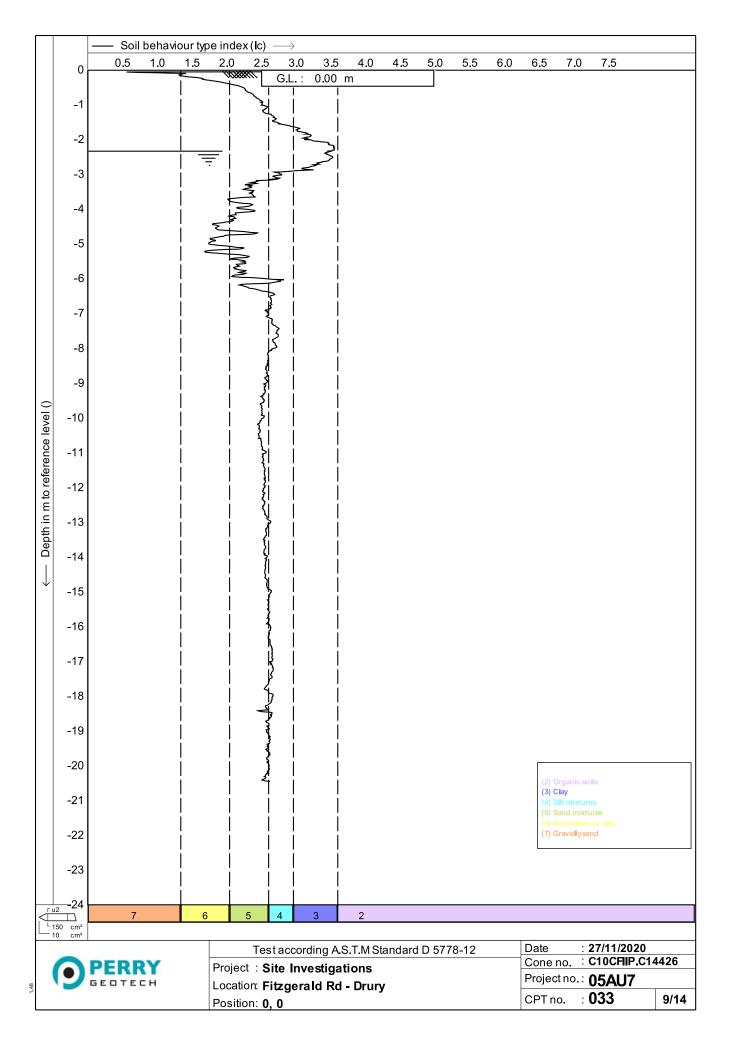


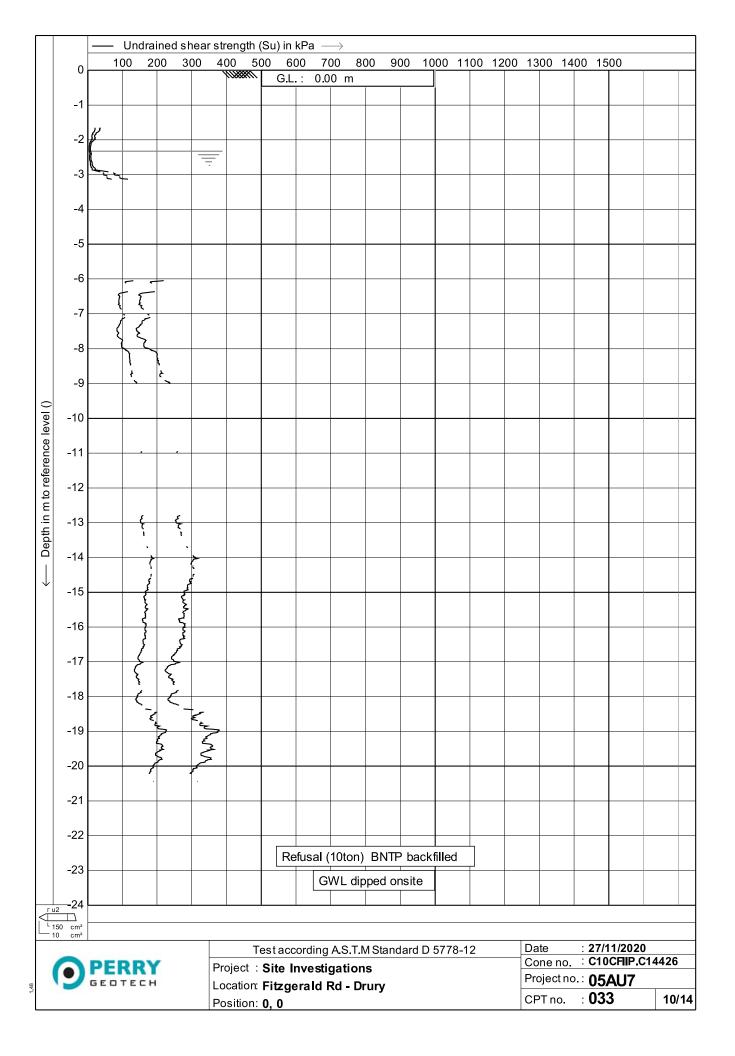


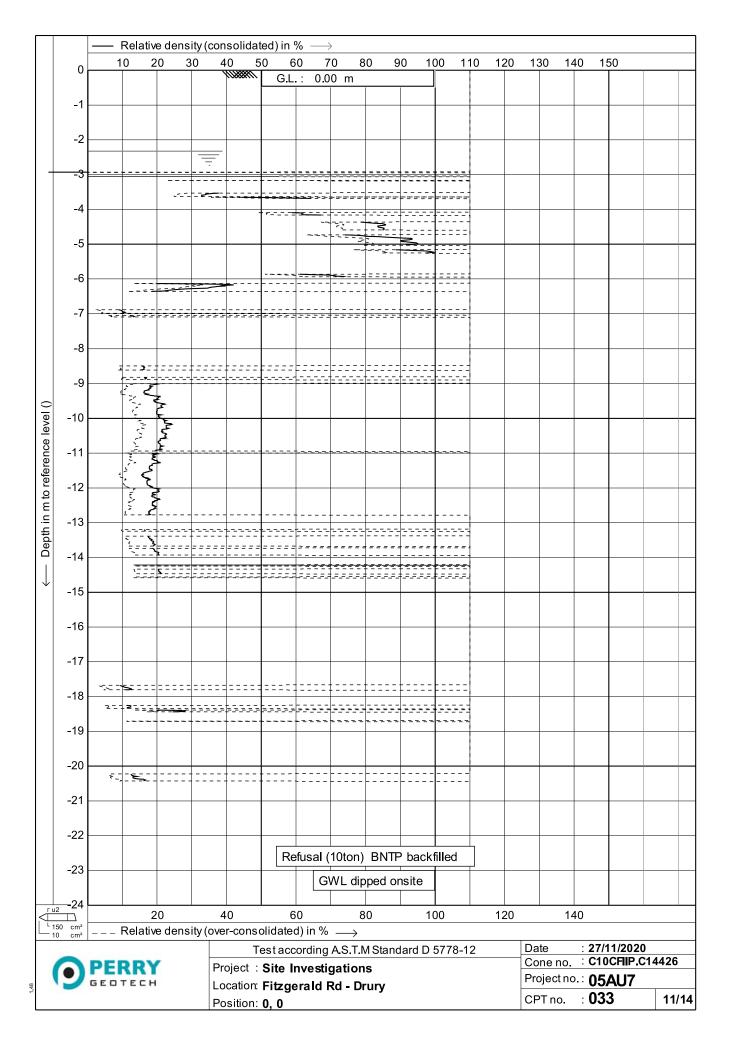


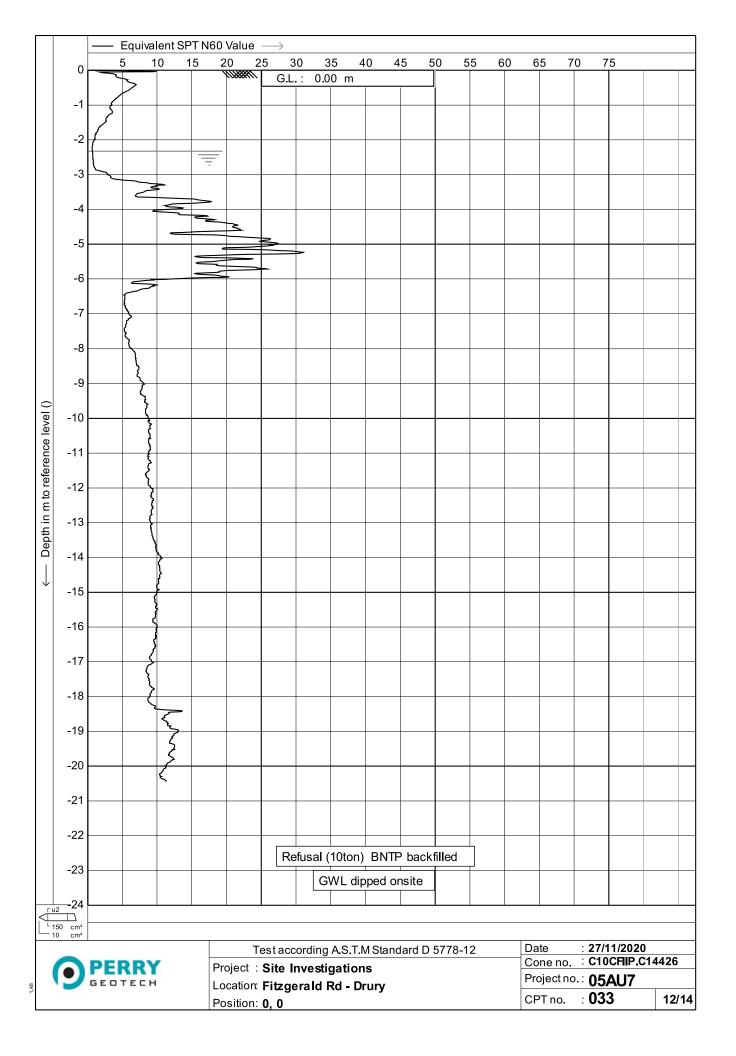


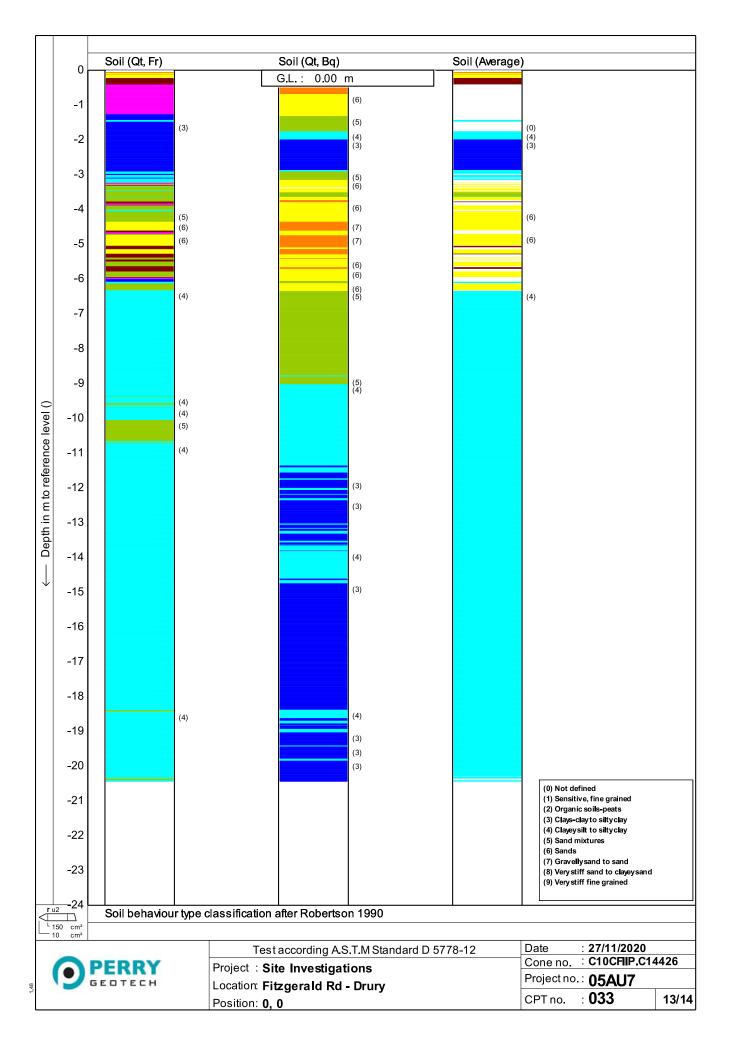


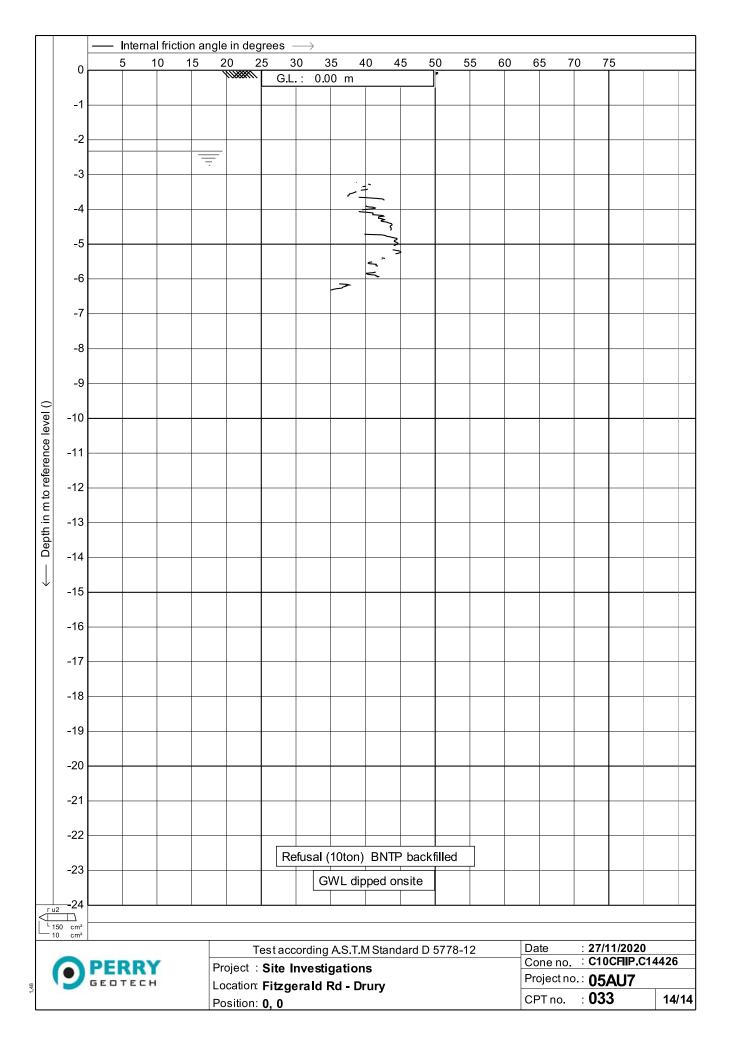


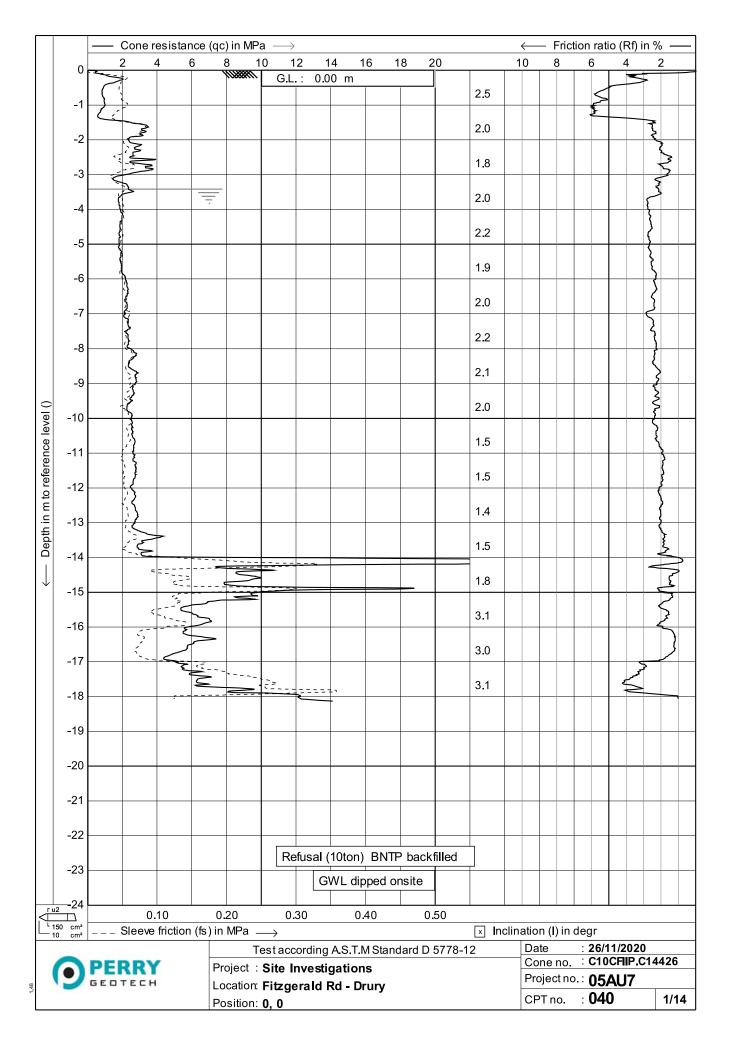


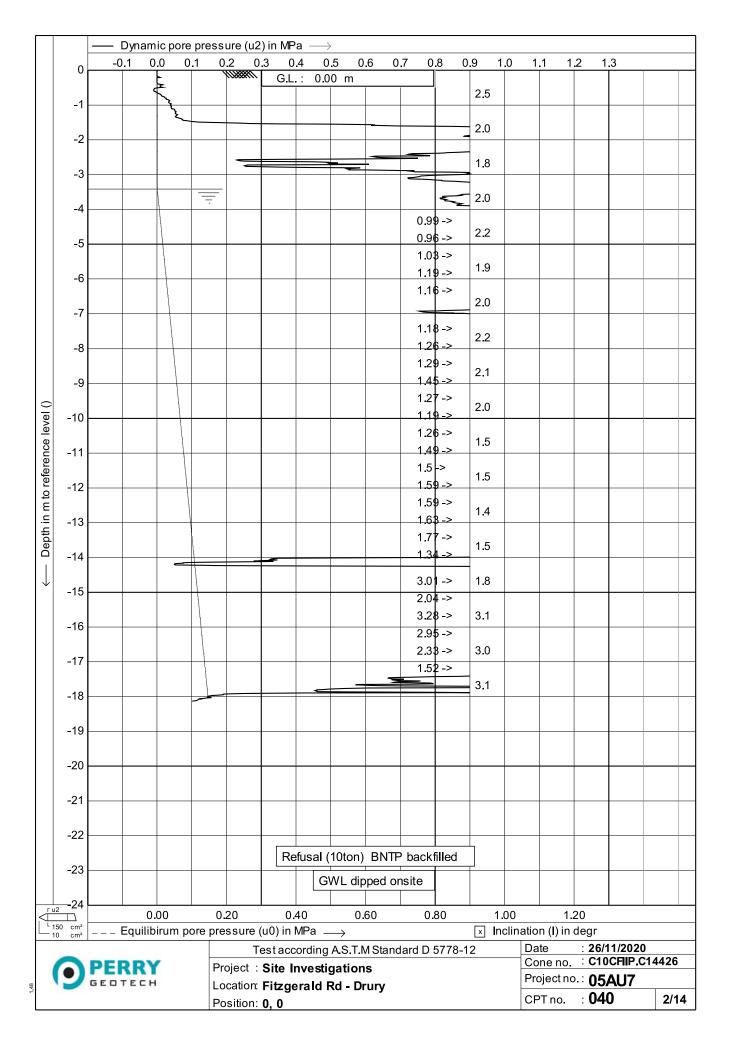


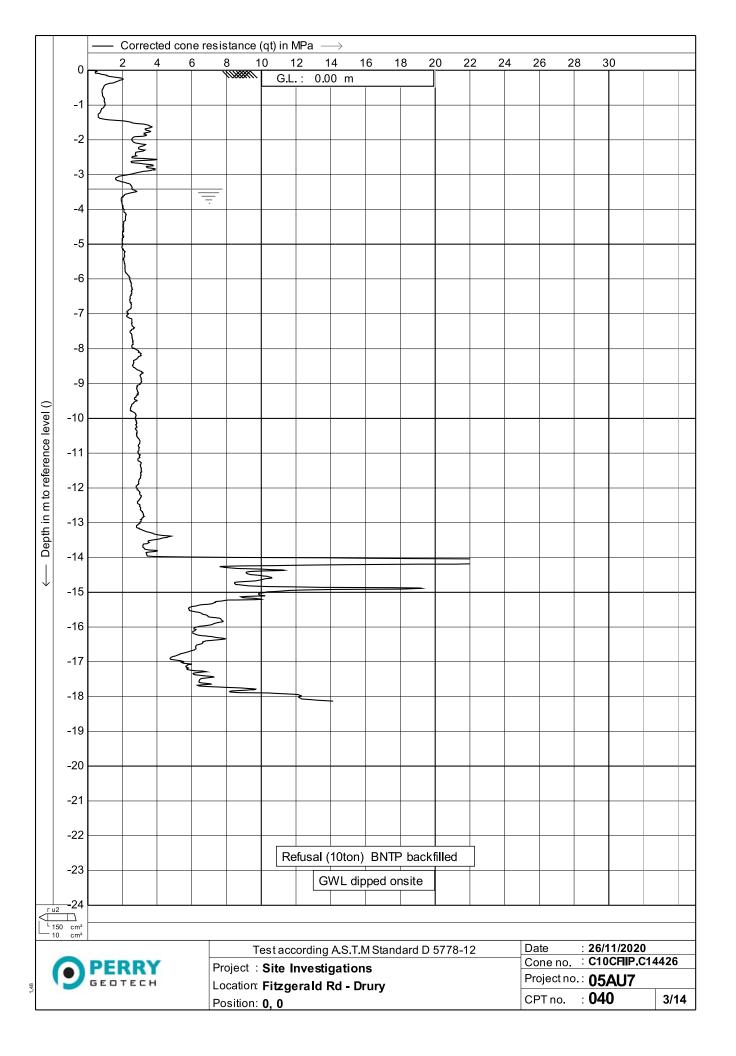


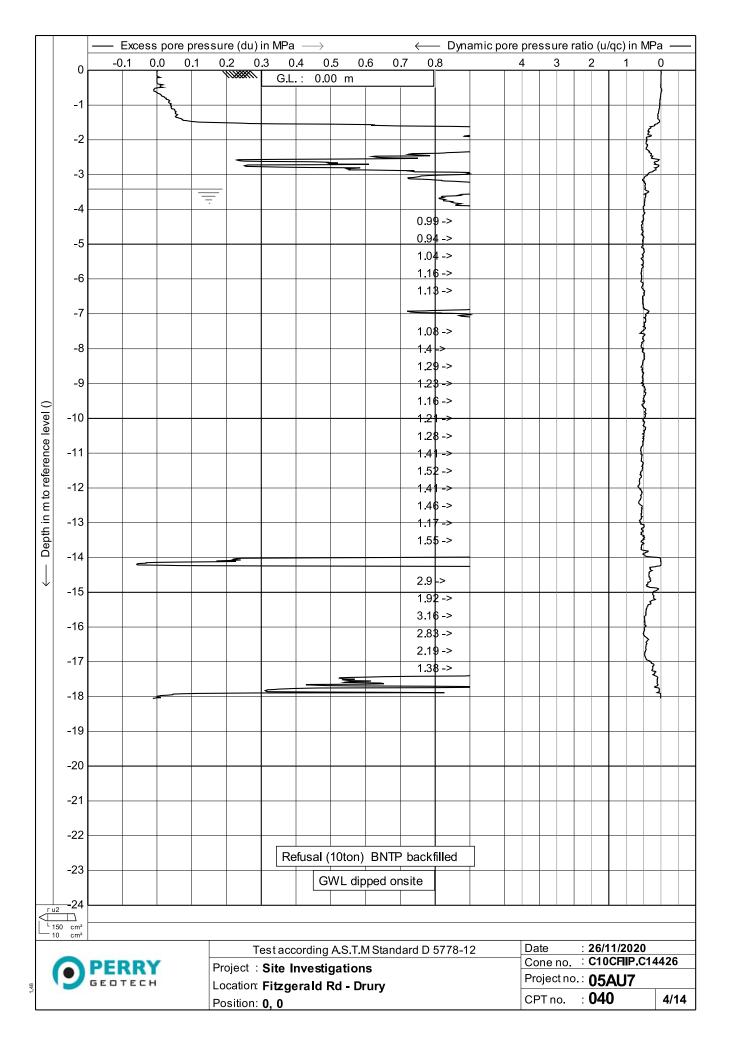


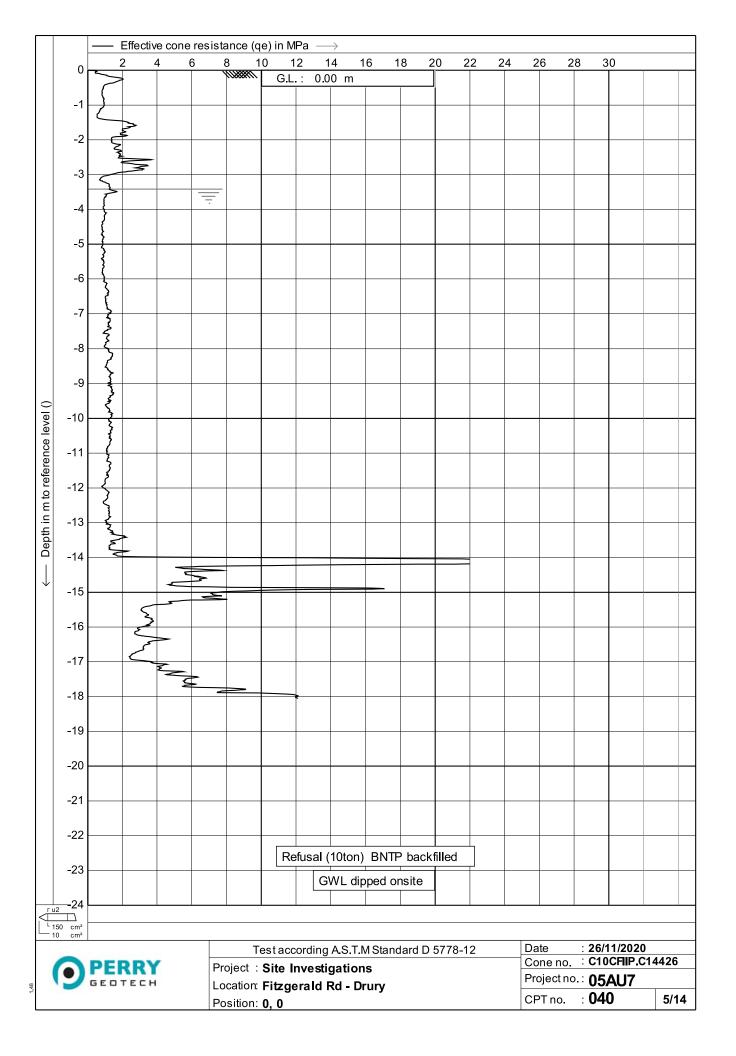


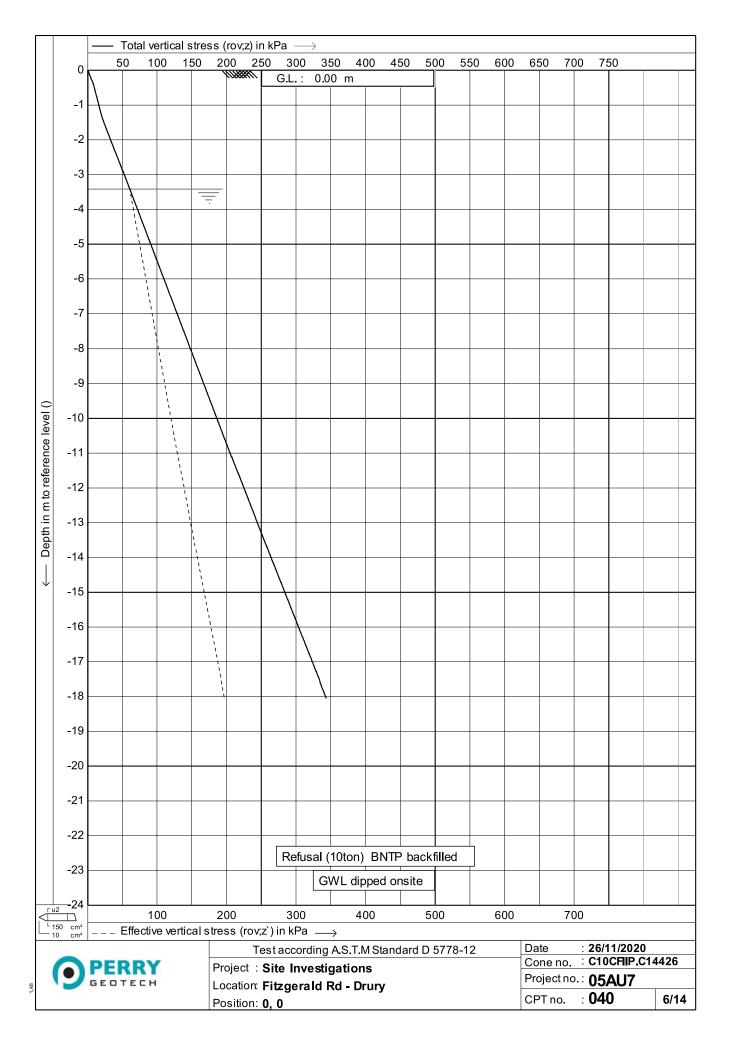


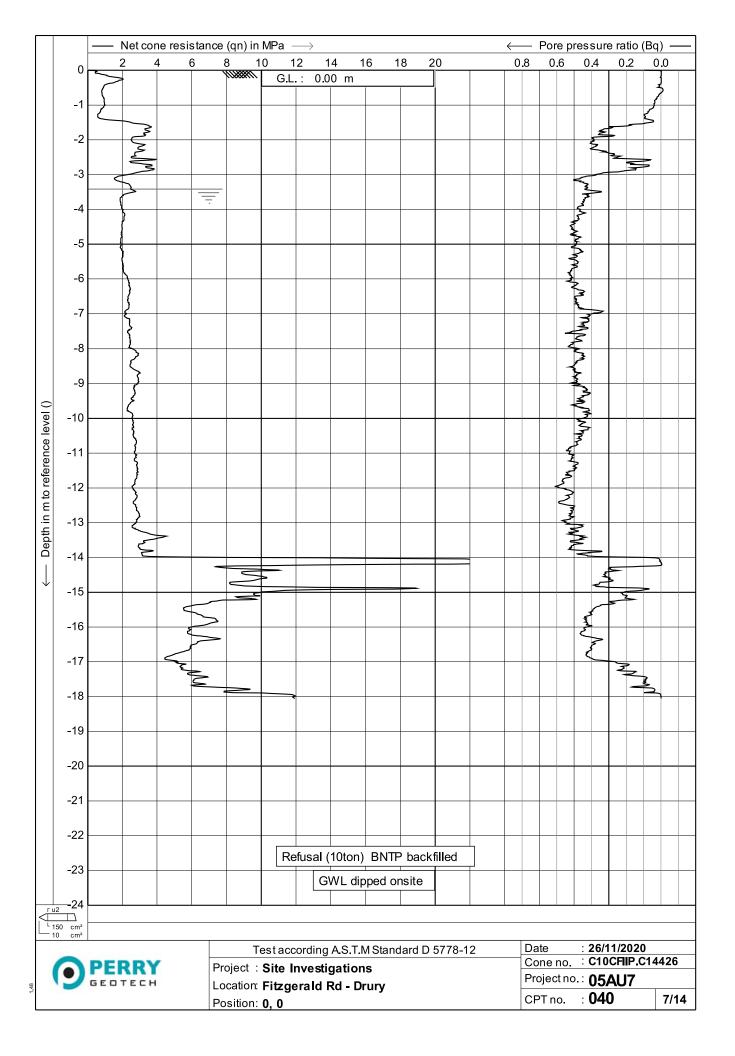


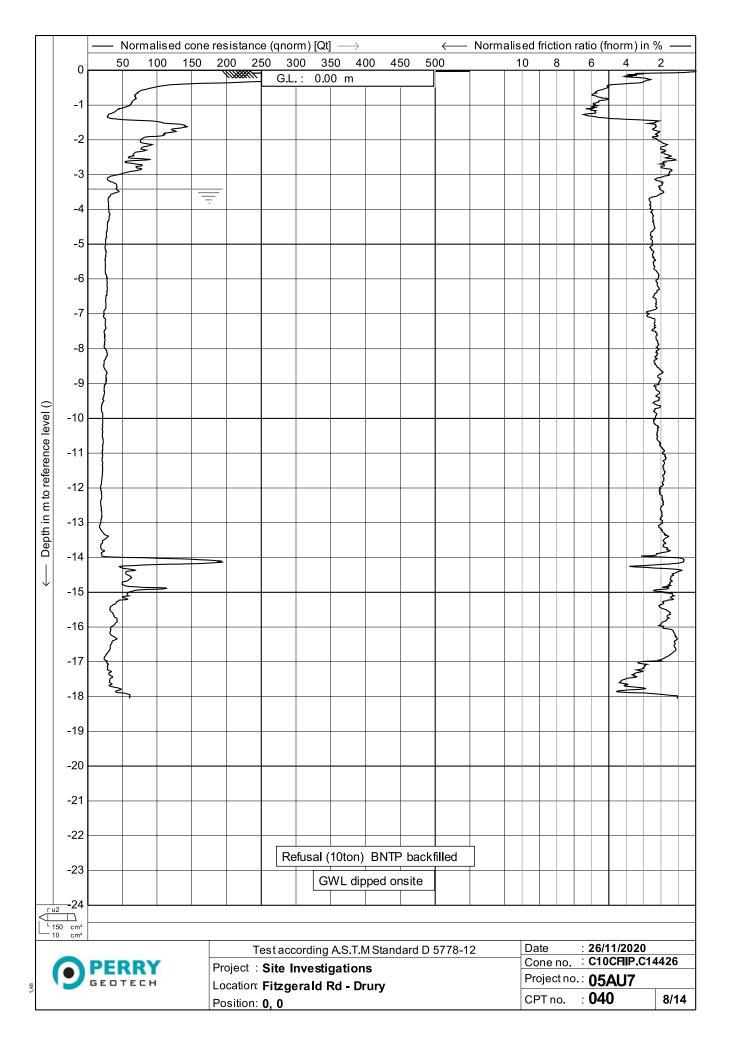


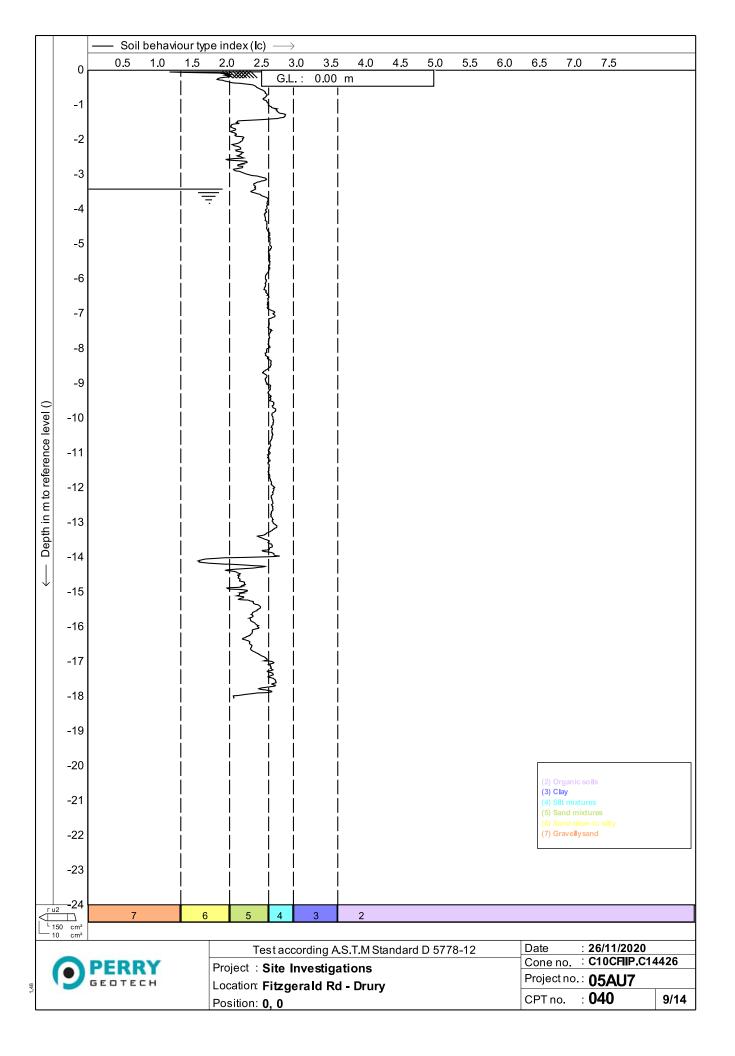


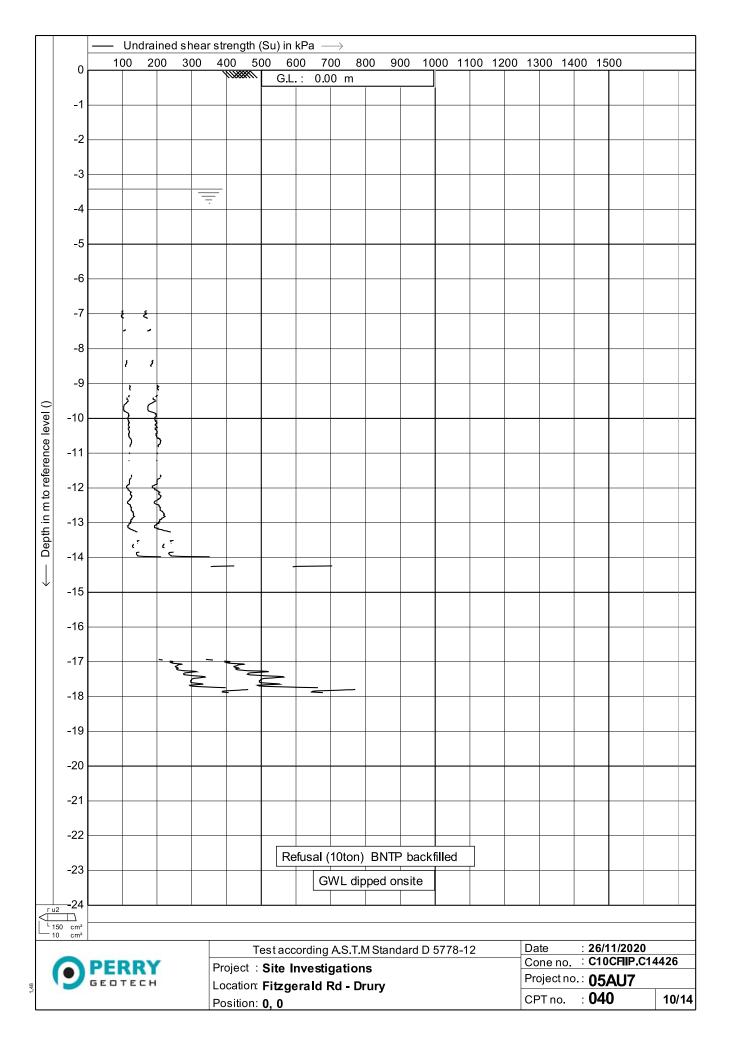


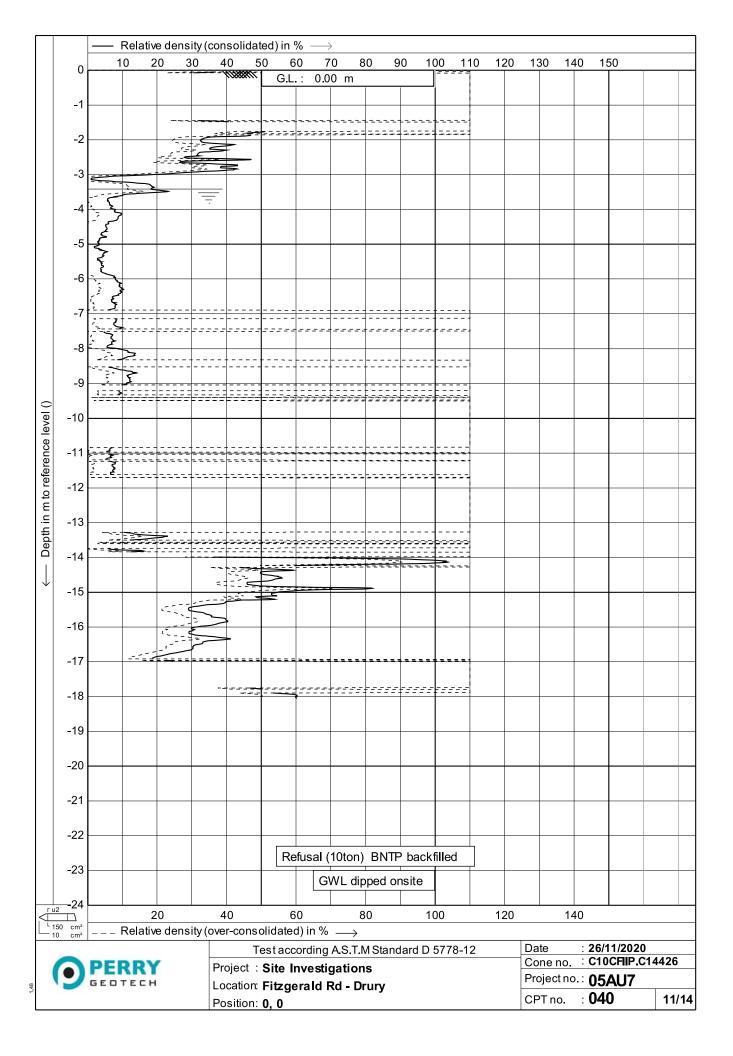


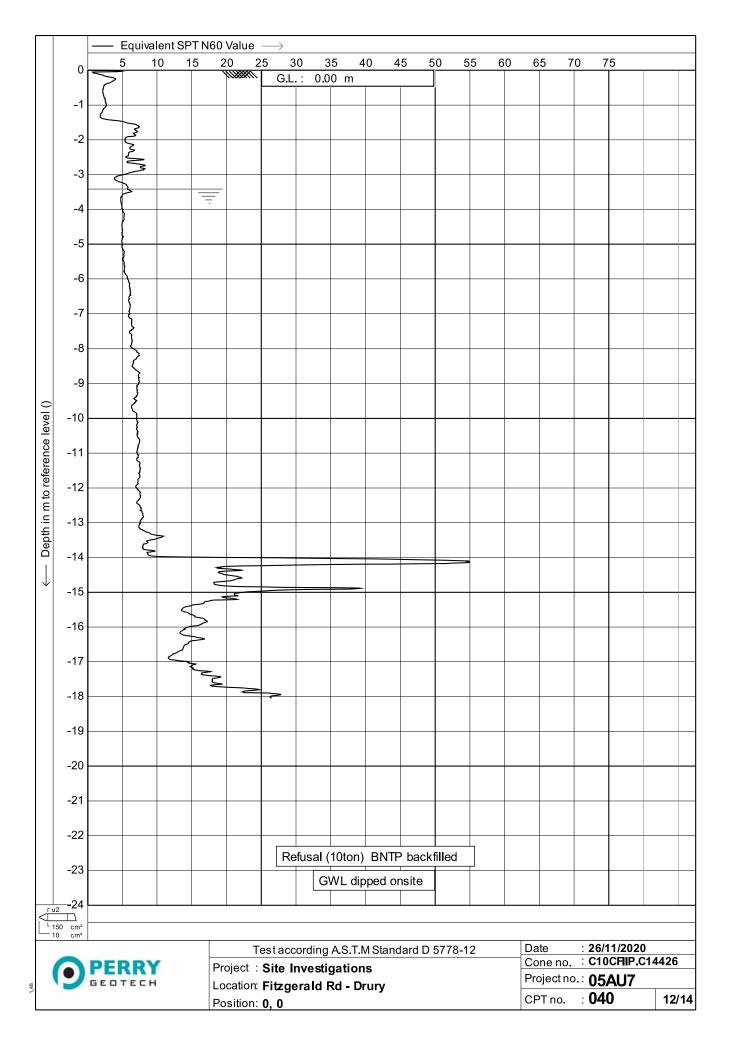


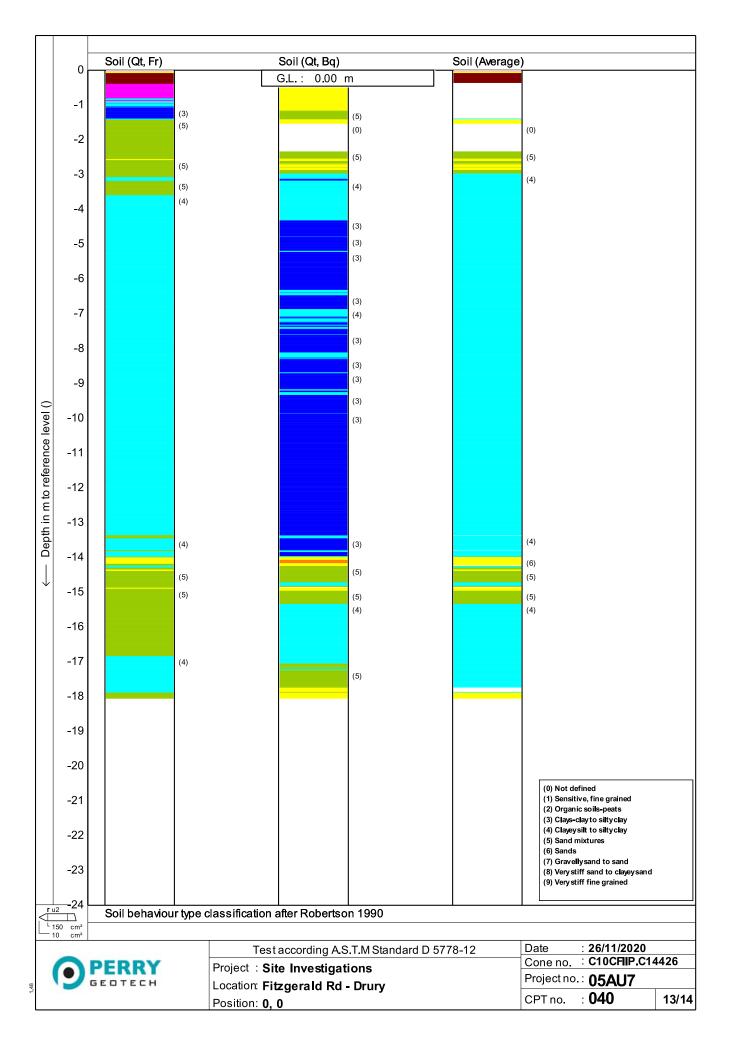


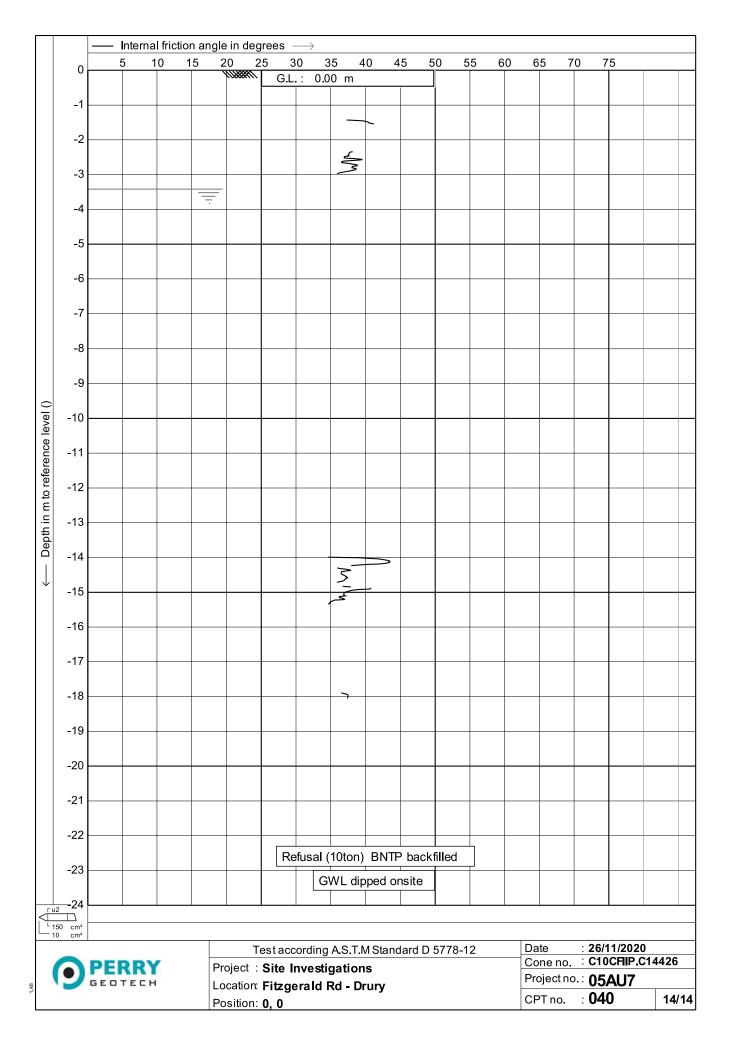


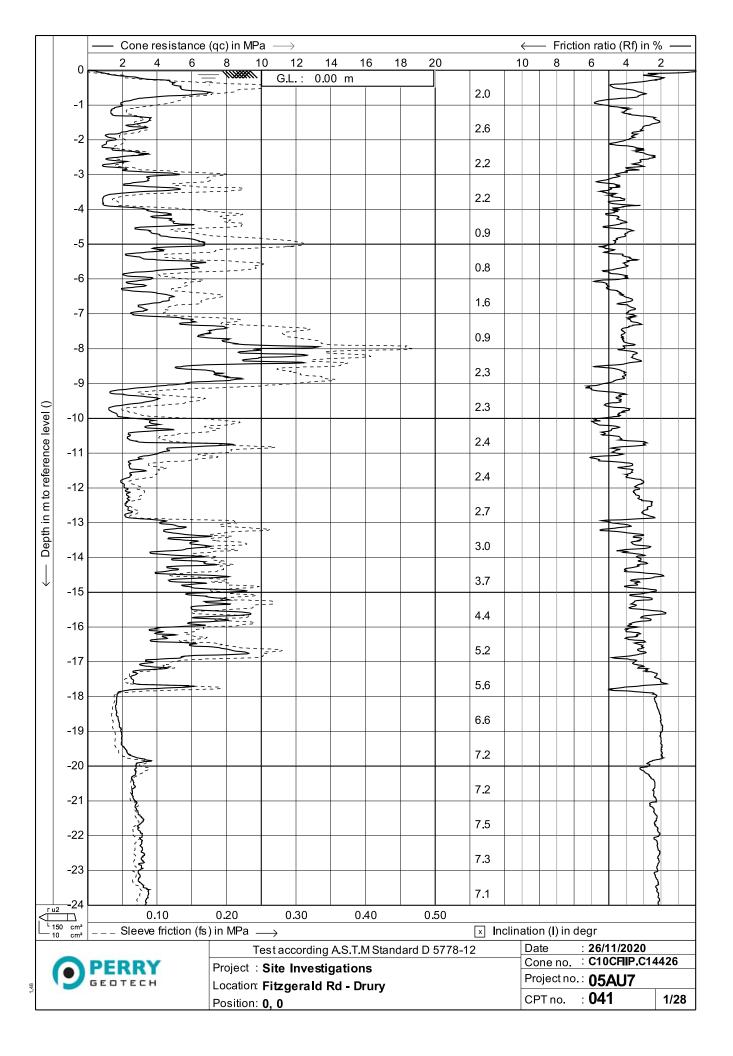


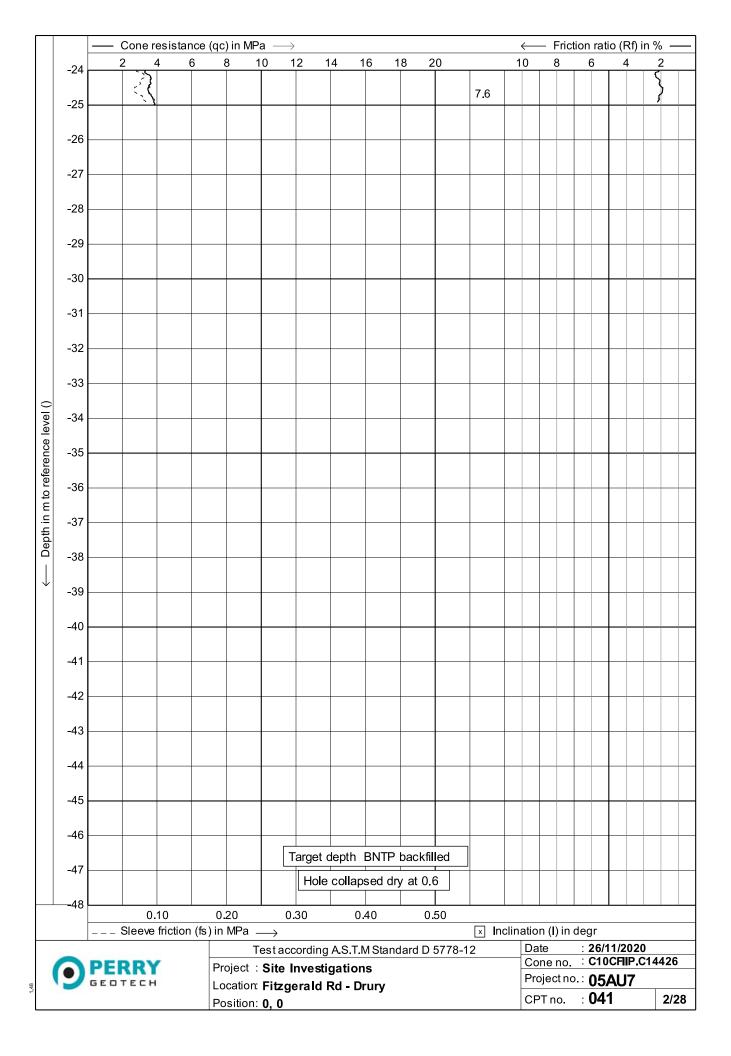


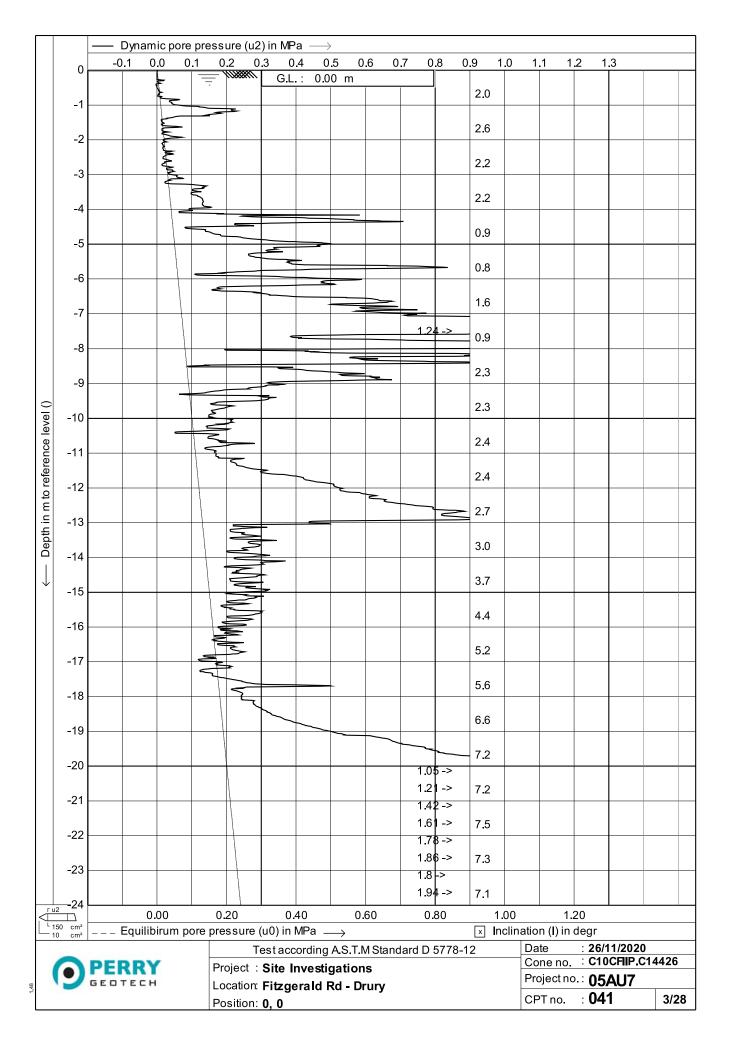


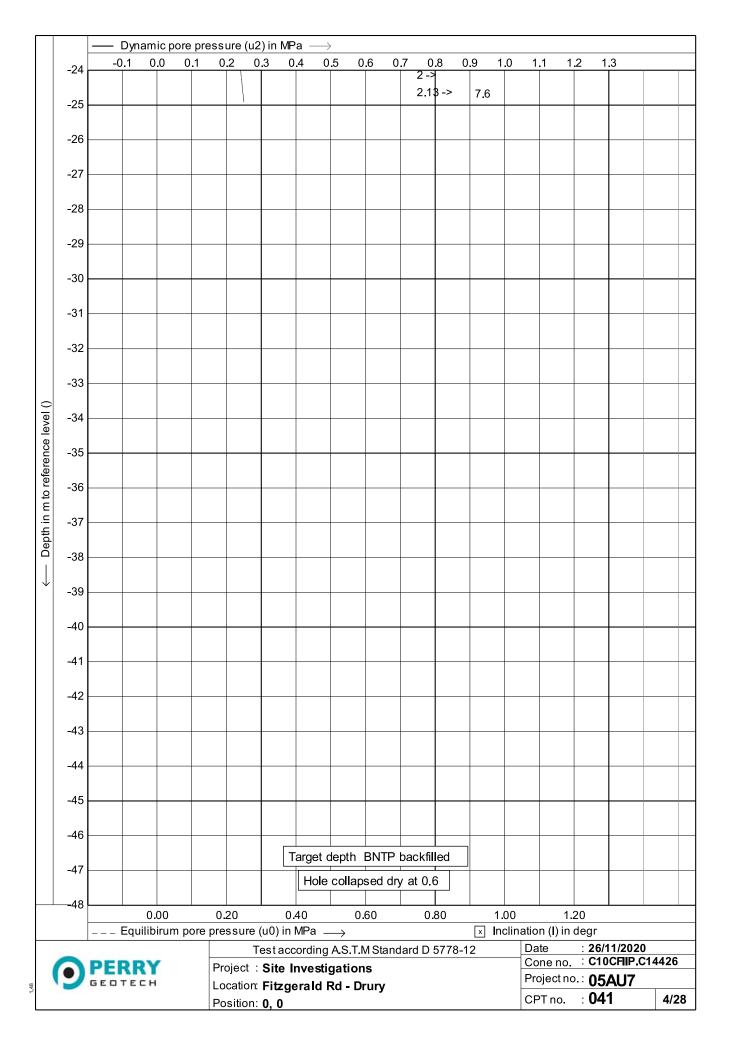


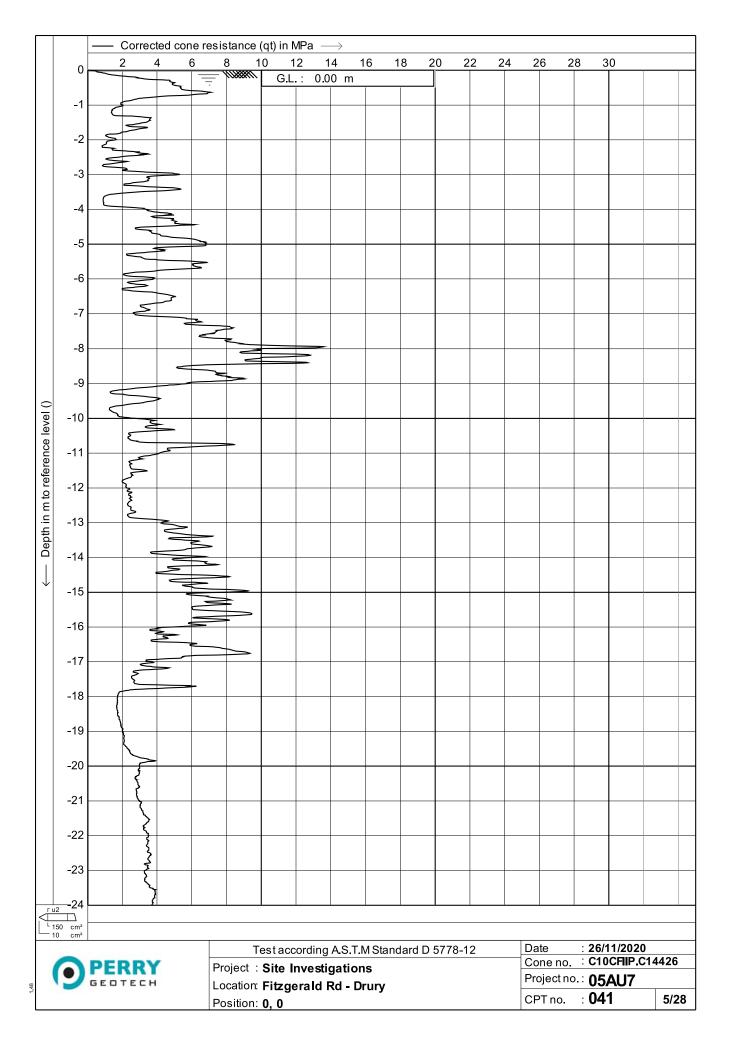


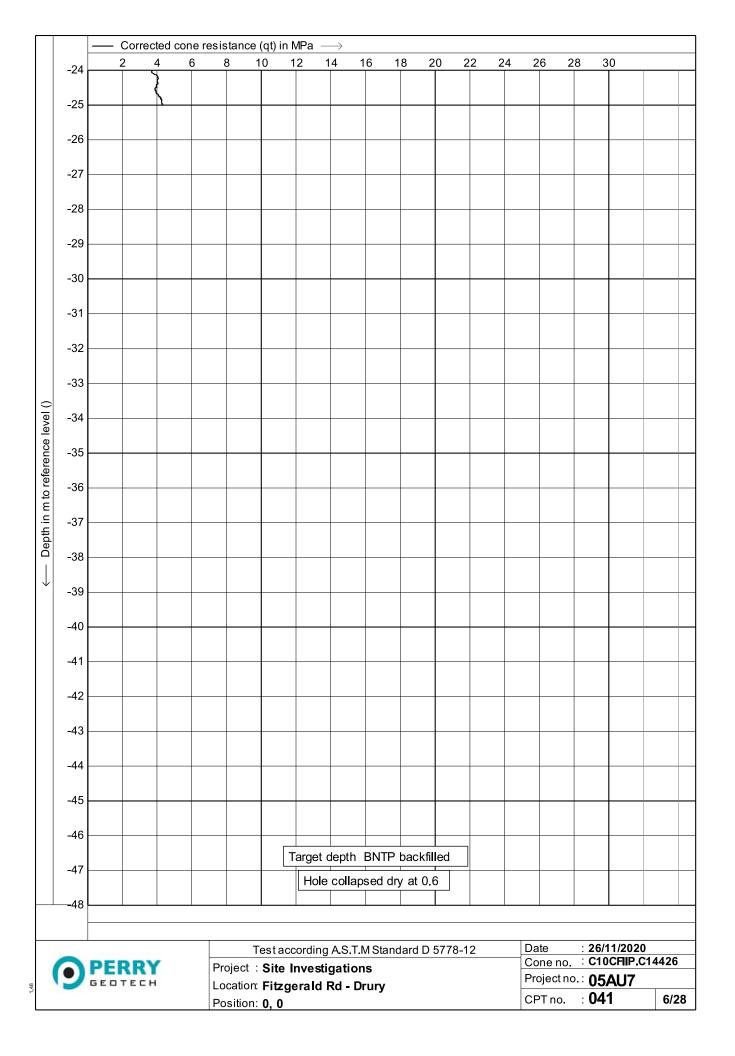


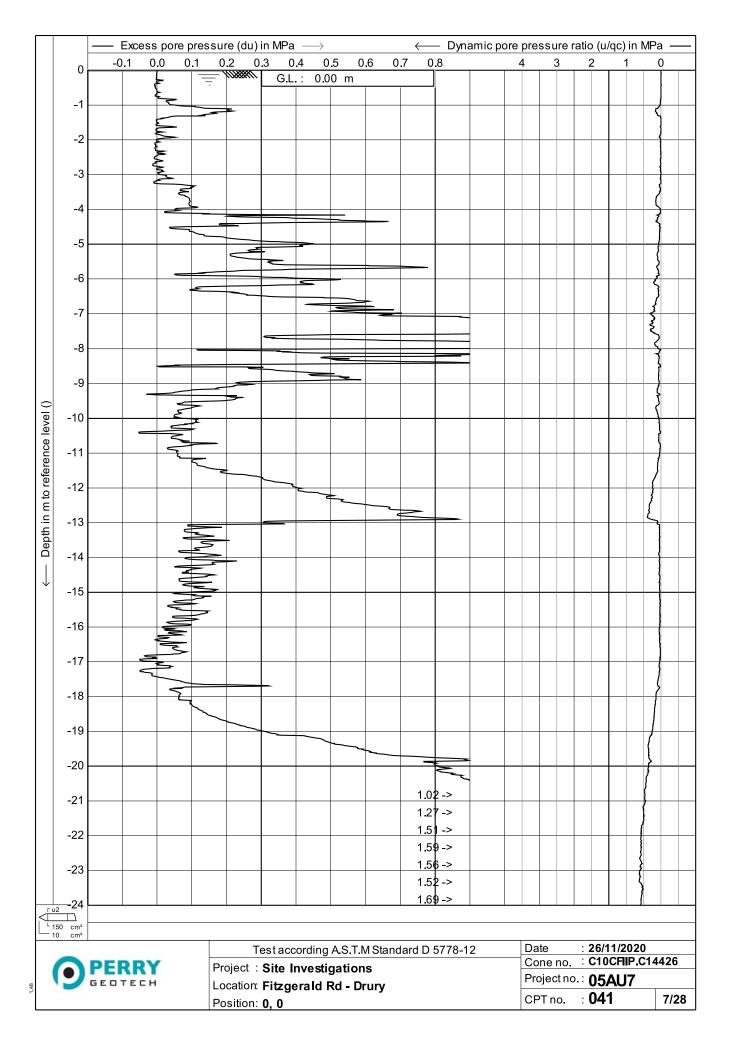


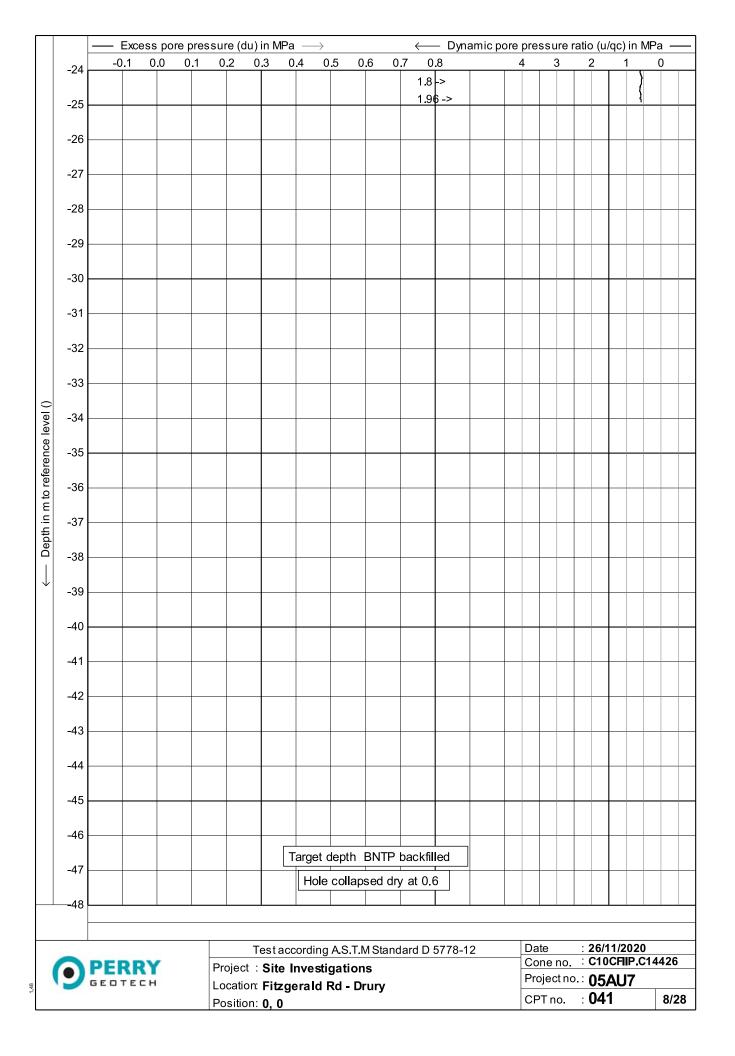


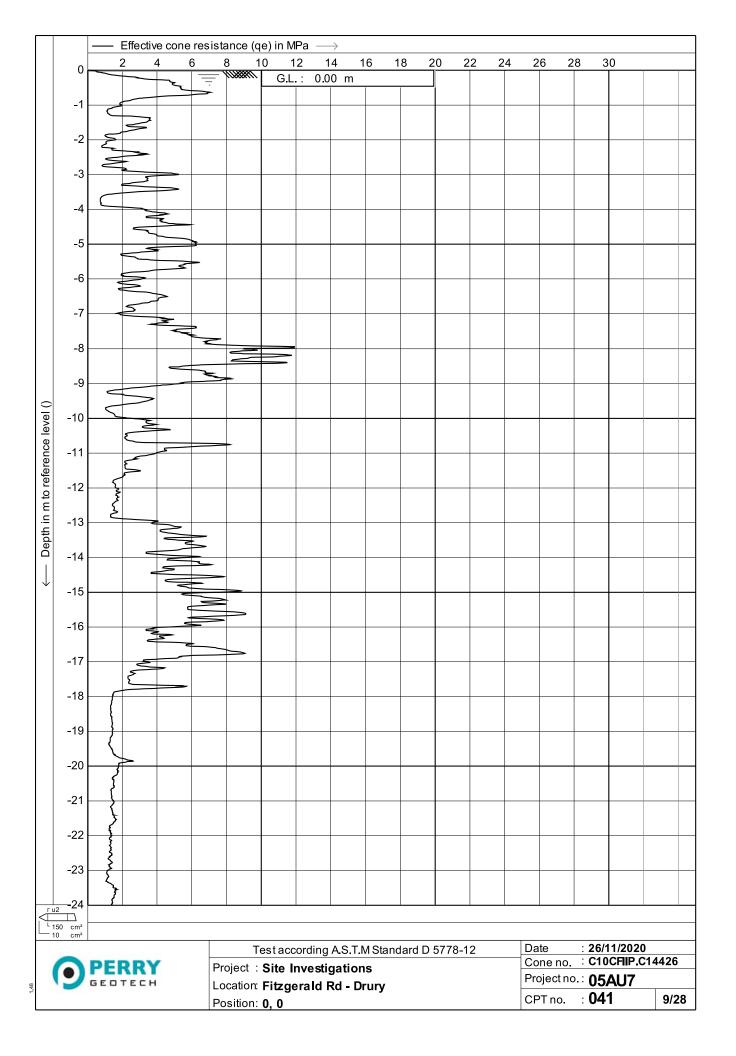


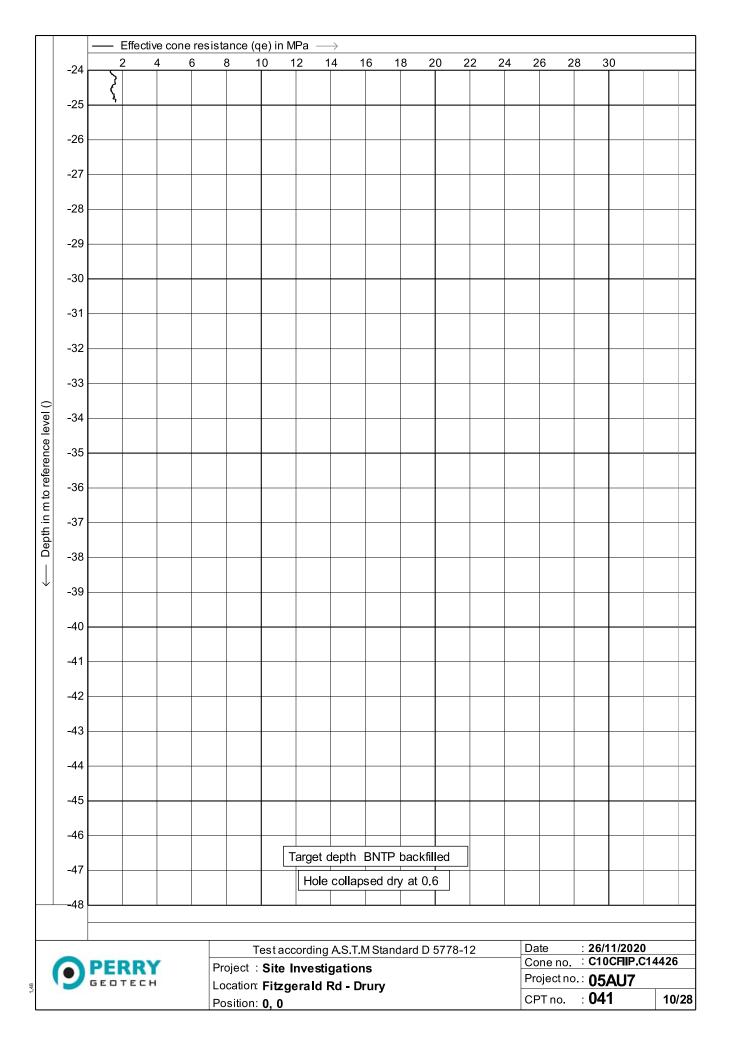


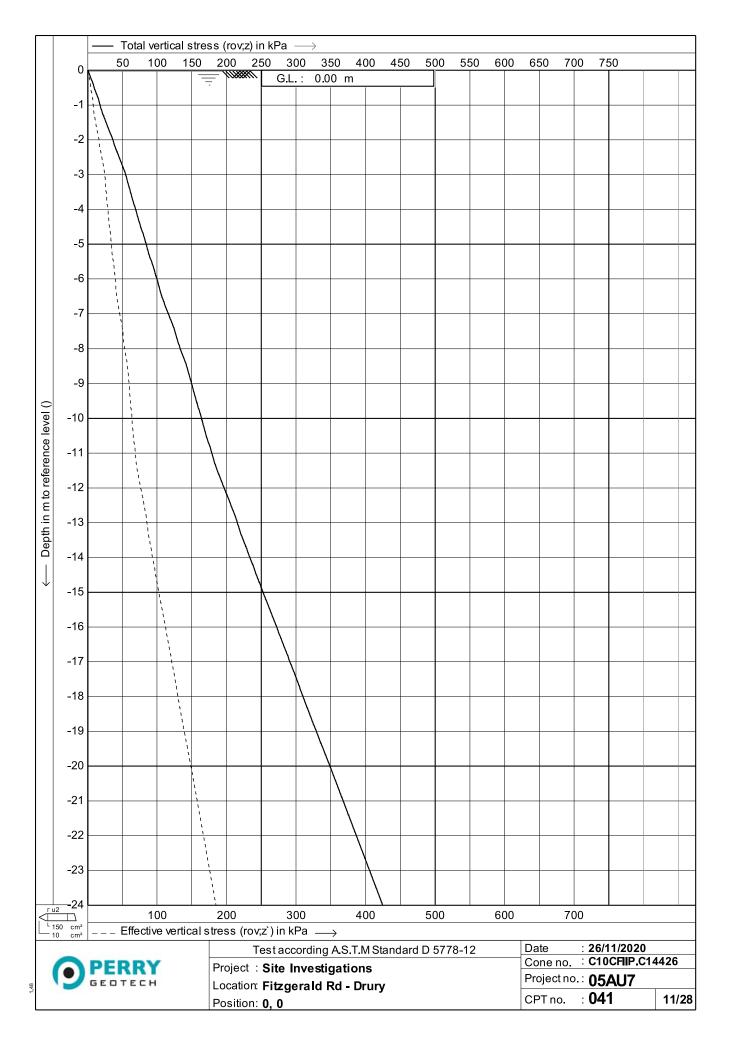


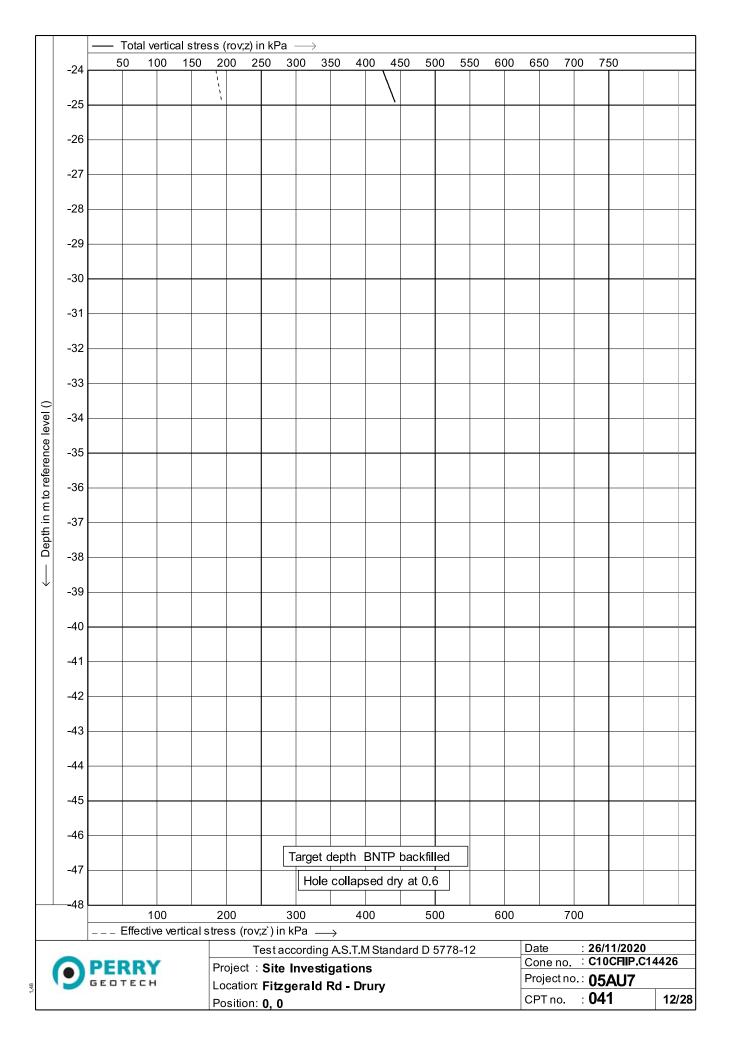


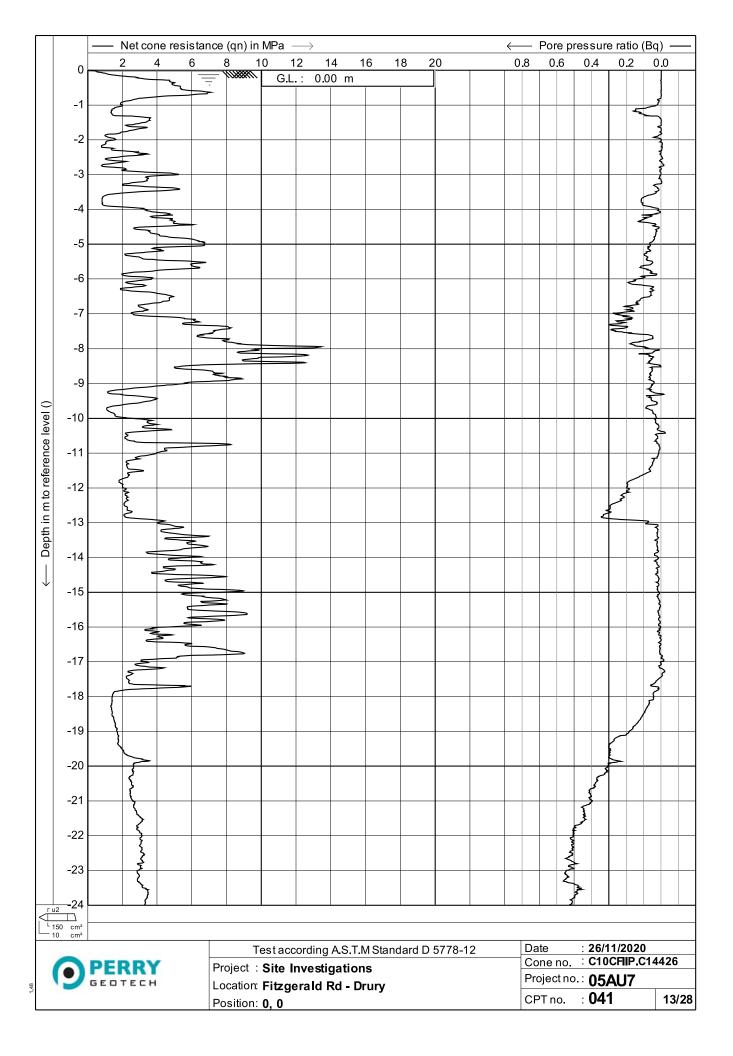


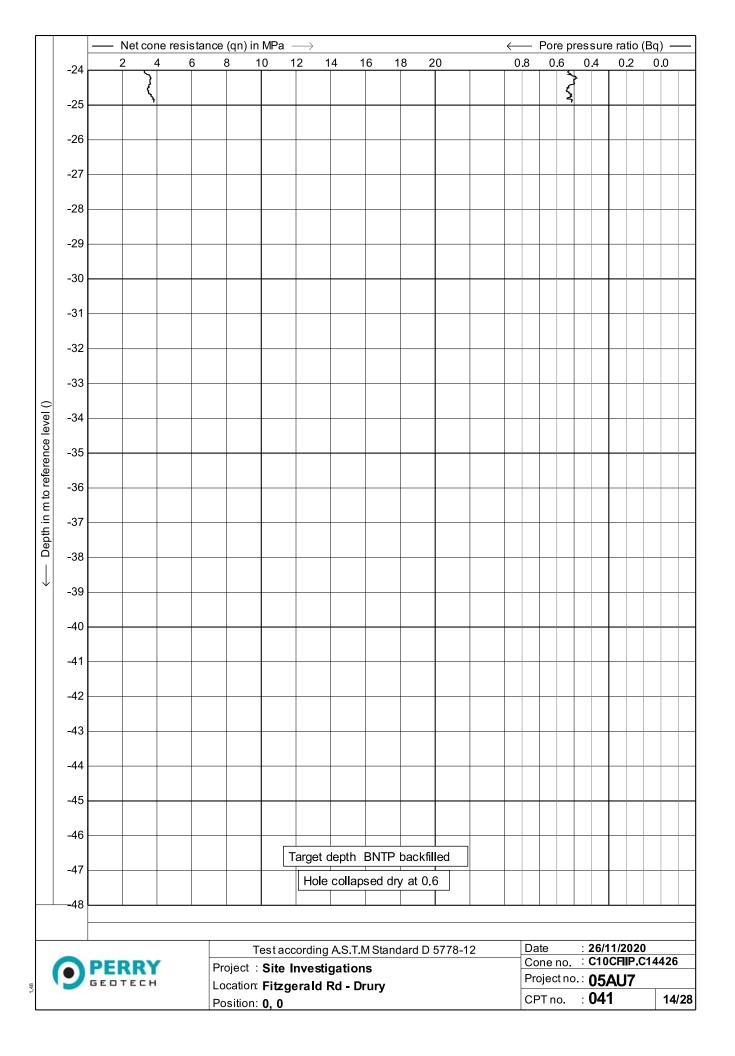


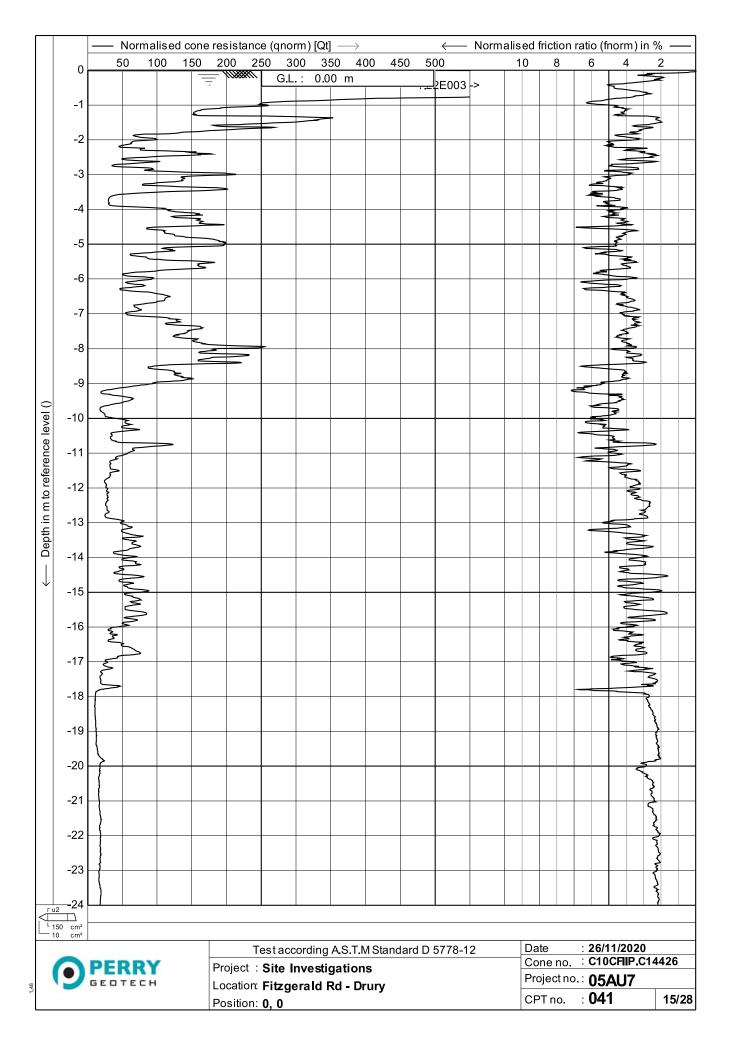


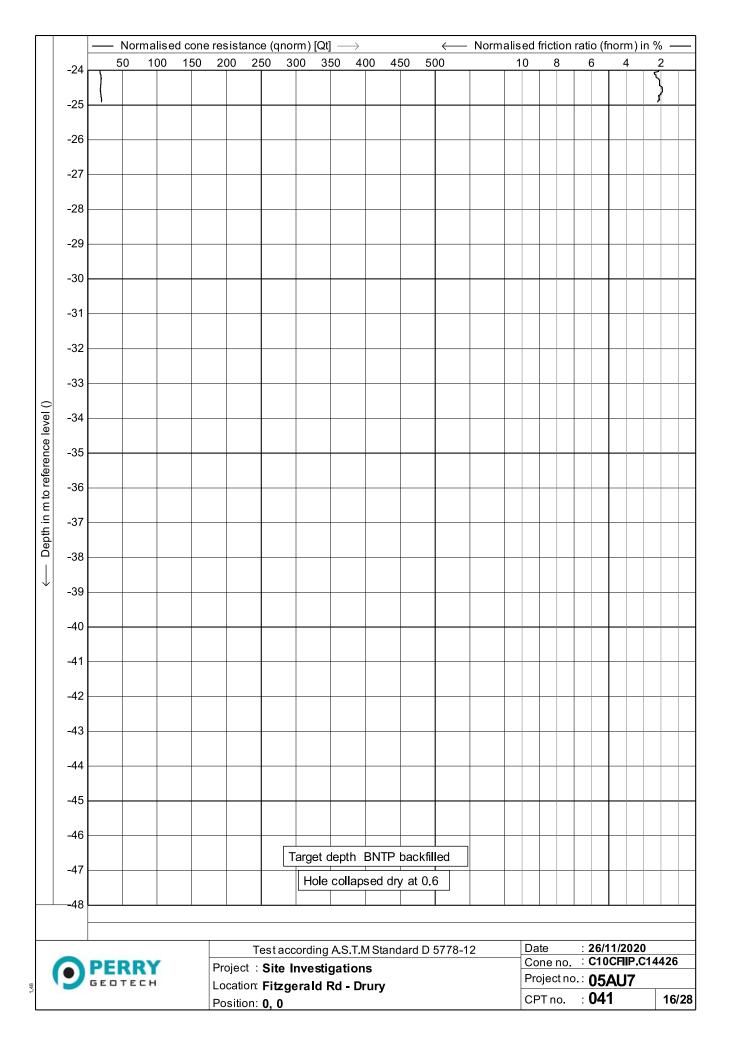


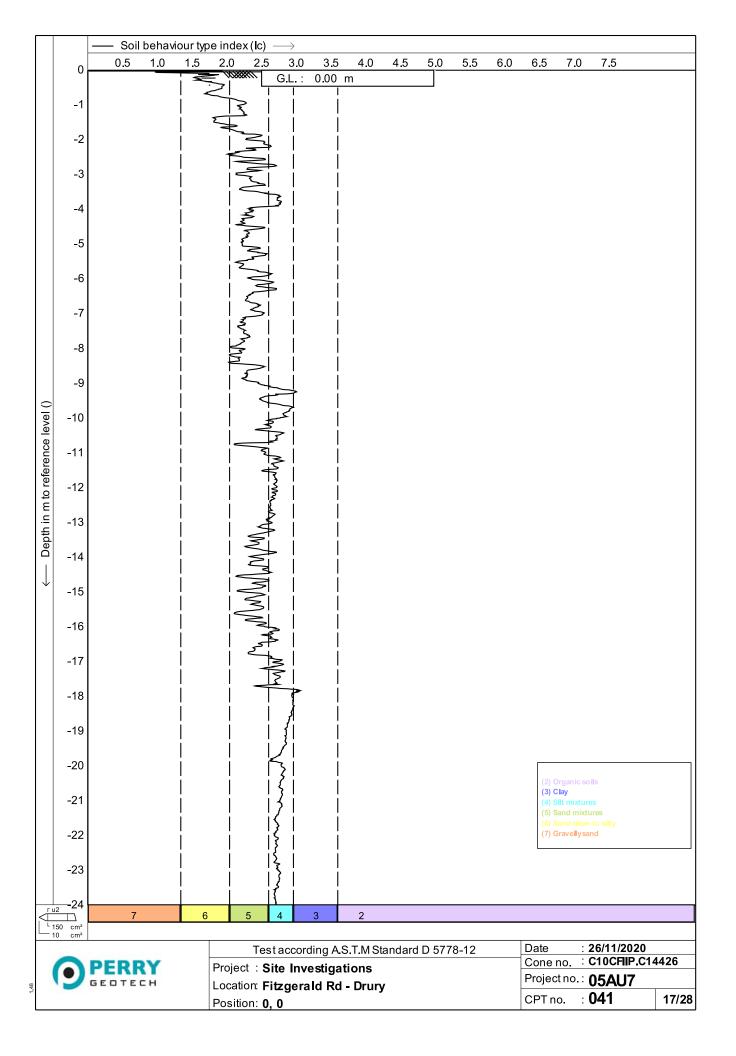


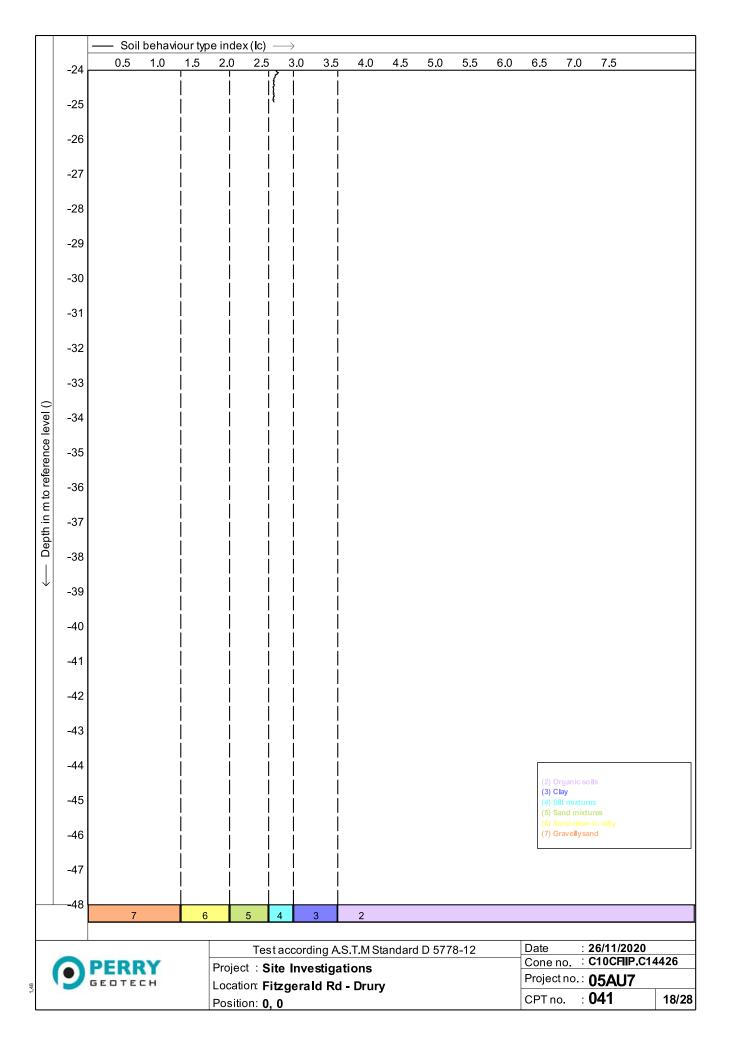


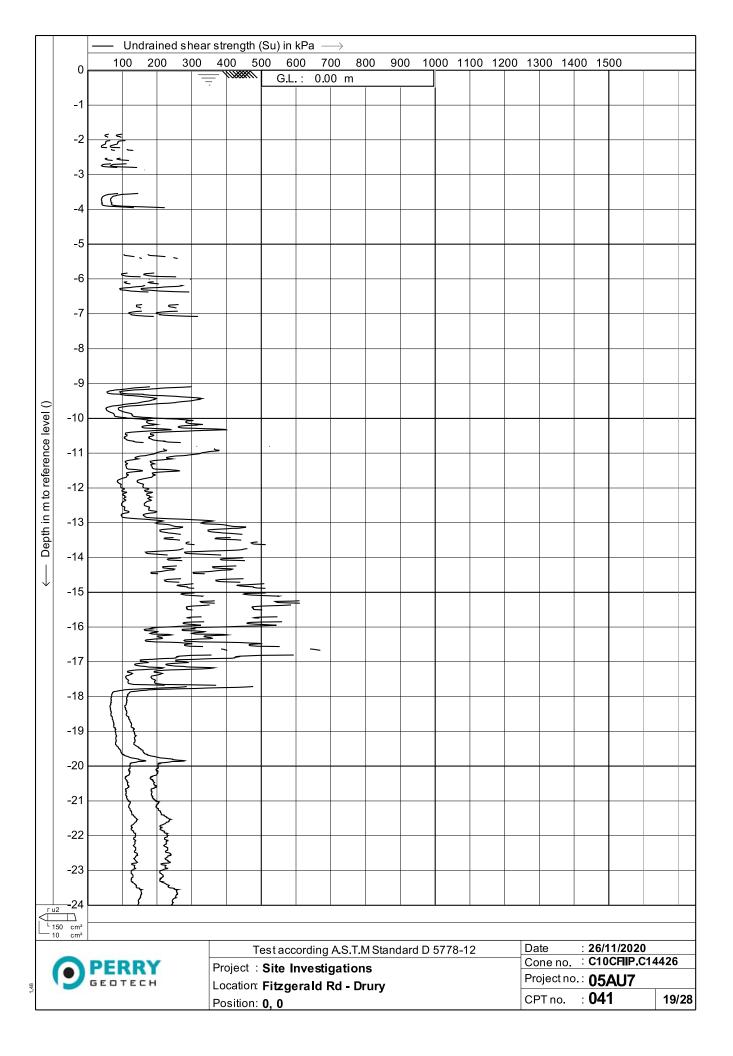


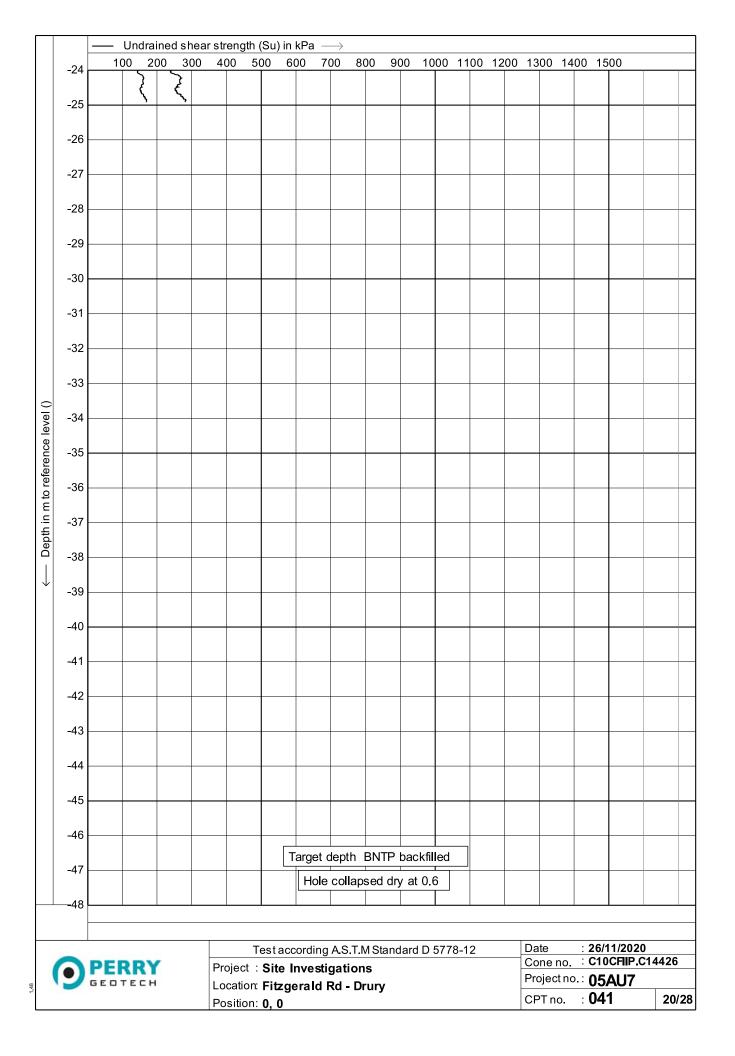


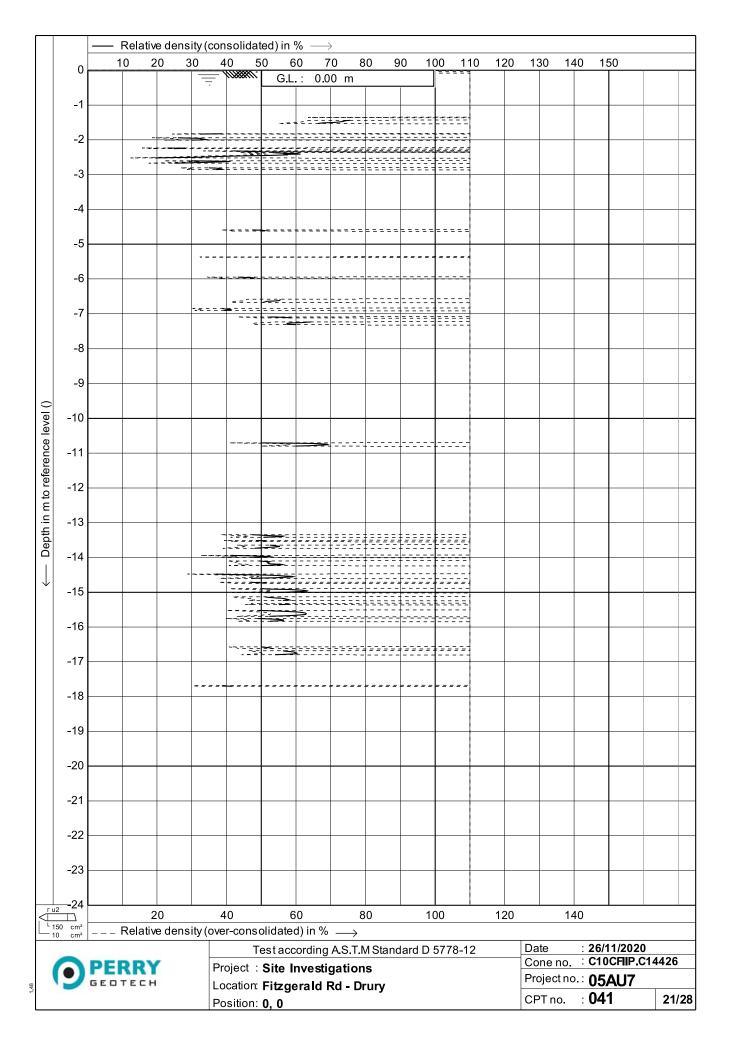


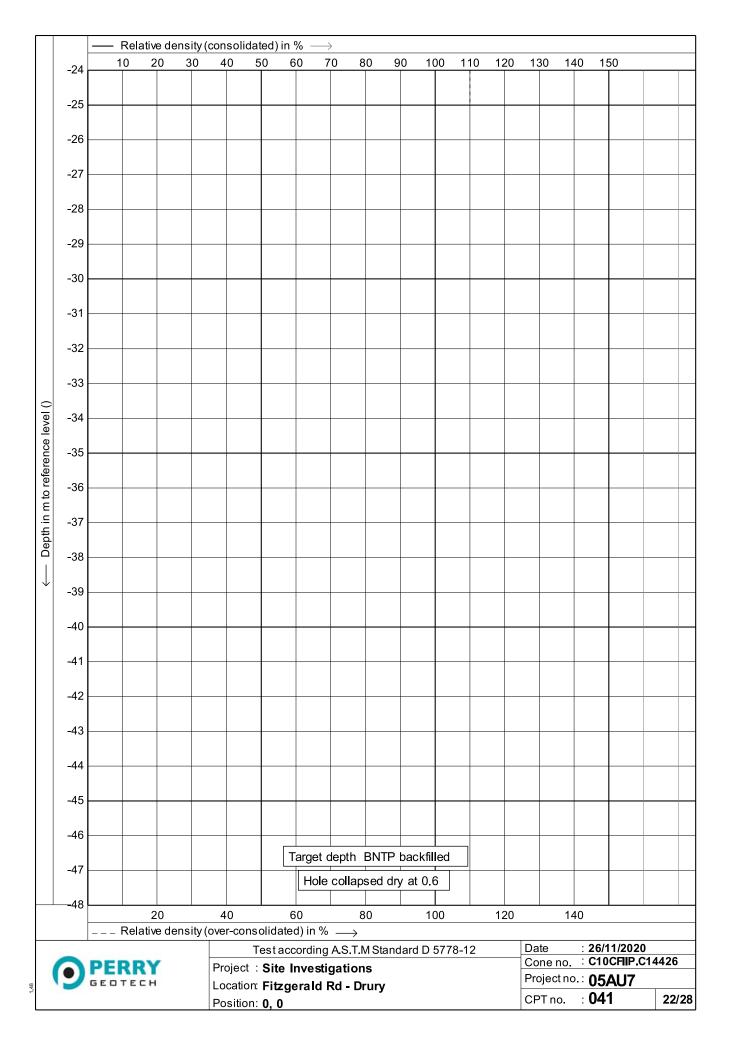


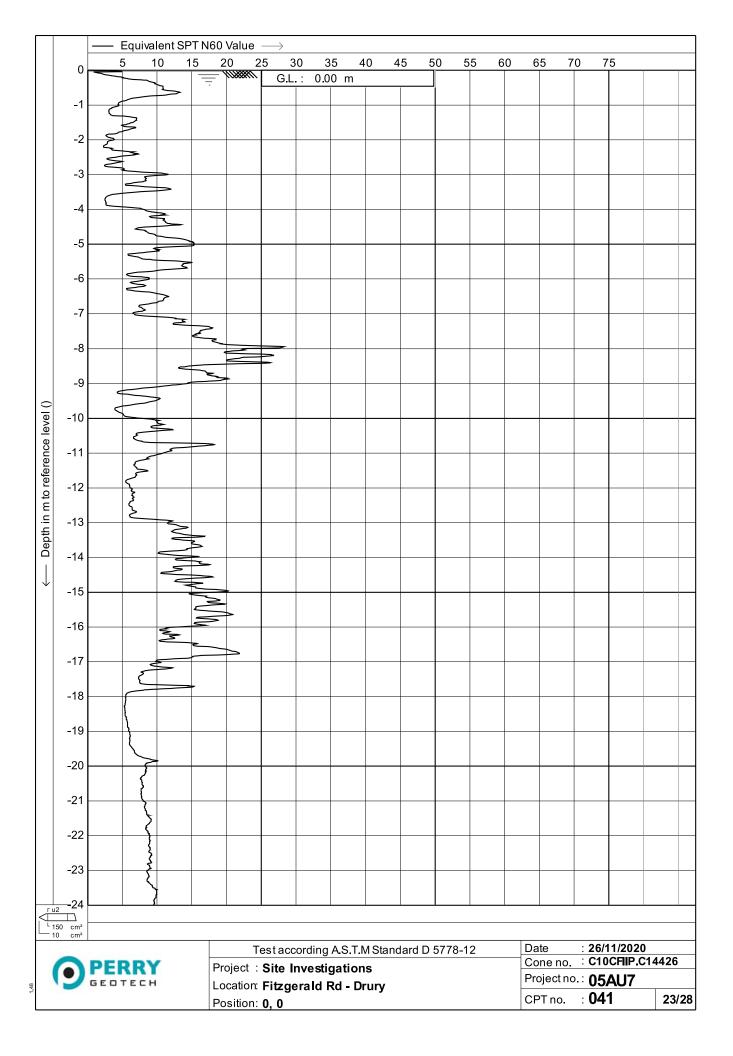


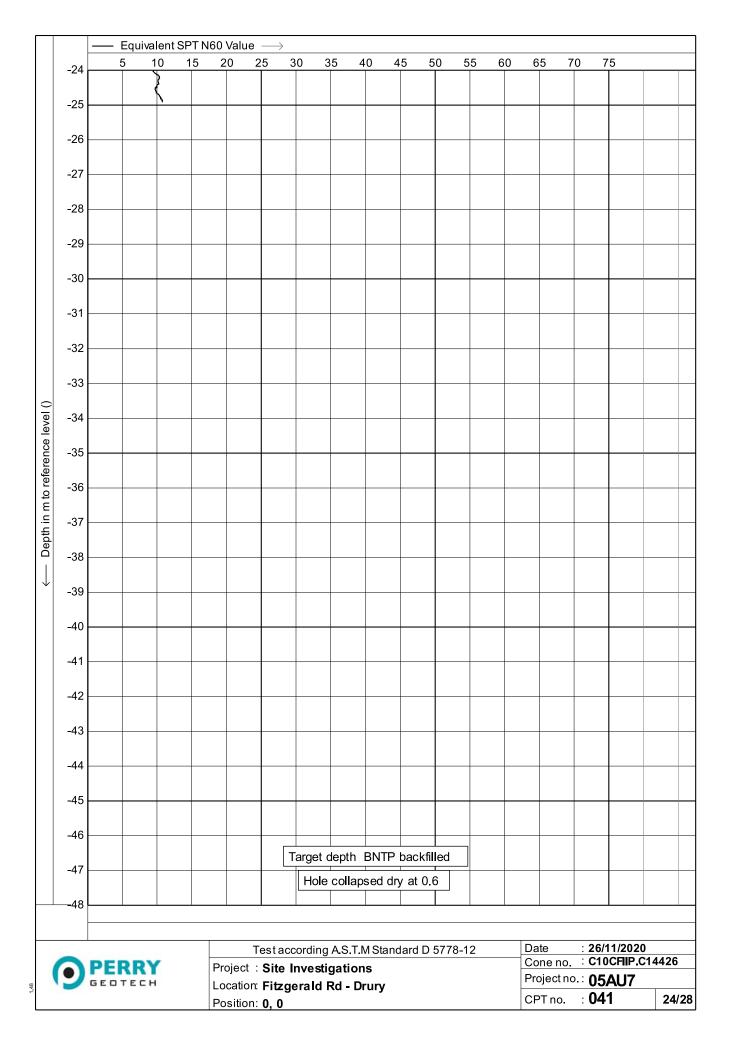


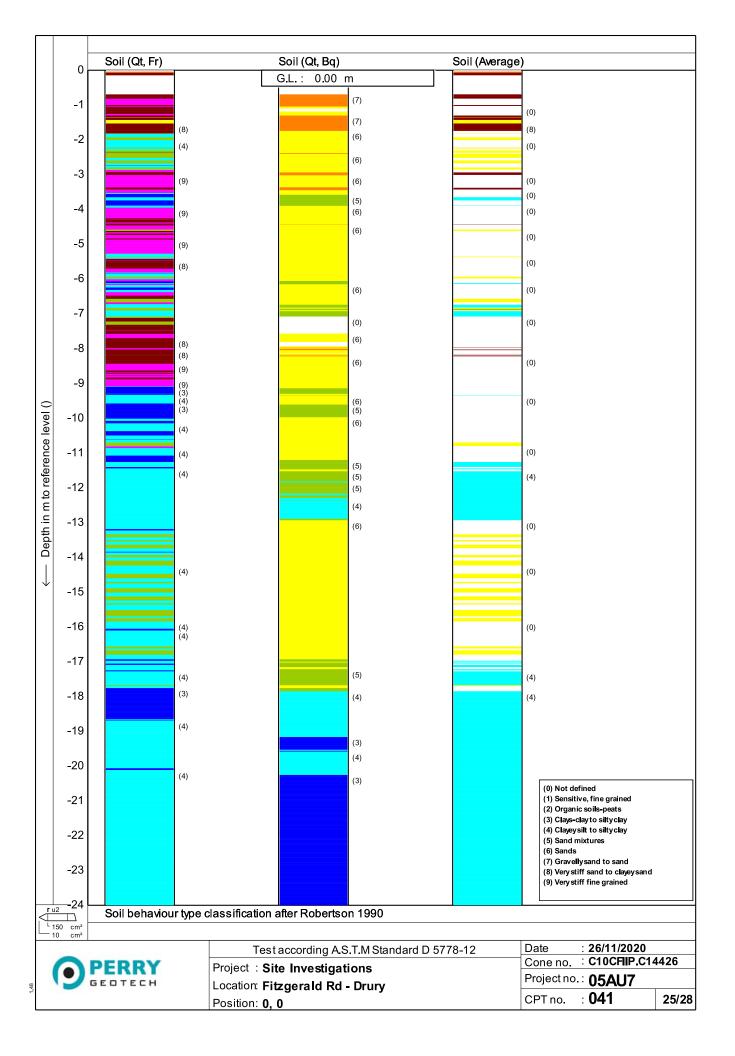


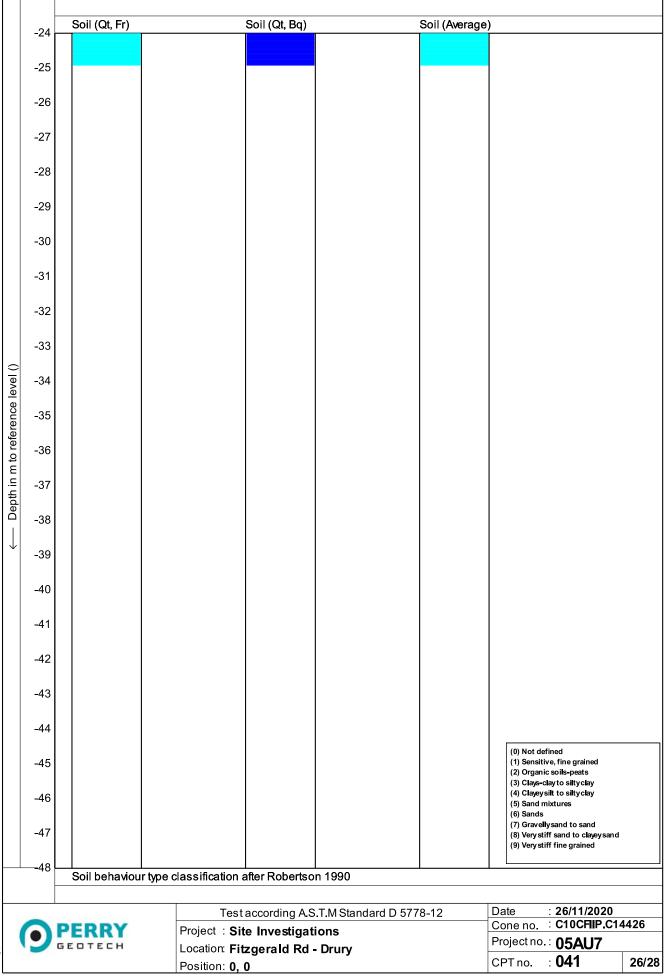


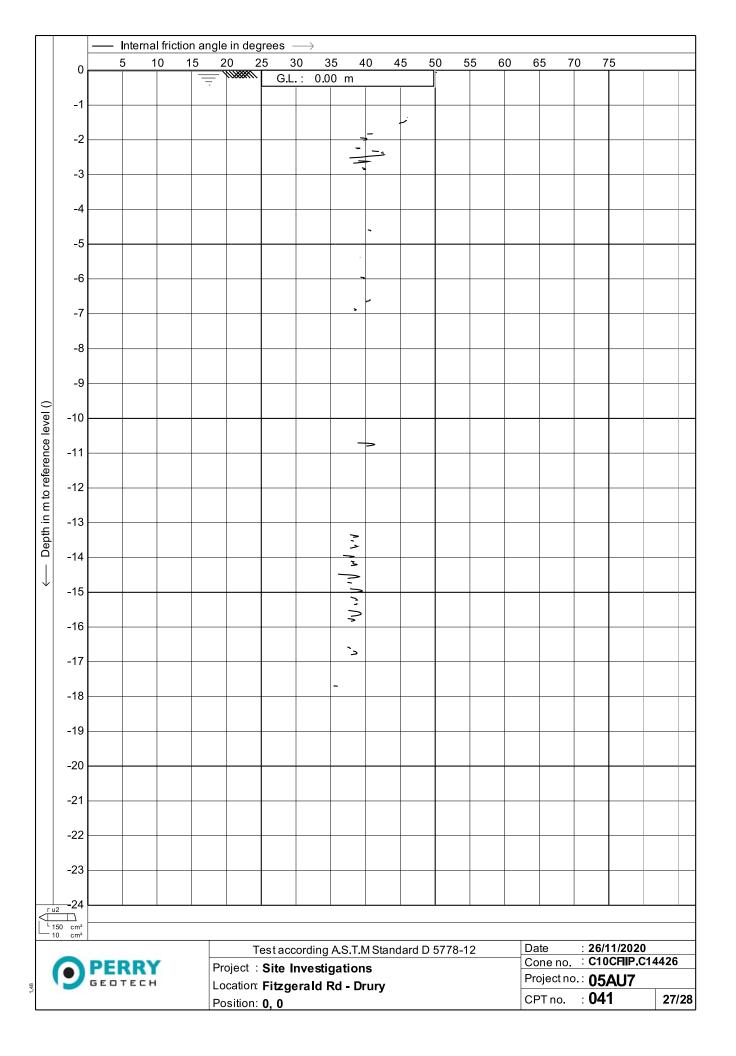


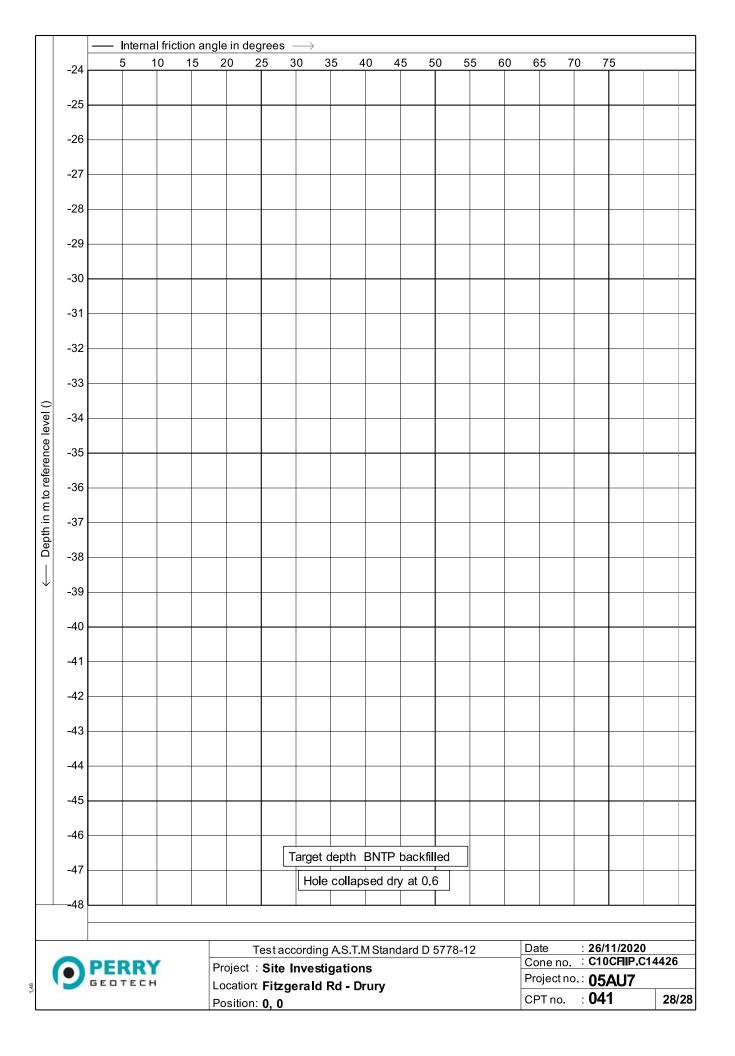


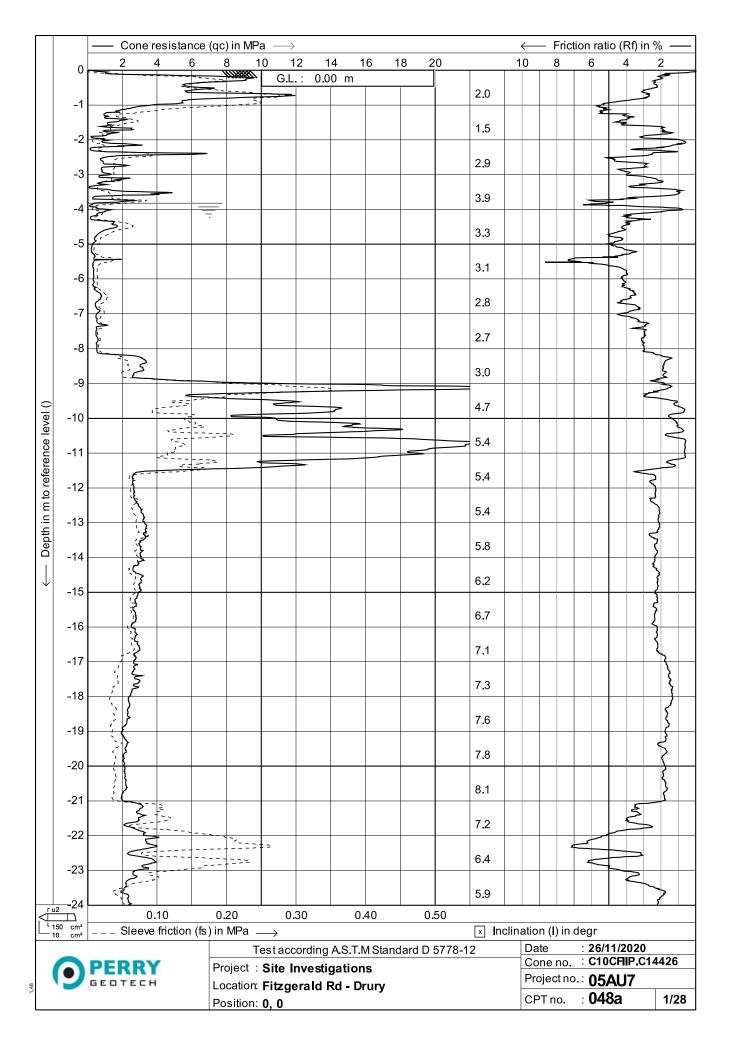


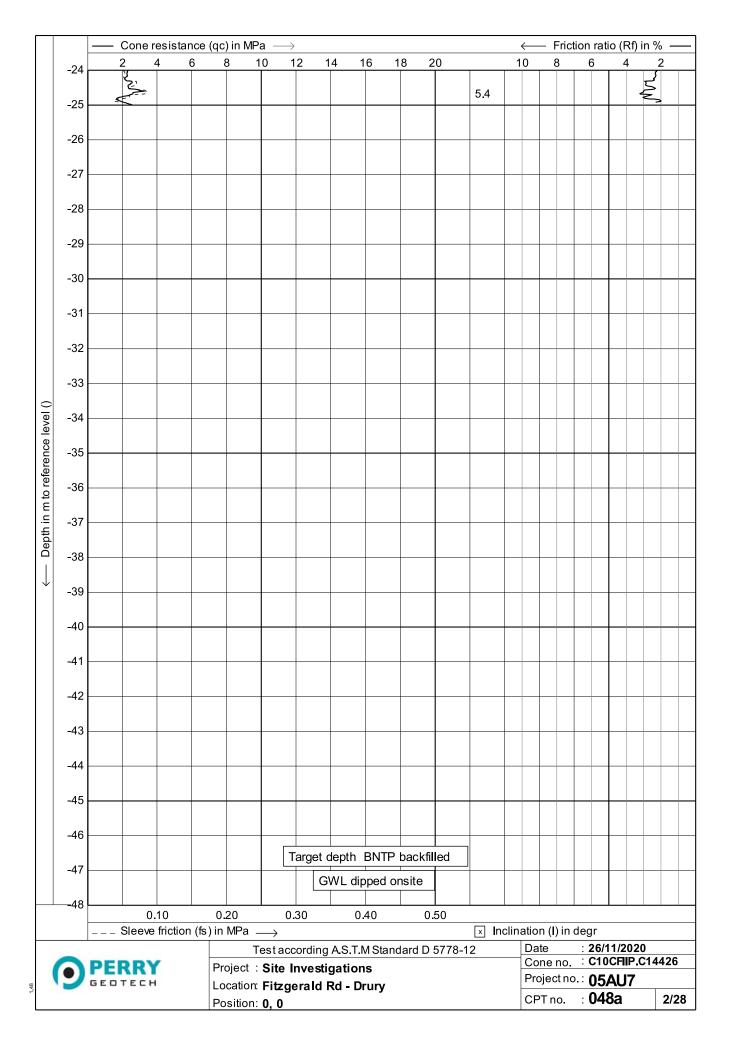


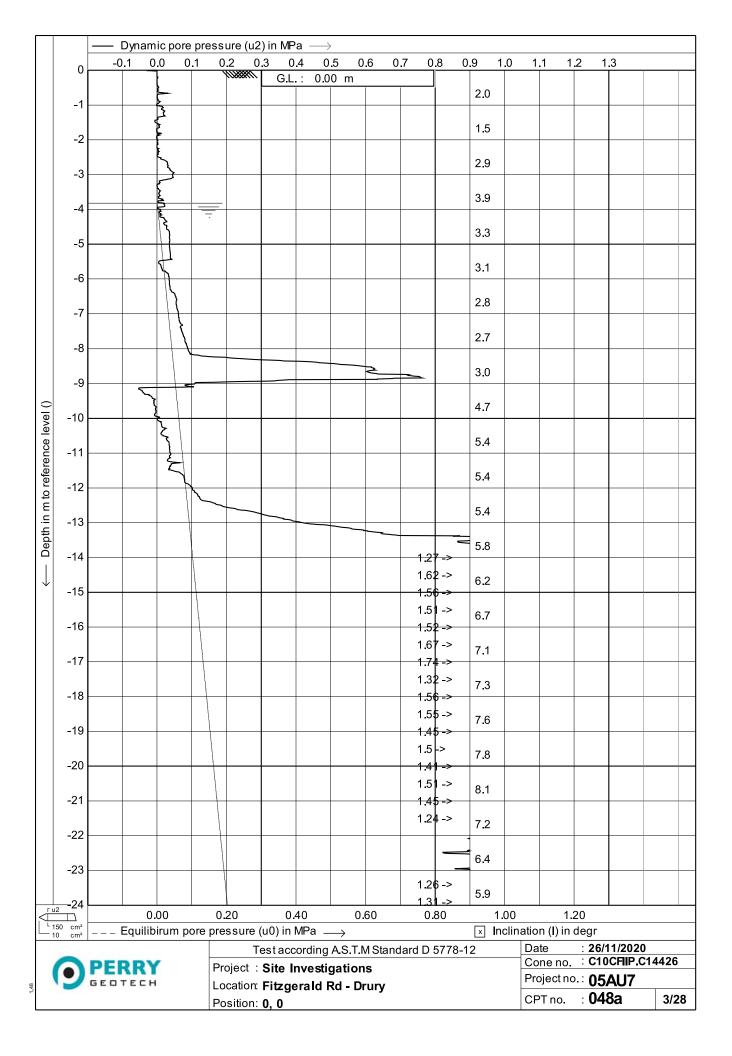


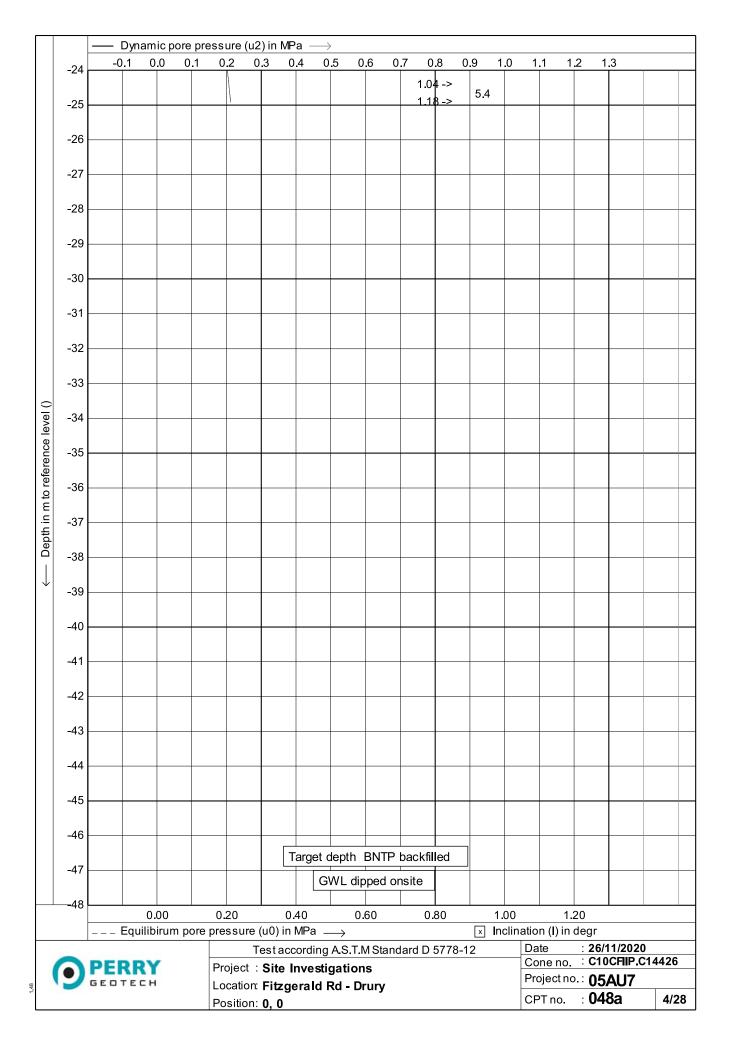


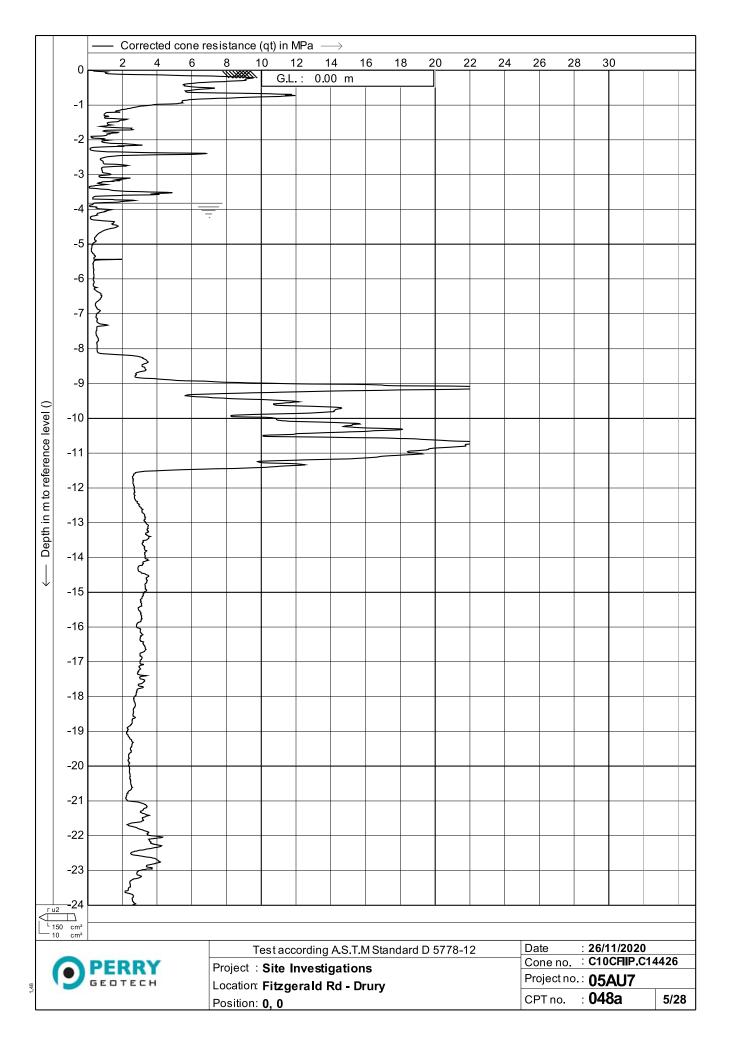


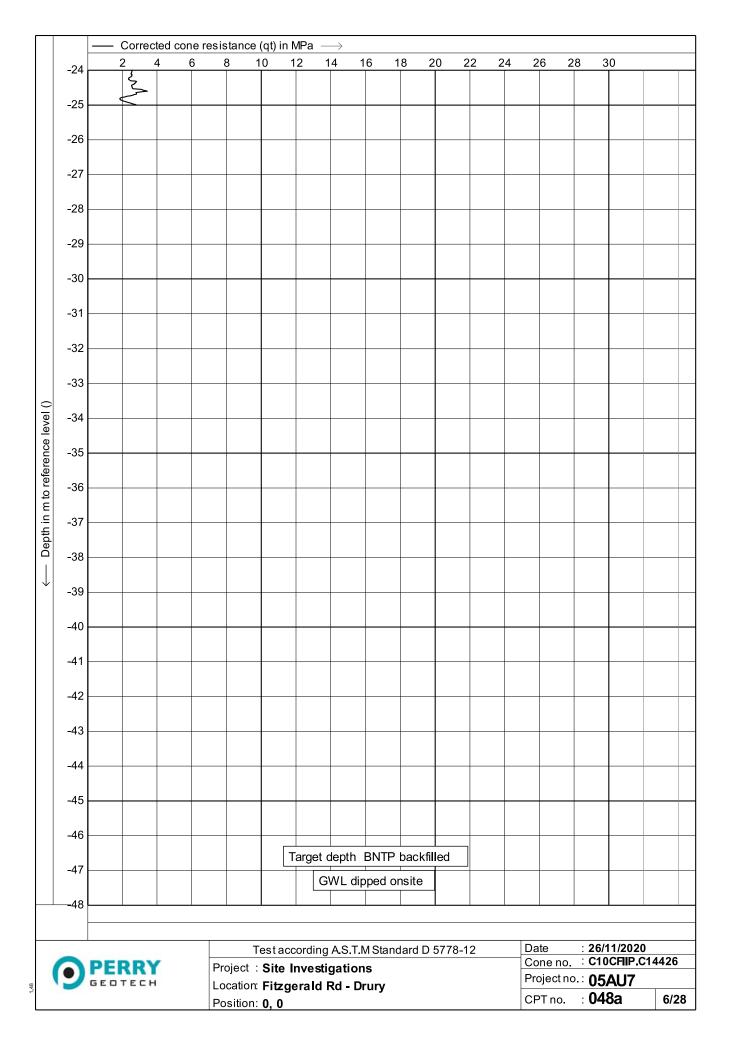


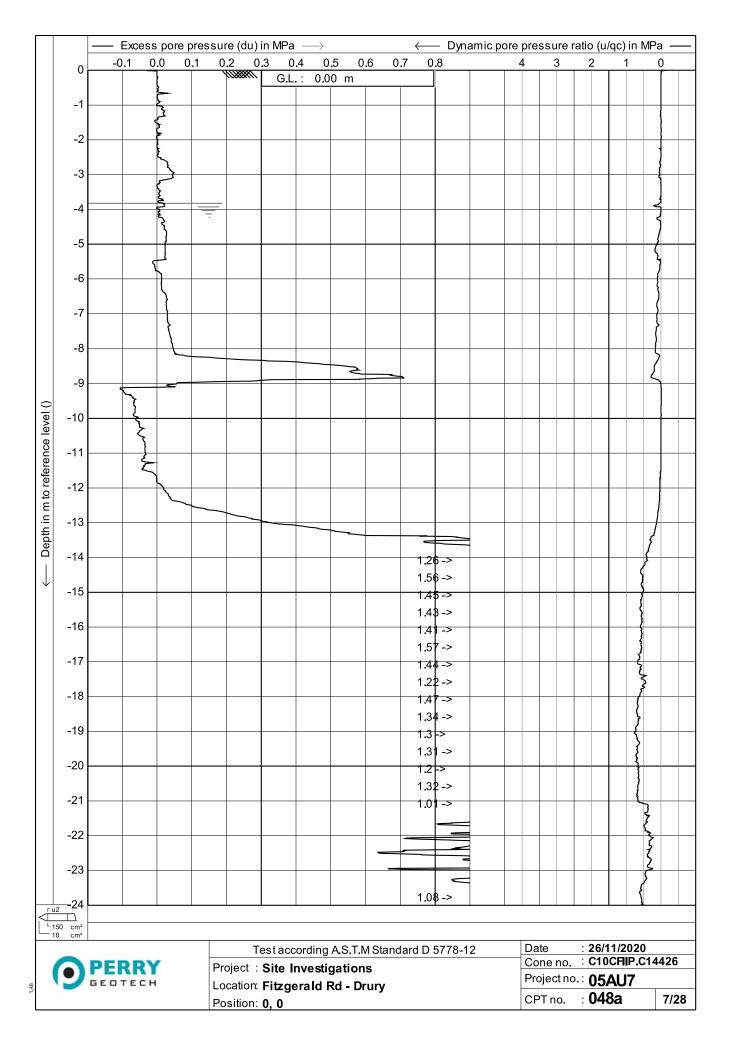


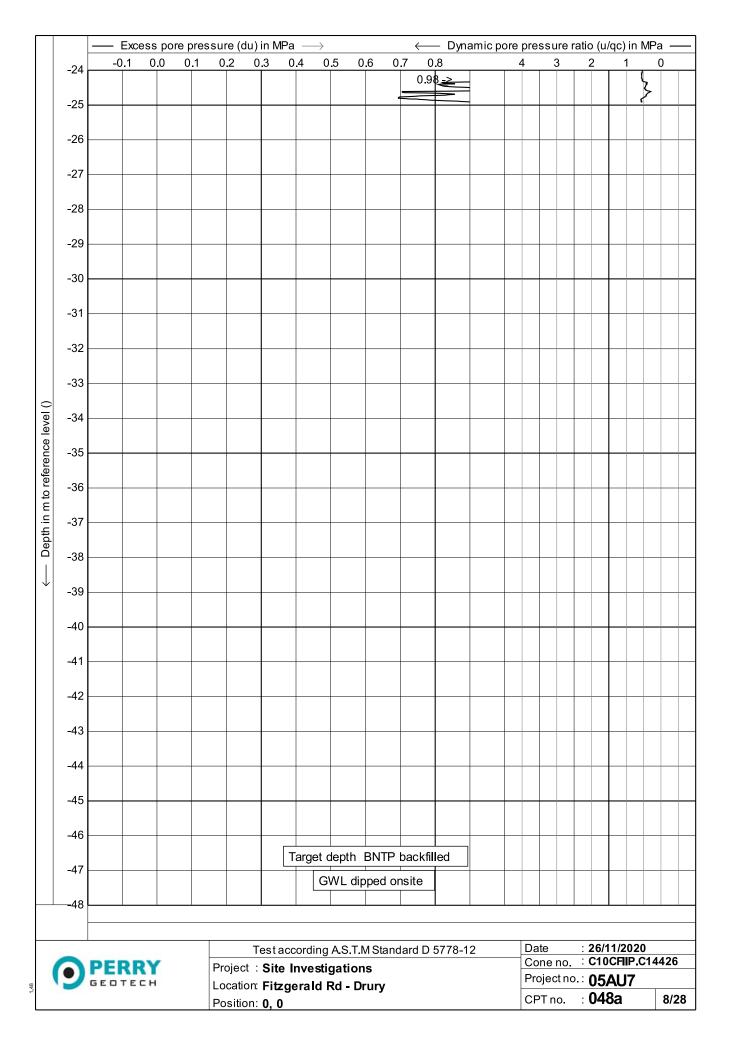


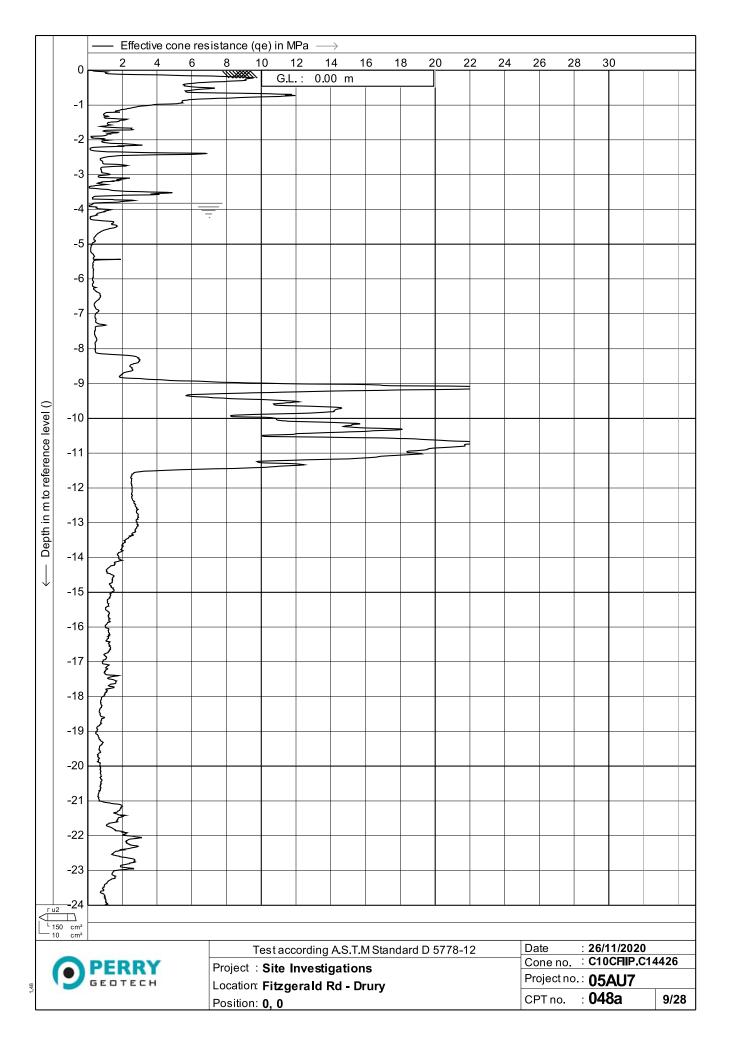


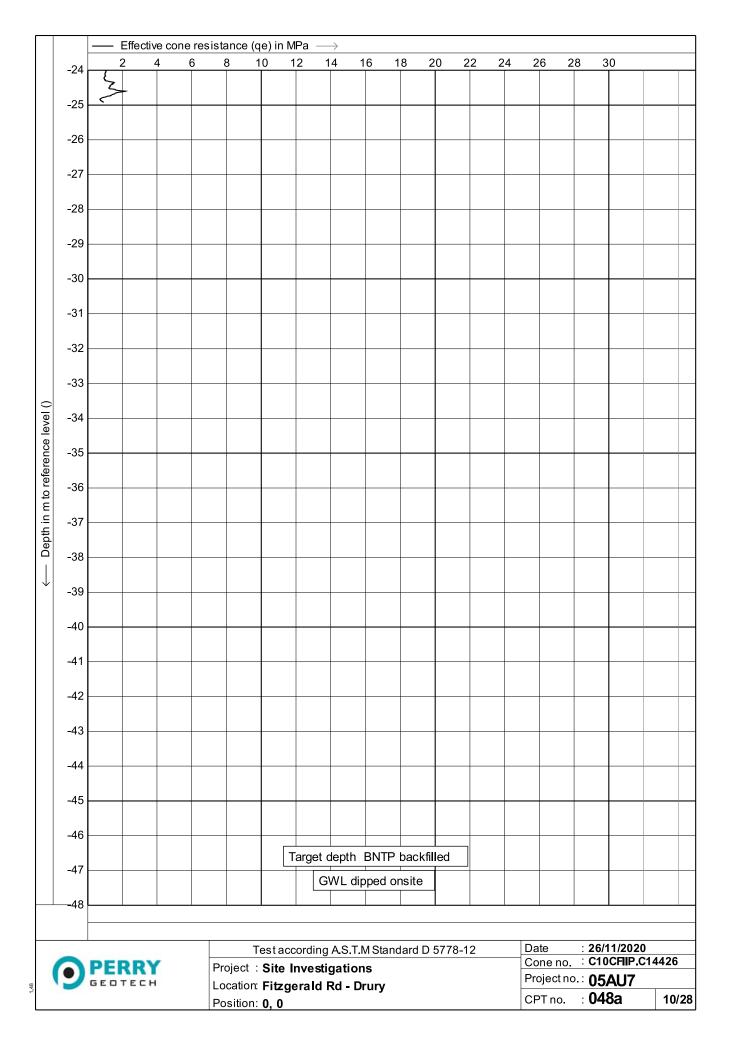


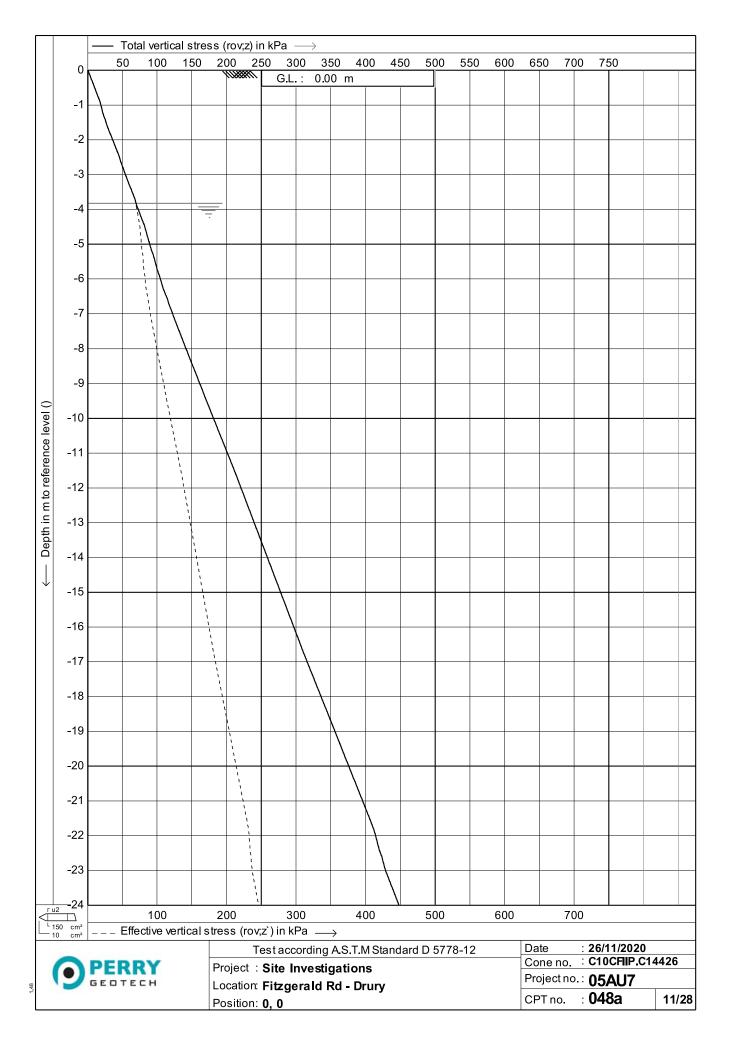


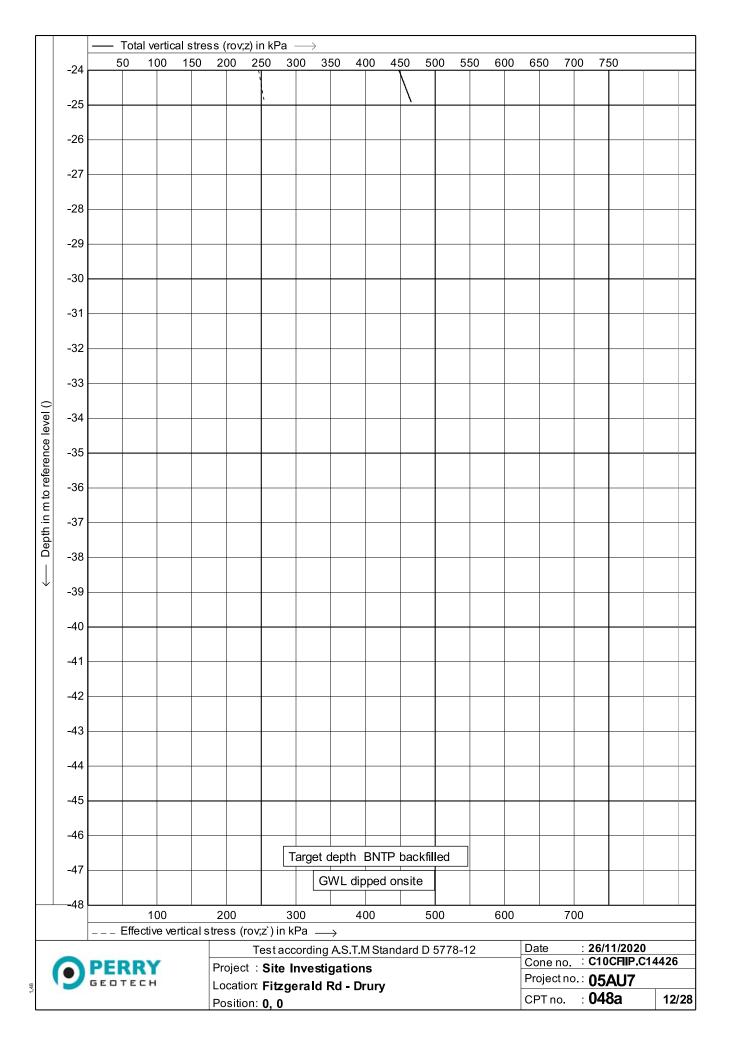


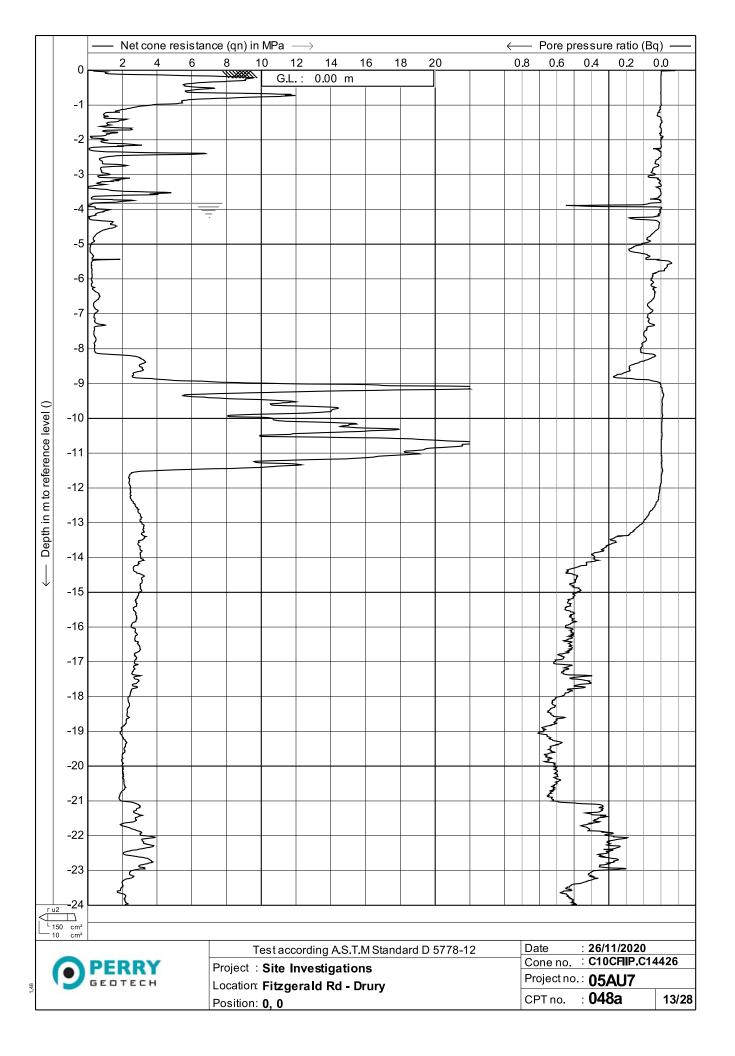


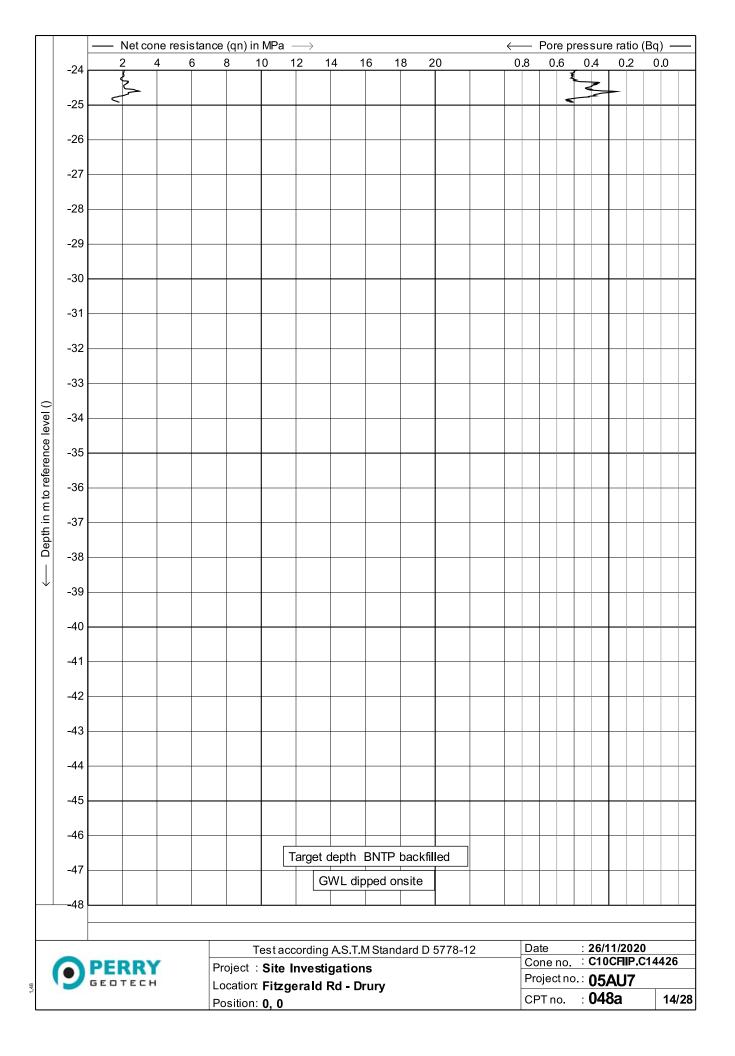


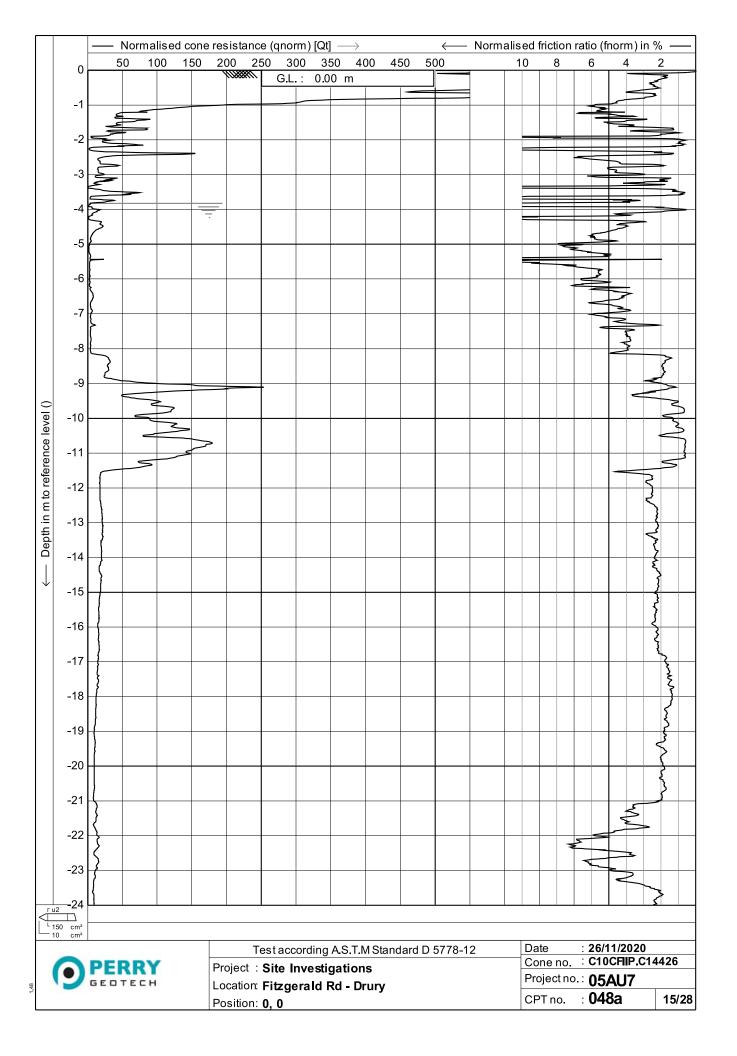


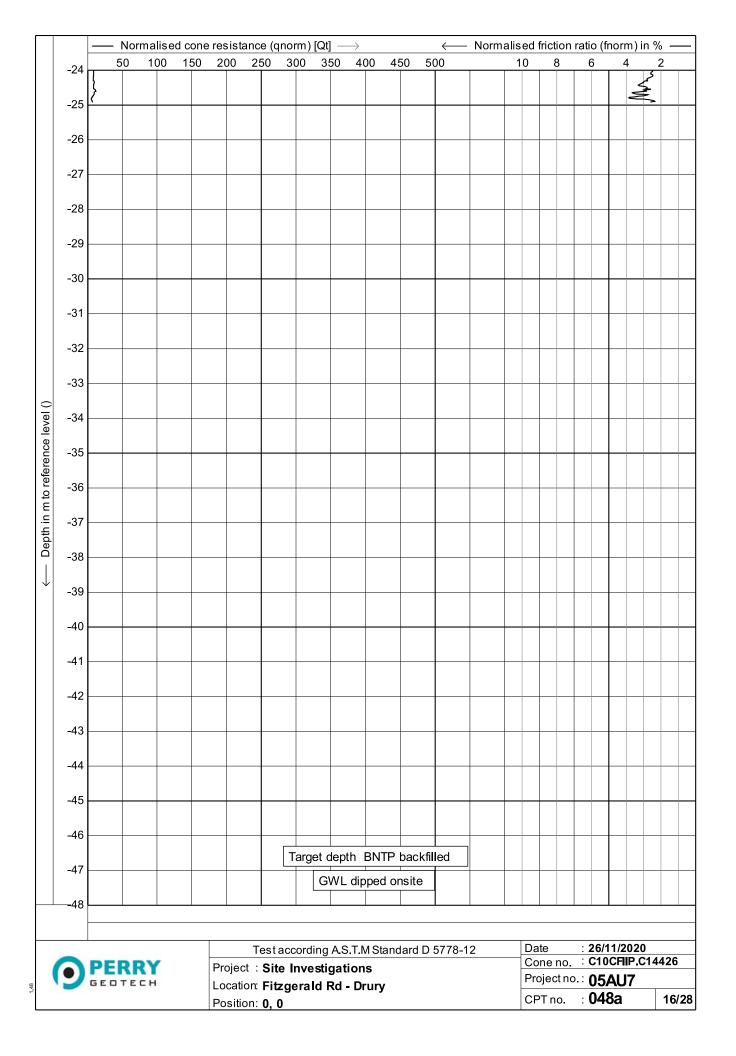


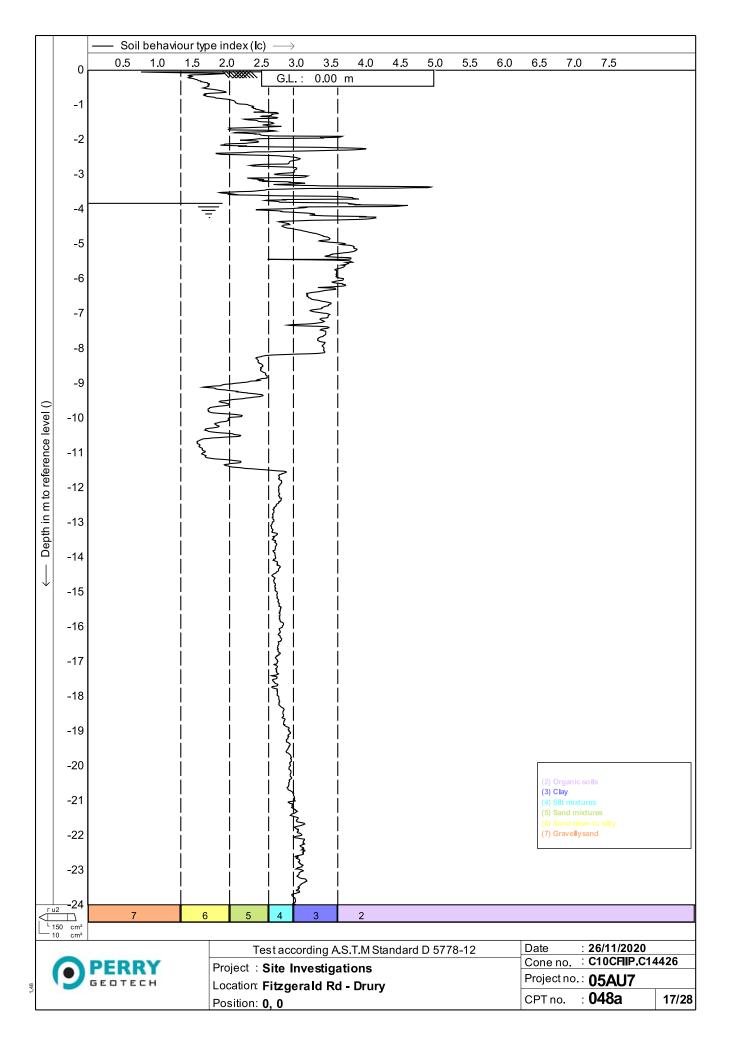


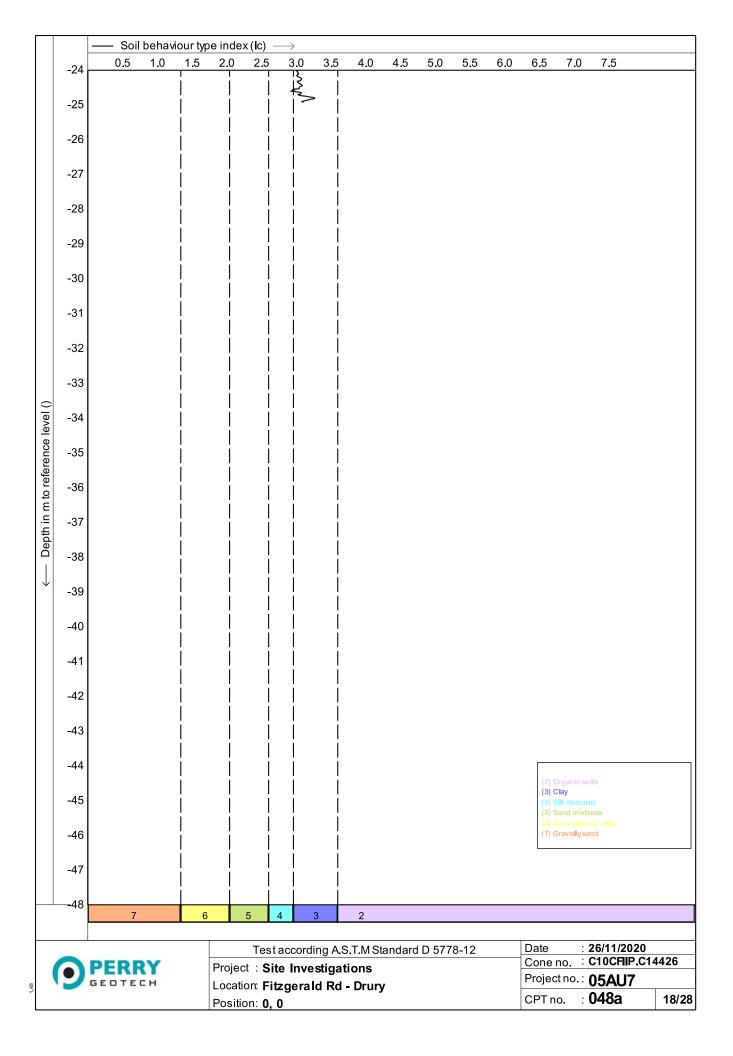


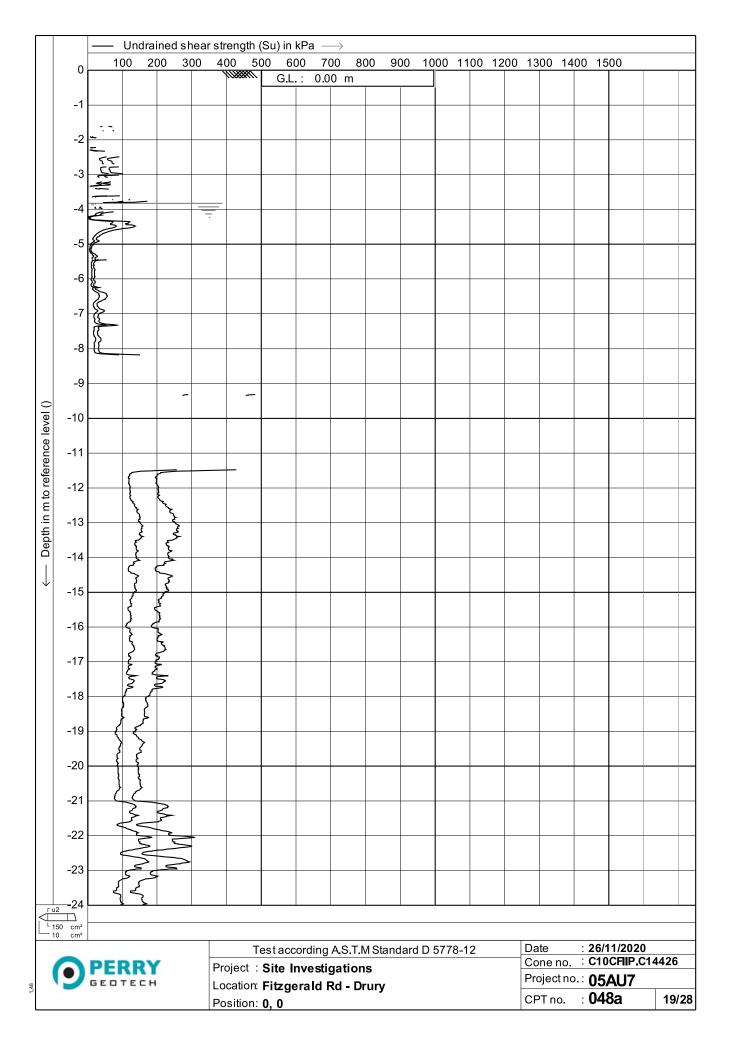


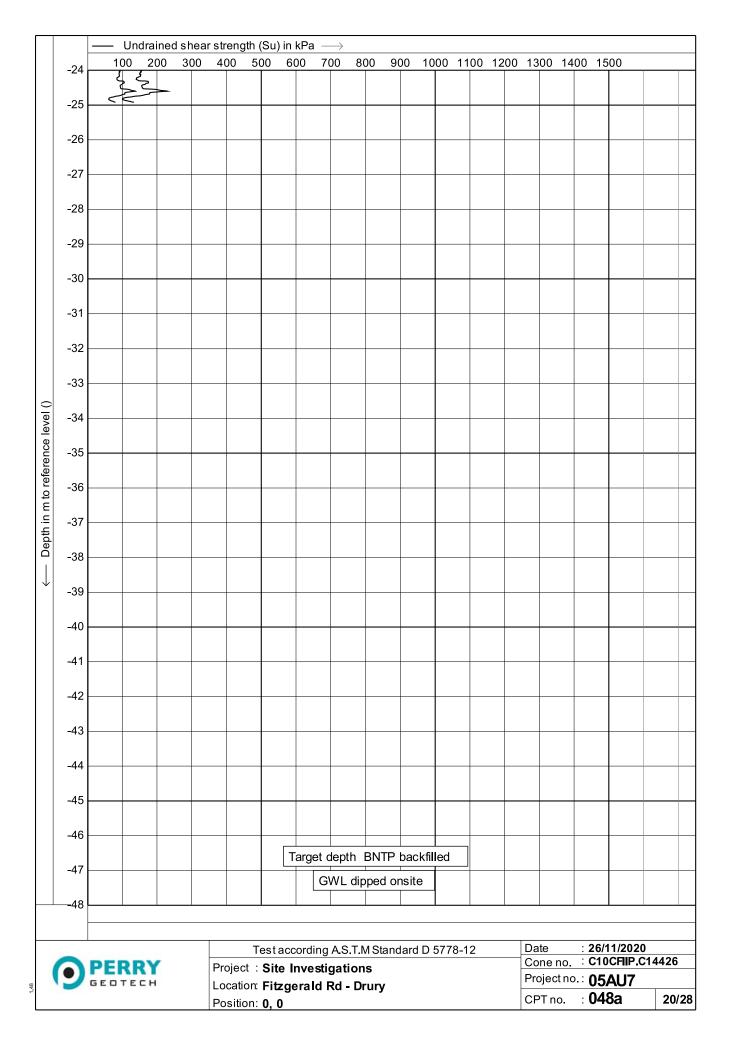


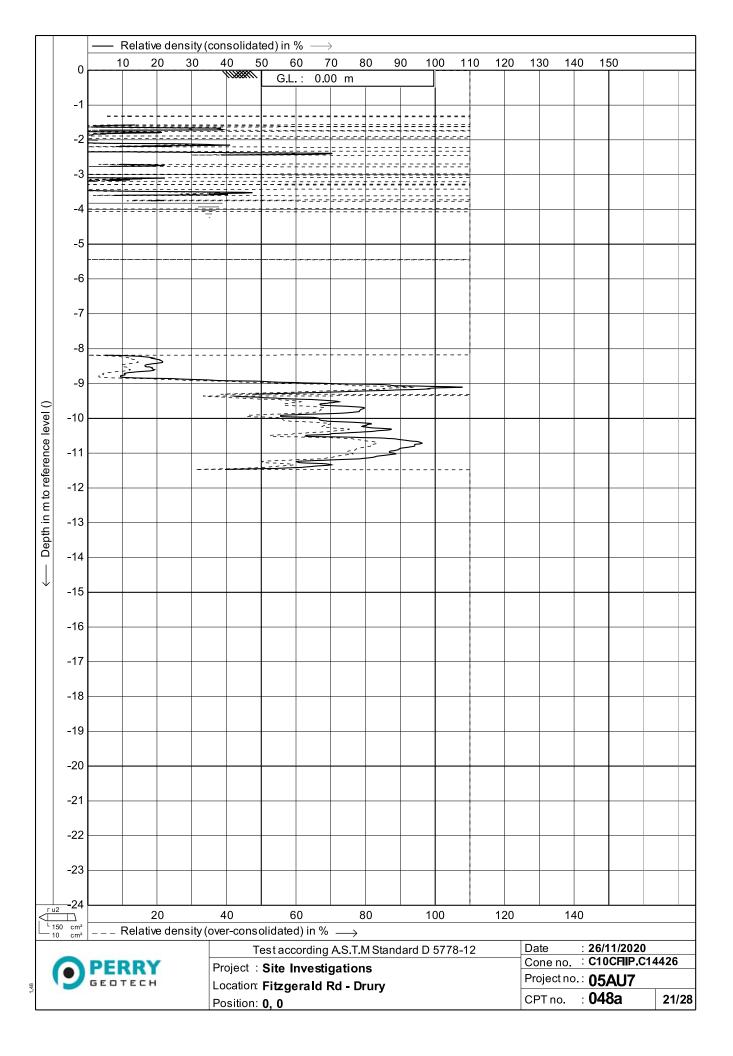


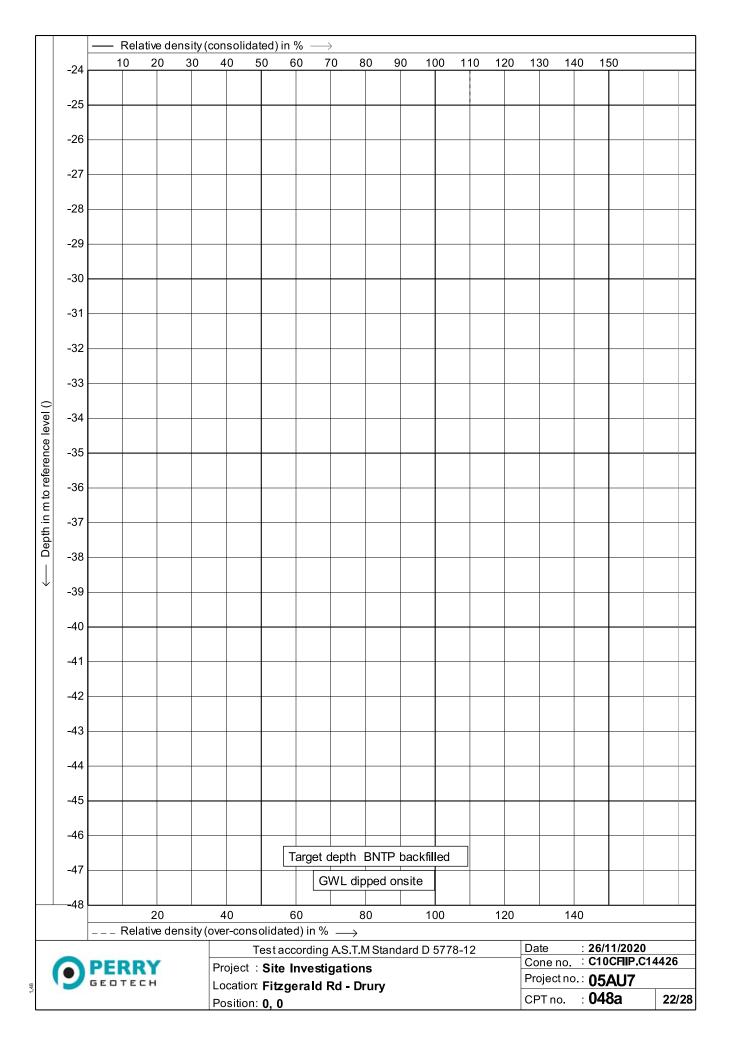


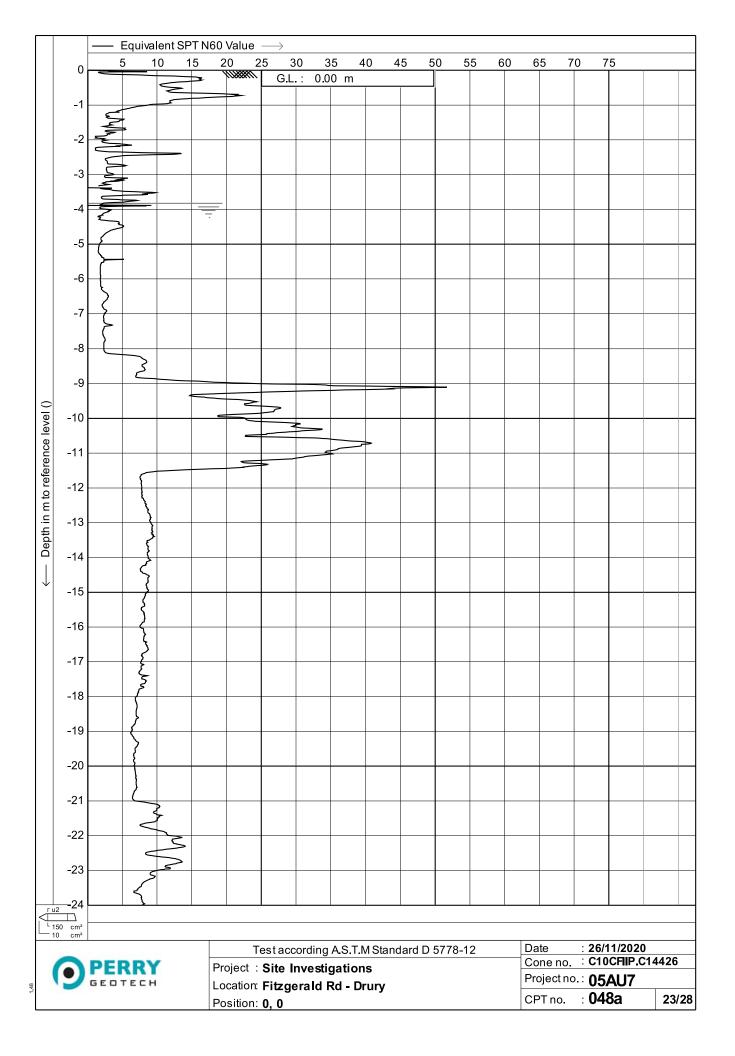


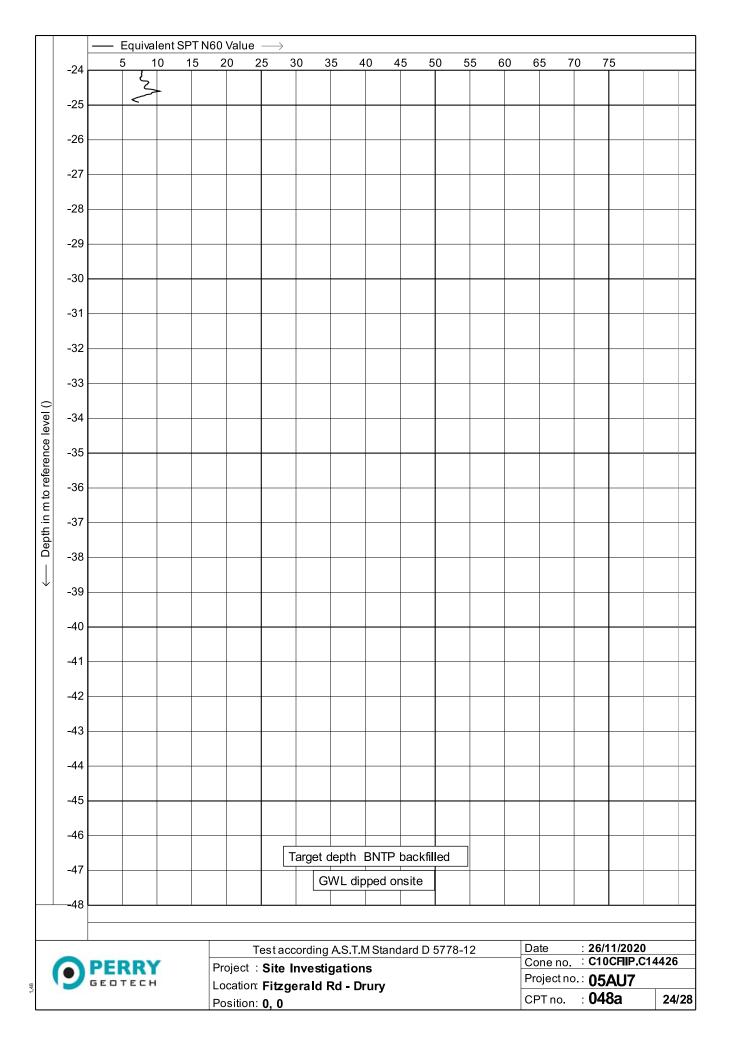


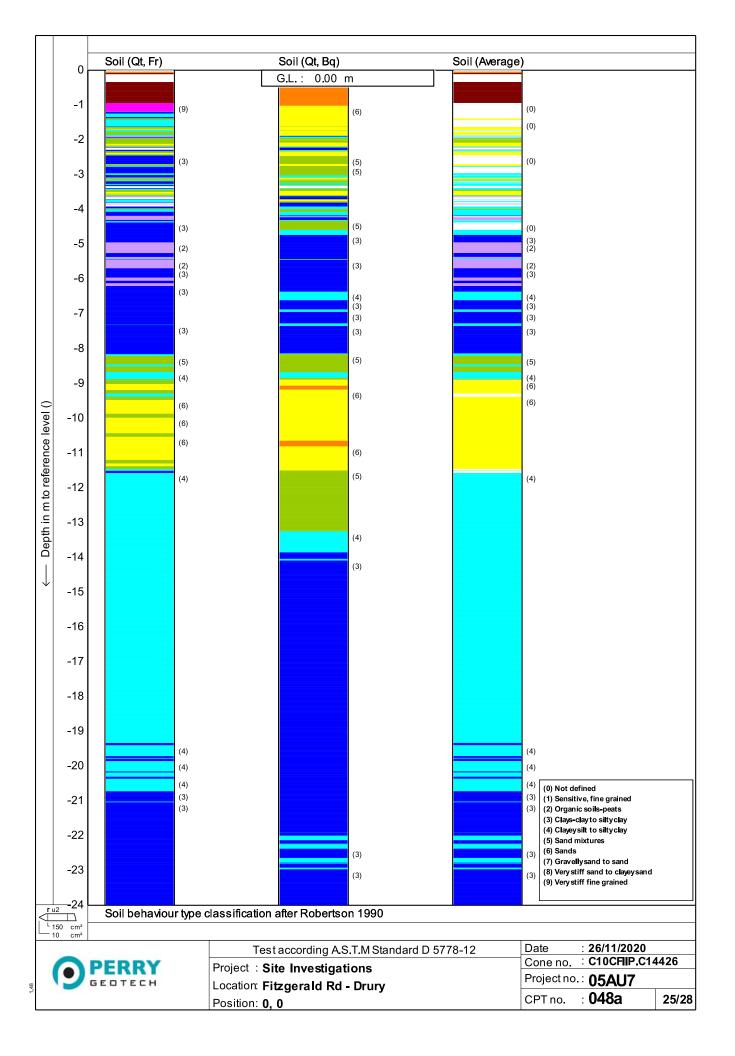


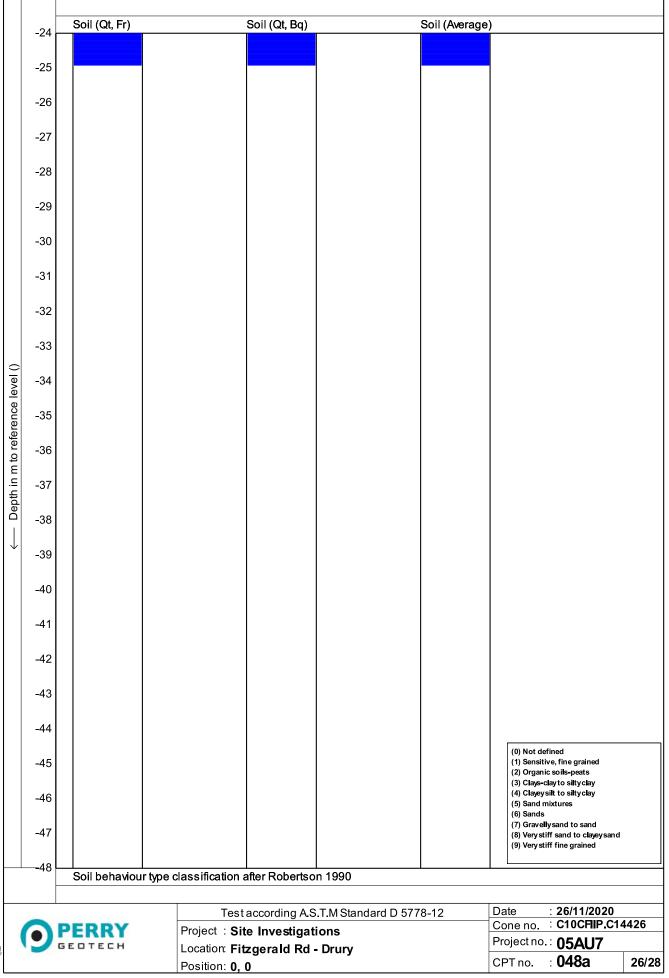


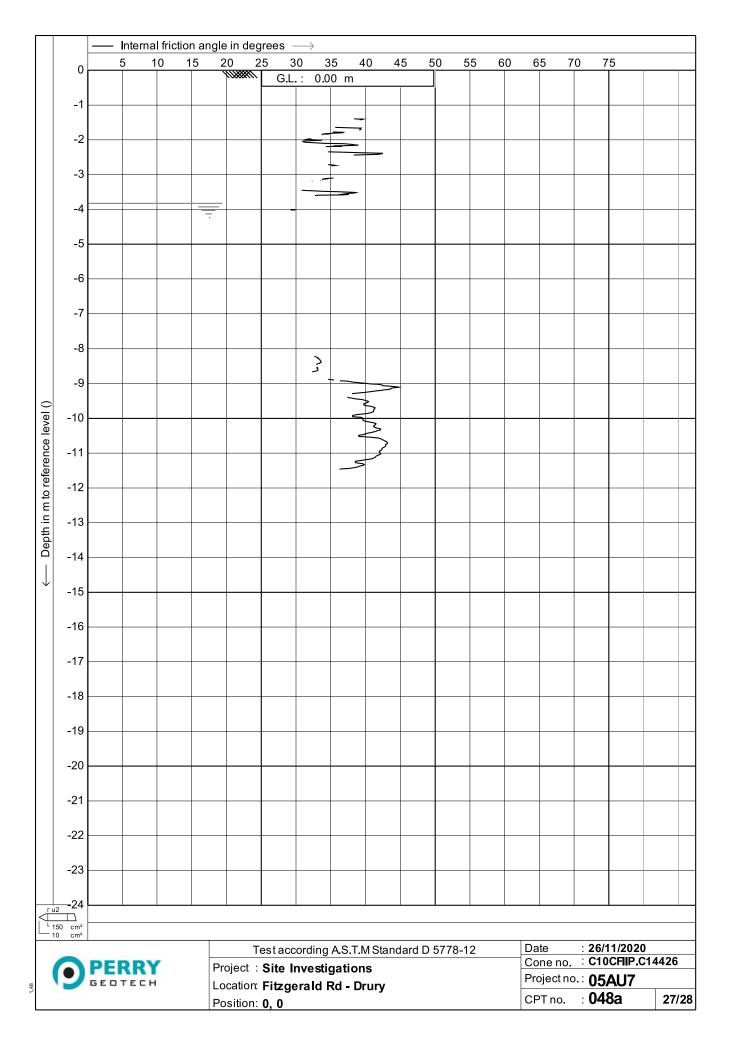


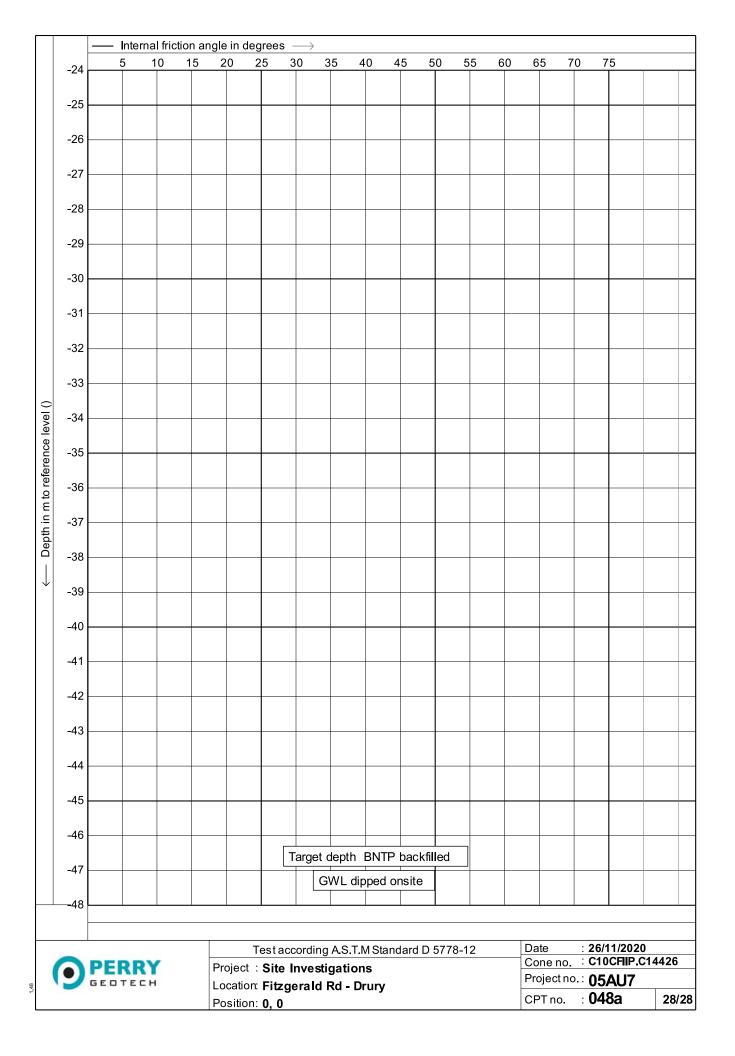


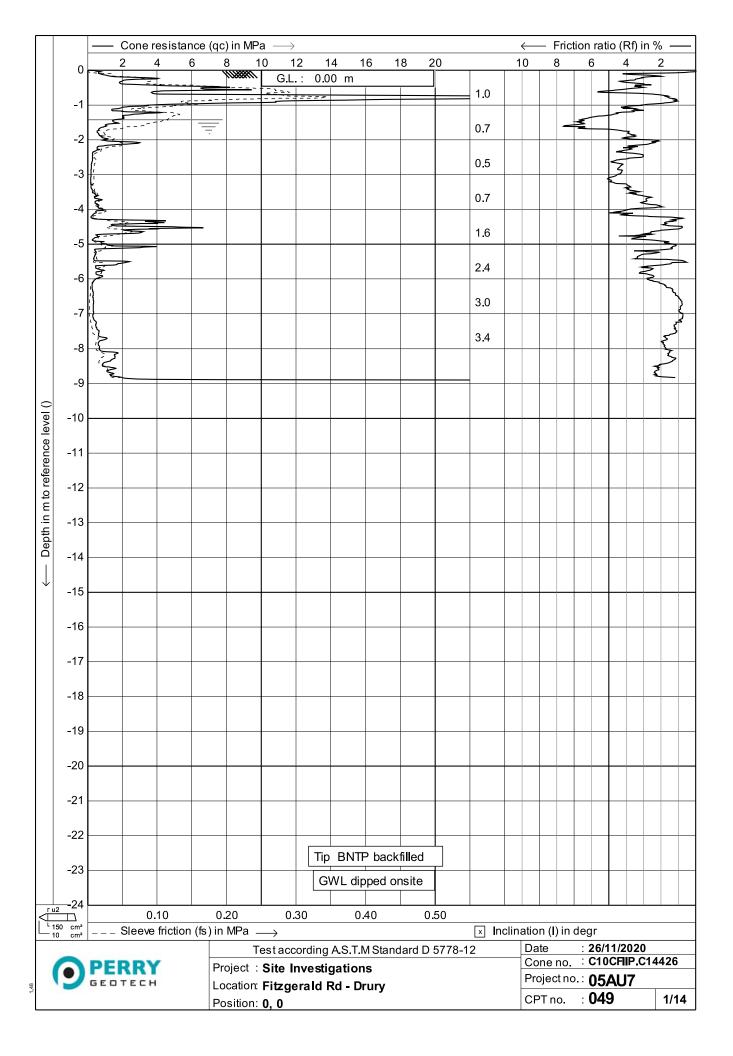


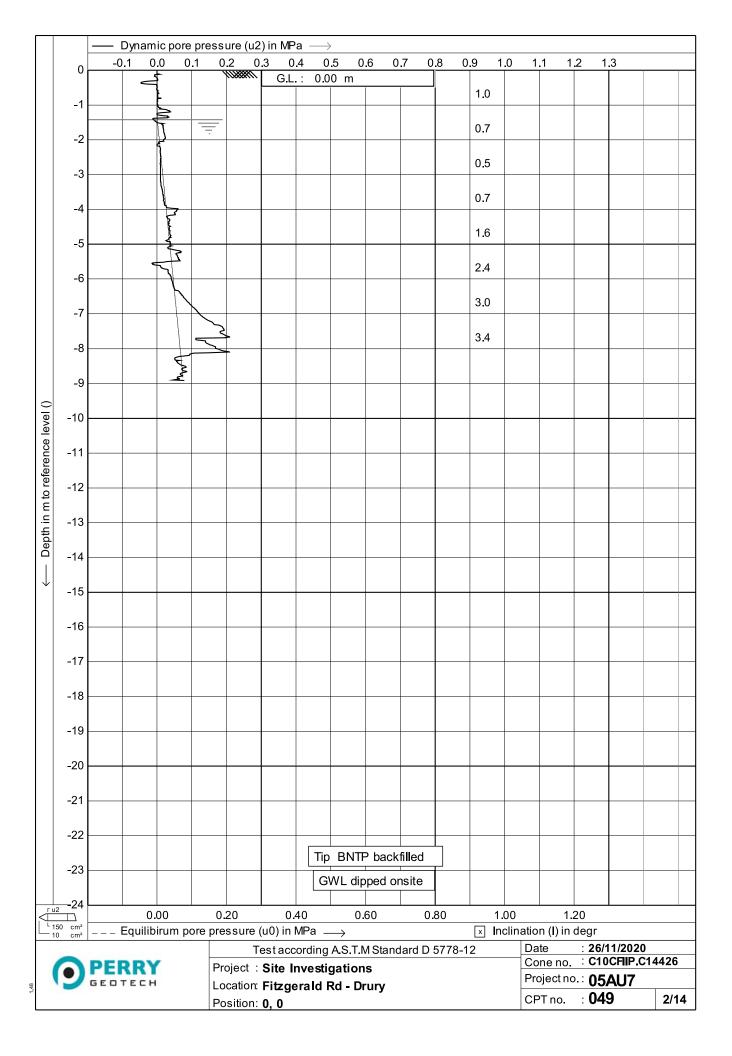


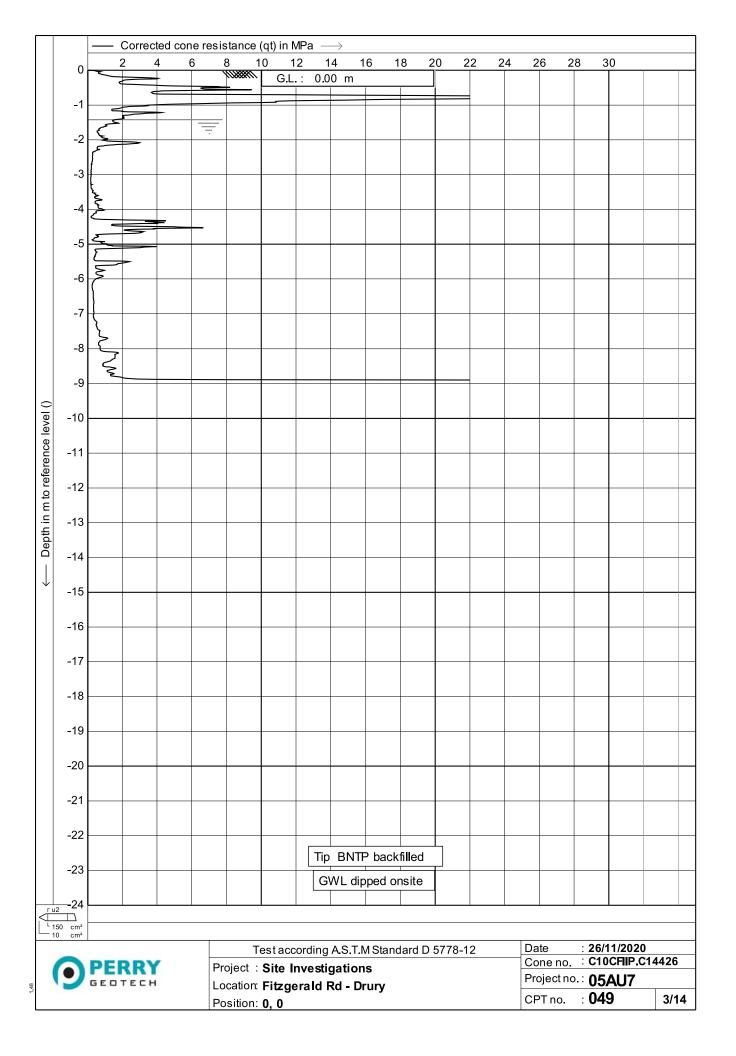


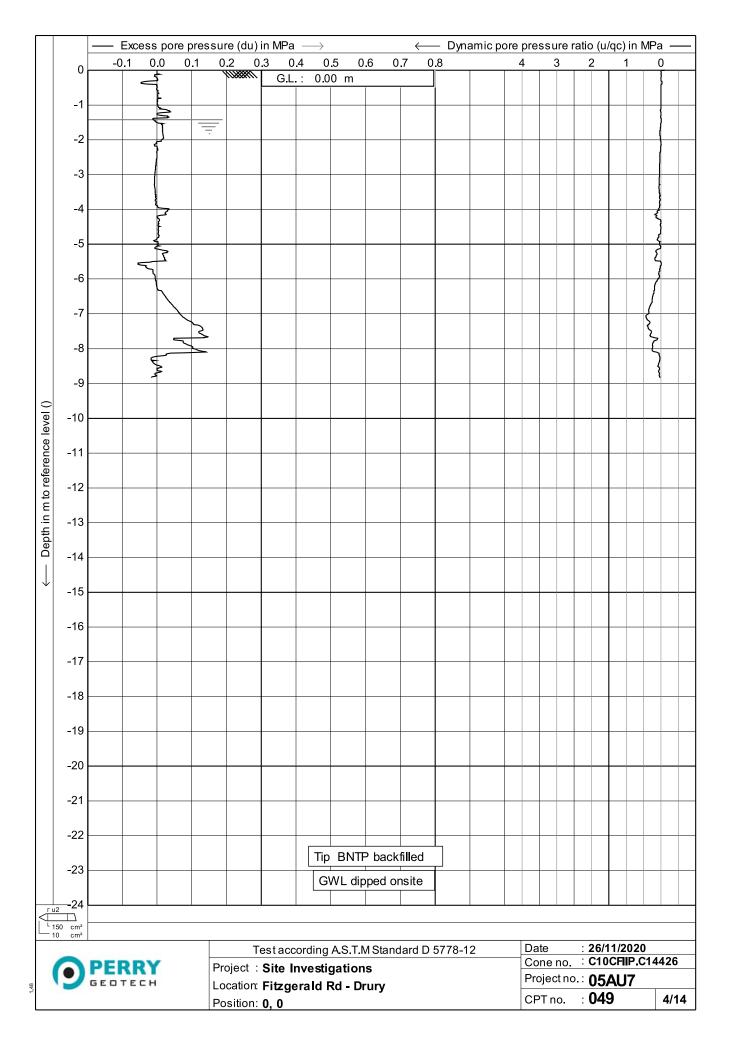


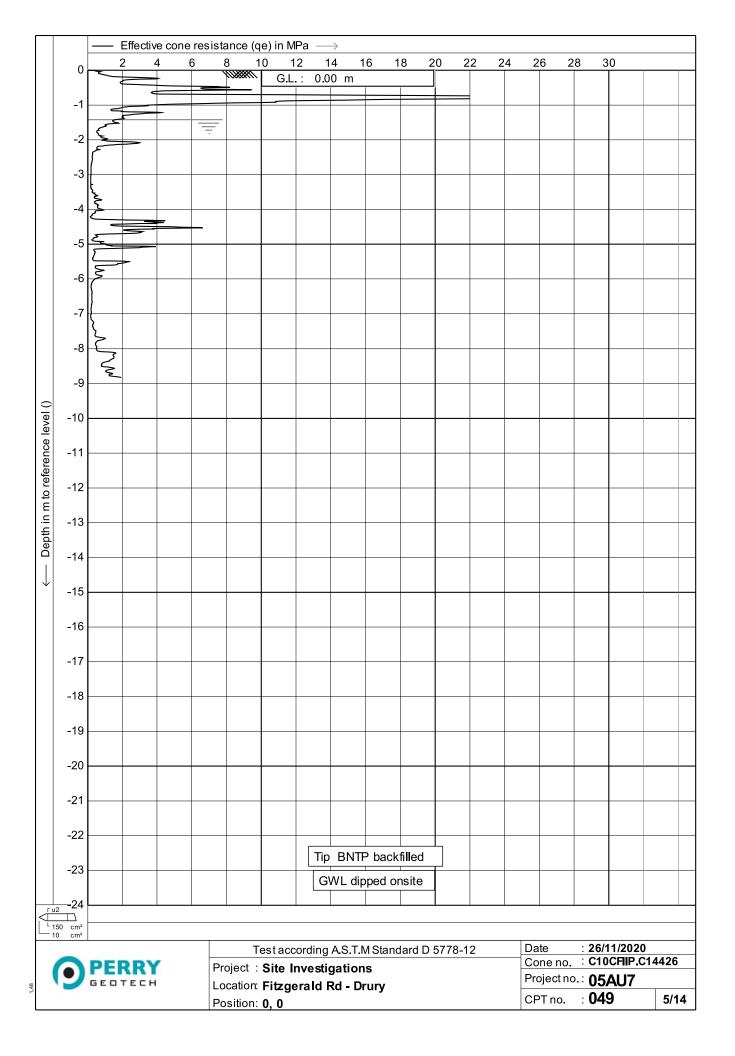


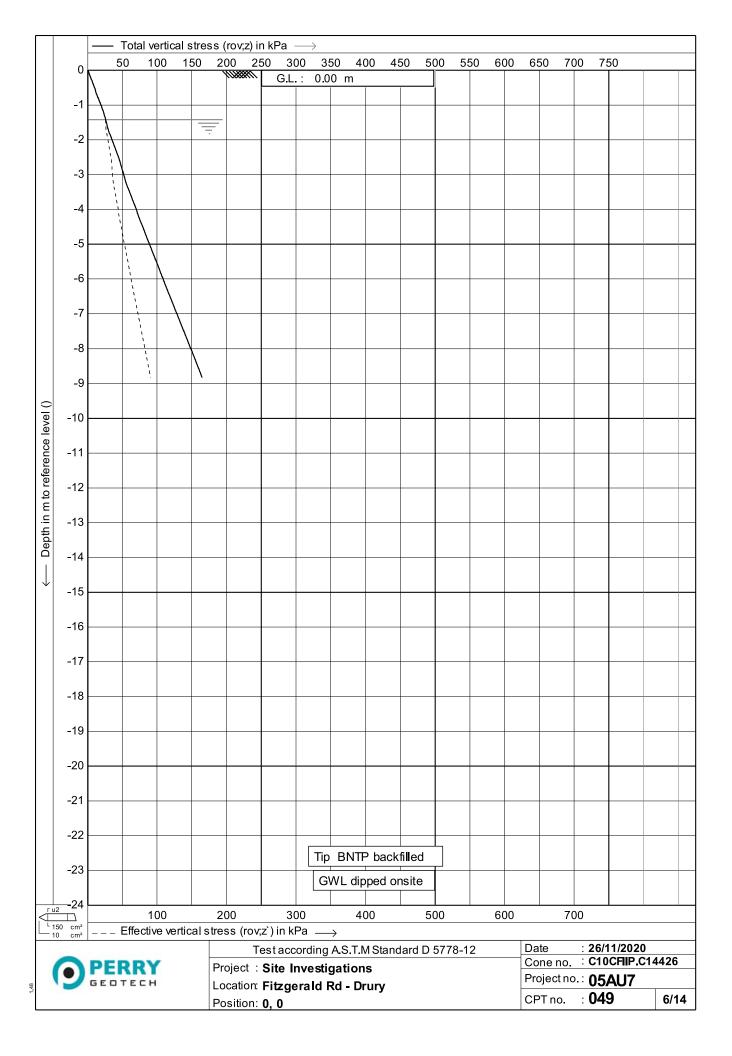


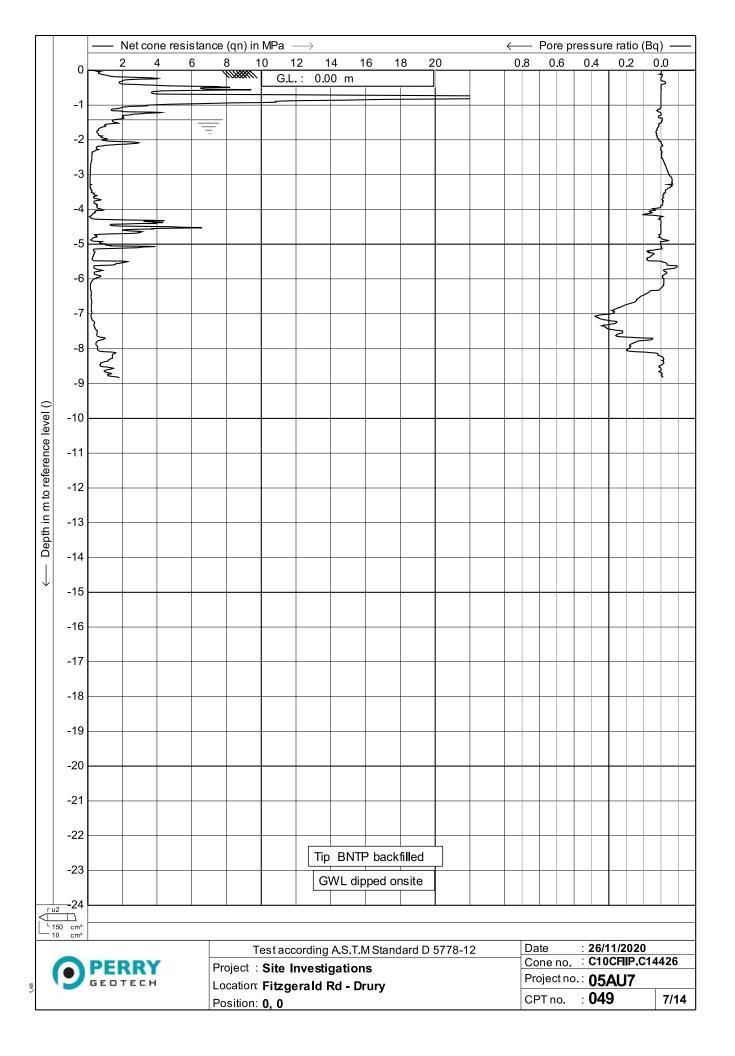


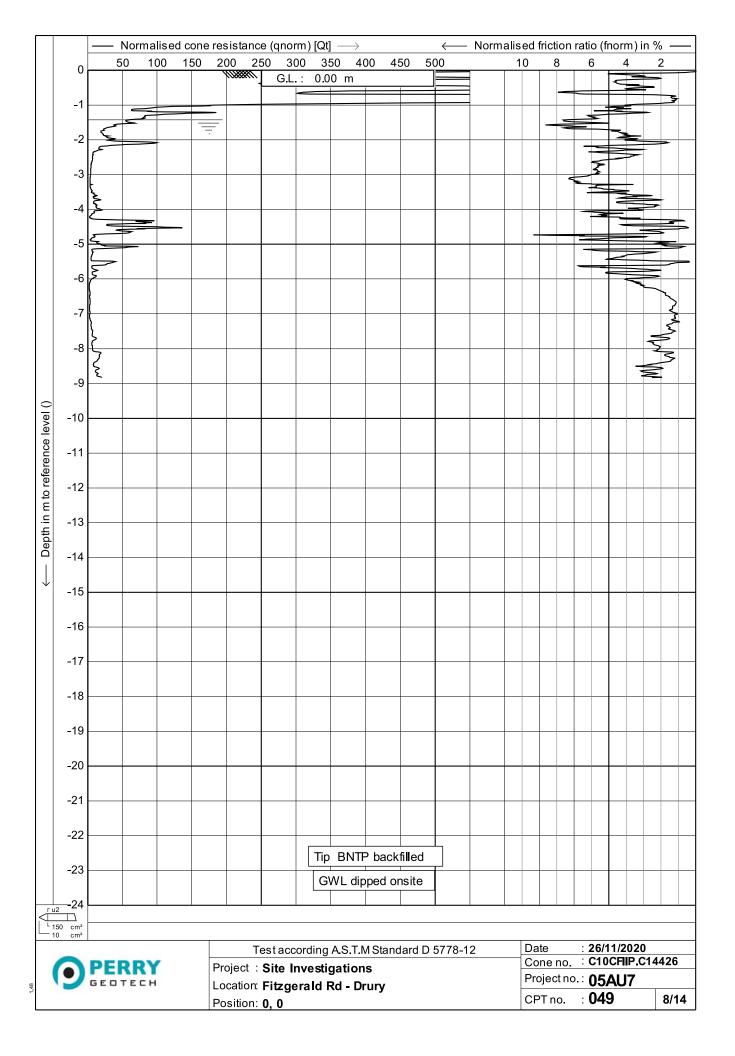


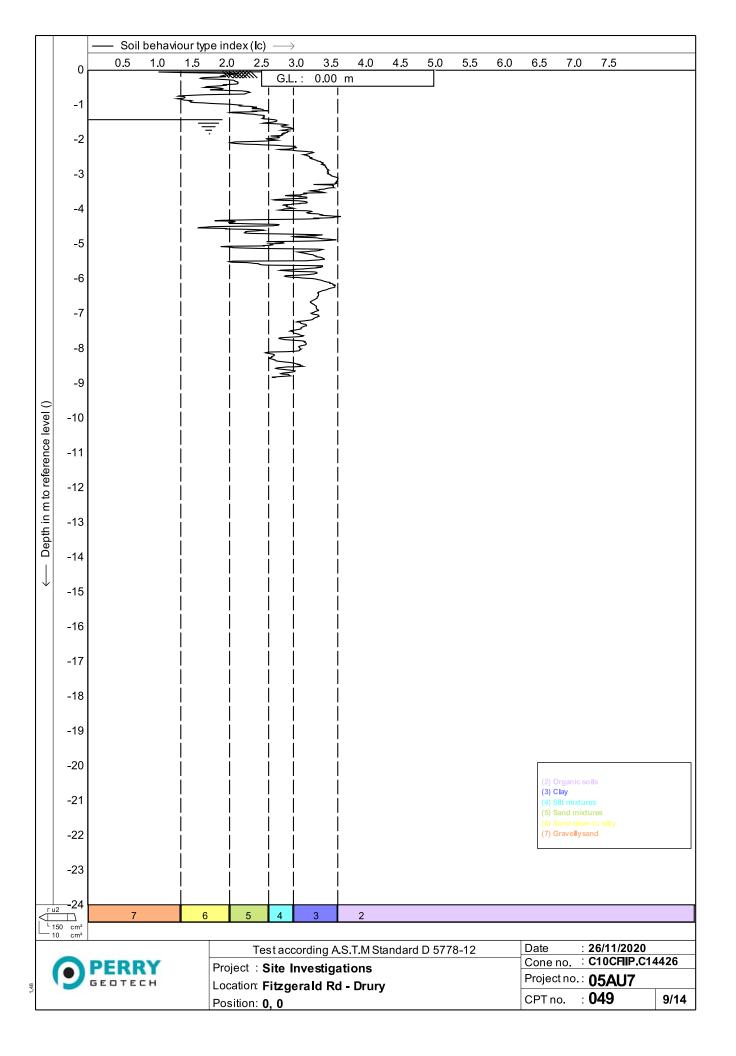


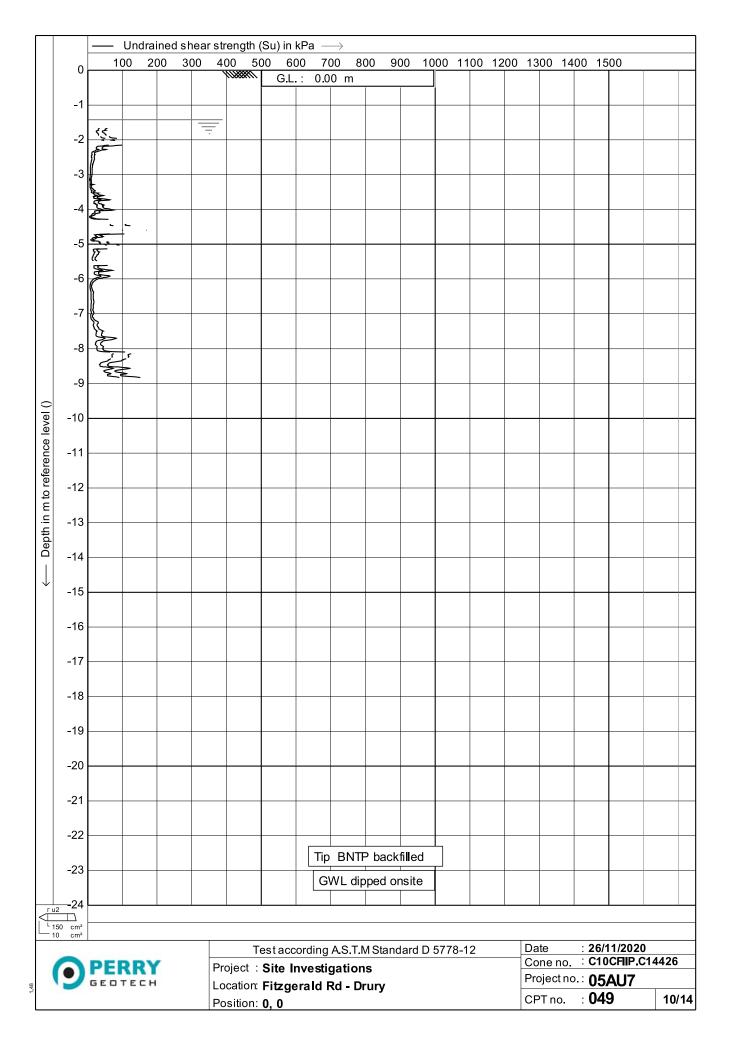


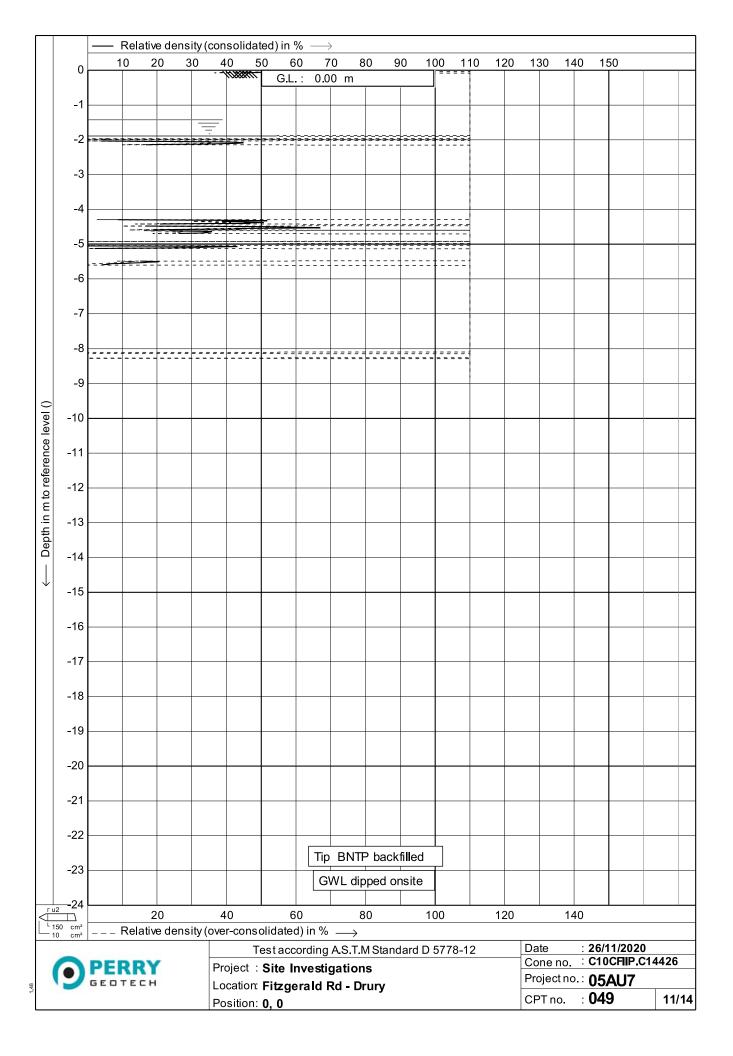


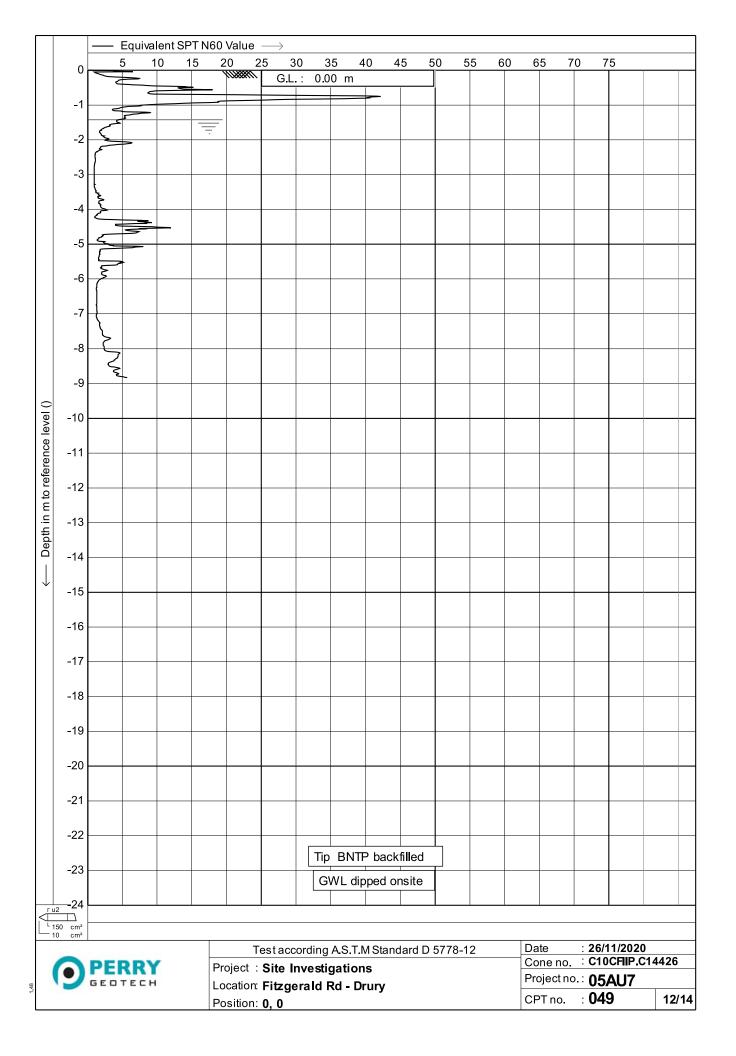


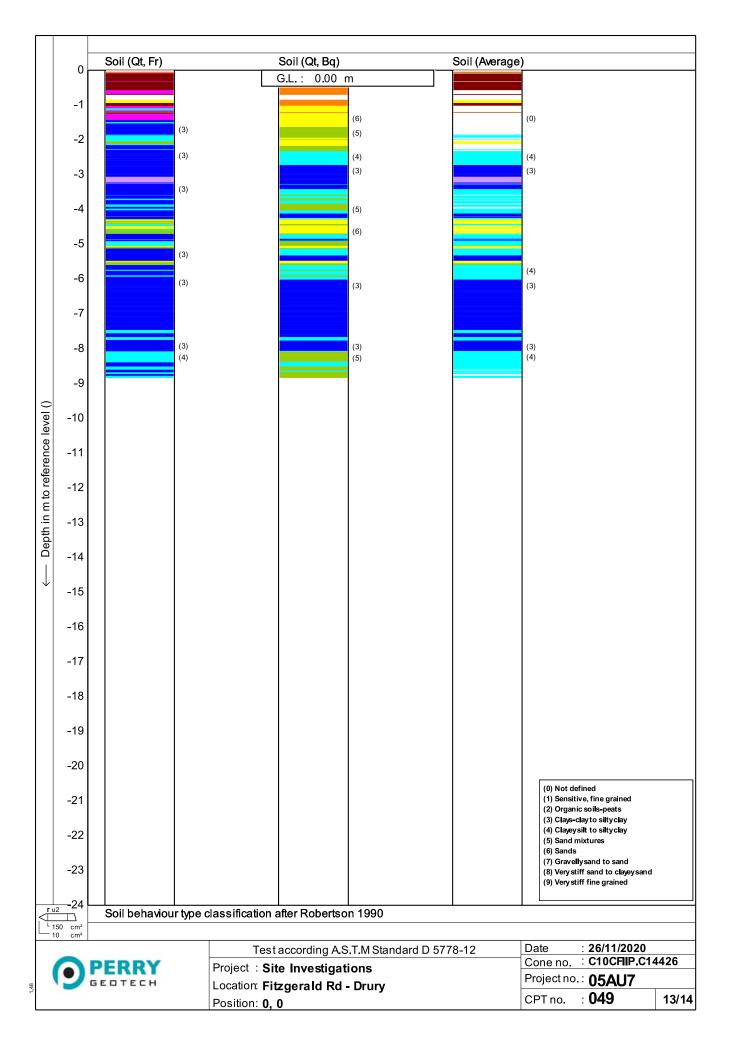


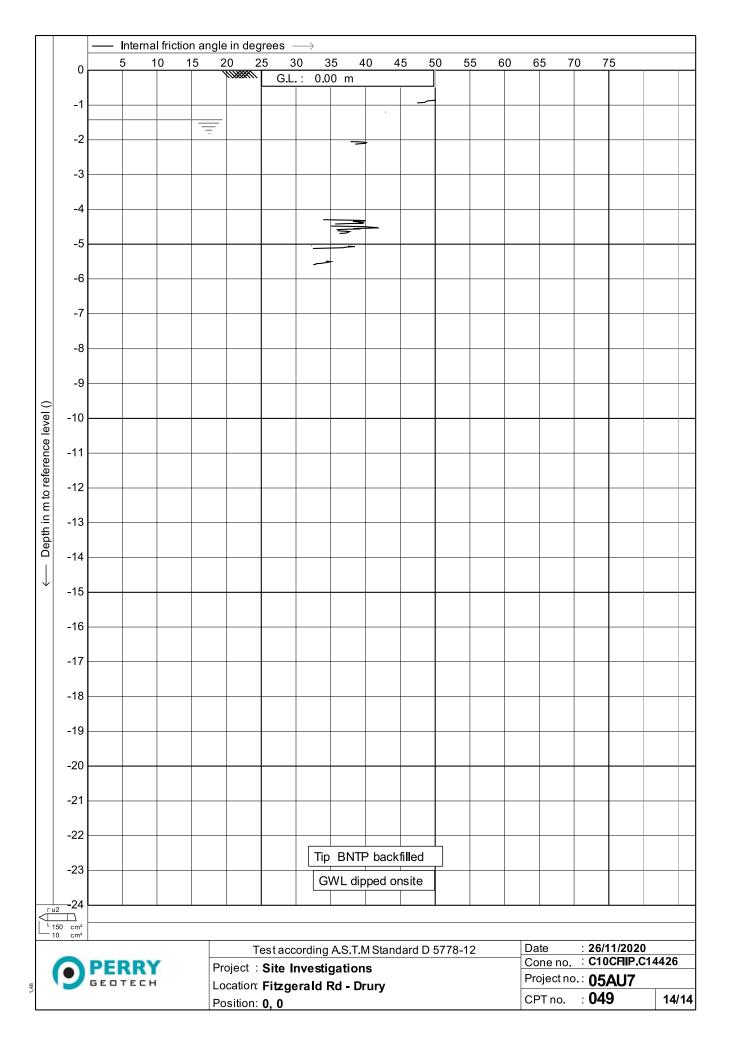














Level 4, 139 Carlton Gore Road PO Box 9762, Newmarket Auckland, New Zealand Tel: +64 9 520 6019 www.aurecongroup.com

HSV Serial No: DR4938 Correction Factor: 1.519

**Kiwi Properties Ltd** Client: Project: Drury Development
Location: 132 Flanagan Road, Drury

Project Reference: 510611

**HA007** 

Sheet 1 of 1

CO-ORDINATES: Mt Eden 2000 DRILLING INFORMATION Method: Hand Auger Equipment: 50mm Auger Contractor: Aurecon 416465m 774645m 10.000m Easting: Northing: Ground Level:

Date started: 15/01/2021 Date completed: 15/01/2021 90° N/A Inclination: Orientation:

Logged by: WBM Input by: WBM Reviewed byGO Verified by: JM

Soil Description  Testing  Pensitrometer Test (Selexos/Homes)  Additional Observations of CLAY with taxon and brown. Soft to firm, dry, high alexitory. Sand is five.  3.8 S 9.12.15.18.21.24.27  Dim: TOPSOIL  3.8 S 9.12.15.18.24.27  Dim: Topsoil  4.8 S 9.12.18.24.24.27  Dim: Topsoil	ontracto	r: Aurecon	(NZVD2016)	Orientation:	N/A	Verified by: Jivi	
Sily CLAY with some sail; brownish orange, specked black. Very aff. most, high plasticity.  3.35m; CLAY with some sail; brownish orange, specked black. Very aff. most, high plasticity.  3.5m; Sily CLAY with some sail; brownish orange, specked black. Very aff. most, high plasticity. Saint as fire.  3.5m; Sily CLAY with some saint orange brown. Very stiff, moist, high plasticity. Saint as fire.  3.5m; Sily CLAY with trace saint orange brown. Very stiff, moist, high plasticity. Saint as fire.  3.5m; ISHSV 12252 NPs  4.5m; ISHSV 12262 NPs  5.5m; ISHSV 12262 NPs  4.5m; ISHSV 12262 NPs  5.5m; ISHSV 12262 NPs  6.5m; ISHSV 12262 NPs  7.5m; ISHSV 12262 NPs  6.5m; ISHSV 12262 NPs  7.5m; ISH	Graphic Log			Testing	Penetrometer Test (Blows/100mm)	Additional Observations	R.L. (m)
D.35m: CLAY with some sill; brownish orange, specified black. Very stiff, most, high plasticity.  D.35m: SBy CLAY with race sand; orange brown. Very stiff, moist, high plasticity. Sand is fine.  1.8m: ISHSV 12252 kPe  1.8m: ISHSV 12252 kPe  2.5m: ISHSV		<b>0m:</b> Silty CLAY with trace sand plasticity. Sand is fine.	; brown. Soft to firm, dry, high			0m: TOPSOIL	-
1.5m; ISHSV 18704 kPa		stiff, moist, high plasticity.		0.5m: ISHSV 122/52 kPa		0,35m: SOUTH AUCKLAND VOLCANIC FIELD	- - -
	X -X- -X- -X- X X	0.8m; Sitty CLAY with trace san high plasticity. Sand is fine.	id; orange brown. Very stiff, moist,	1m: ISHSV 213+/- kPa			- - 9 - -
ARKS:  All Shay (and the part of the part	x  x  x  x			1.5m: ISHSV 167/94 kPa			- - - -
ARKS:  Water Level Readings:	× × × ×			2m: ISHSV 129/97 kPa			- - 8 - -
Hand Auger terminated at 3m (Target Depth Reached)  3m: ISHSV UTP	× × × × × × ×			2.5m: ISHSV UTP			- - -
ARKS: Water Level Readings:	<u>xx</u>	Hand Augustamainatad at 2m	Torget Death Decembed)	2m; ICHC// HTD			7
Trater Level Neadings.			Target Deptif Reached)	SIII. ISHSV OTF			- - - - - - - - - - - - - - - - - - -
estigation collar is recorded to an accuracy of ±10 m horizontal and ±1 m vertical.  Date Time   Hole Depth   Water Level No water level recorded	MARKS Investiga		of ±10 m horizontal and ±1 m vertical.		Date Time   Hole	Depth   Water Level	



HSV Serial No: DR4938 Correction Factor: 1.519

Client: Kiwi Properties Ltd
Project: Drury Development

	uckland, el: +64 9 ww.aure	New Zealand LOC 520 6019 Congroup.com	cation: 132 Flanagan Road oject Reference: 510611	i, Drury					Sheet 1 of 1	
Met Equ	hod: ipmen	i <b>INFORMATION</b> Hand Auger t: 50mm Auger r: Aurecon	CO-ORDINATES: Mt Eden 2000 Easting: 416352m Northing: 774619m Ground Level: 6.000m (NZVD2016)		Date started Date comple Inclination: Orientation:				Logged by: WBM Input by: WBM Reviewed byGO Verified by: JM	
Depth (m)	Graphic Log	Soil I	Description	Tes	ting	(Bl	Scalation Scalat	r Test	Additional Observations	R.L. (m)
	V., 23	<b>0m:</b> Clayey SILT; brown. Firm, o	dry, high plasticity.			: : :	: : :	: : :	Qm: TOPSOIL	<del>                                     </del>
•			ownish orange, mottled dark brown.						0.05m: FILL	1
		Very stiff, moist, high plasticity. <b>0.2m:</b> CLAY with some gravel a stiff, moist, high plasticity. Grave slightly vesicular basalt	nd minor silt; orange brown. Very el is fine to medium, sub-rounded,	-						-
2		stiff, flust, flug plasticity. Grave, slightly vesicular basalt.  Hand Auger terminated at 0.4m	,	0.5m: ISHSV U	TP				0.4m: Scala bouncing.	
-										-
1. E	MARKS:	refusal at 0.4m for both hand auger ar	nd scala penetrometer.				Date	er Level Readir Time   Hole D	epth   Water Level	

**HA009** 



Level 4, 139 Carlton Gore Road PO Box 9762, Newmarket Auckland, New Zealand Tel: +64 9 520 6019 www.aurecongroup.com

Client: Kiwi Properties Ltd
Project: Drury Development
Location: 132 Flanagan Road, Drury
Project Reference: 510611

**HA010** 

Sheet 1 of 1

DRILLING INFORMATION Method: Hand Auger Equipment: 50mm Auger

HSV Serial No: DR4938 Correction Factor: 1.519

CO-ORDINATES: Mt Eden 2000
Easting: 416408m
Northing: 774537m Easting: Northing:

18/01/2021 18/01/2021 Date started: Date completed: Inclination:

Logged by: WBM Input by: WBM Reviewed byGO

	or: Aurecon  Northing: 774537m  Ground Level: 8.000m (NZVD2016)	Orientation:	N/A	Verified by: JM	
Graphic Log	Soil Description	Testing	● Scala Penetrometer Test (Blows/100mm)	Additional Observations	
~	<b>0m:</b> Clayey SILT; brown. Soft, dry, high plasticity.		3 6 9 12 15 18 21 24 27	0m: TOPSOIL	
				Um: TOPSOIL	F
2	0.25m: CLAY with some silt; light brown. Very stiff, moist, high				┝
	plasticity.			0,25m: TAURANGA GROUP	
	-	0.5 101101/ 407/07 1.D.			
- -X -	- 0.6m: Silty CLAY; light orange brown. Very stiff, moist, high plasticity.	0.5m: ISHSV 197/37 kPa			F
					F
<u> </u>	- X				Ĺ
<u>-</u>		1 101101/0401/110			Ĺ.
<u>X</u> -		1m: ISHSV 213+/- kPa			-
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<u>X</u> -:	1.6m: CLAY with minor silt; brownish orange. Very stiff, moist, high	1.5m: ISHSV 177/68 kPa			-
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_	1	2m: ISHSV 161/91 kPa			-
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Level 4, 139 Carlton Gore Road PO Box 9762, Newmarket Auckland, New Zealand Tel: +64 9 520 6019 www.aurecongroup.com

Client: Kiwi Properties Ltd
Project: Drury Development
Location: 132 Flanagan Road, Drury
Project Reference: 510611

**TP026** 

Sheet 1 of 1

Exca Exca Date	avated avator e start	by: type ed:	LCS Ltd: 13t Excavator 10/12/2020 d: 10/12/2020	Easting: Northing: Ground level:	416480m 774510m 13.00m (NZVD2016)	Width: 2m Length: 3m		B ➡ 90 (De	bogged by: STH Input by: STH Checked by: GO Verified by: JM	
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-	× × × × × × × × × × × × × × × × × × ×		0.3m: Clayey SILT; dark brow	wn. Very stiff, moist, Iov	w plasticity.			0.3m: S0 FIELD	OUTH AUCKLAND VOLCANIC	+
- (			0.5m: Silty fine to coarse GR Gravel and cobbles are sub- moderately vesicular, basalt. [Completely weathered BAS/	angular, highly weathe	les; brownish red. Moist. red to completely weathered, i	brownish red,	0.5m: ISHSV 161/	(33 kPa		-
- (			<b>1.3m to 1.6m</b> :Amorphous	organics			1m: ISHSV UTP			12  
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Client: **Kiwi Properties Ltd** Project: Drury Development Location: 114 Flanagan Road, Drury Project Reference: 510611

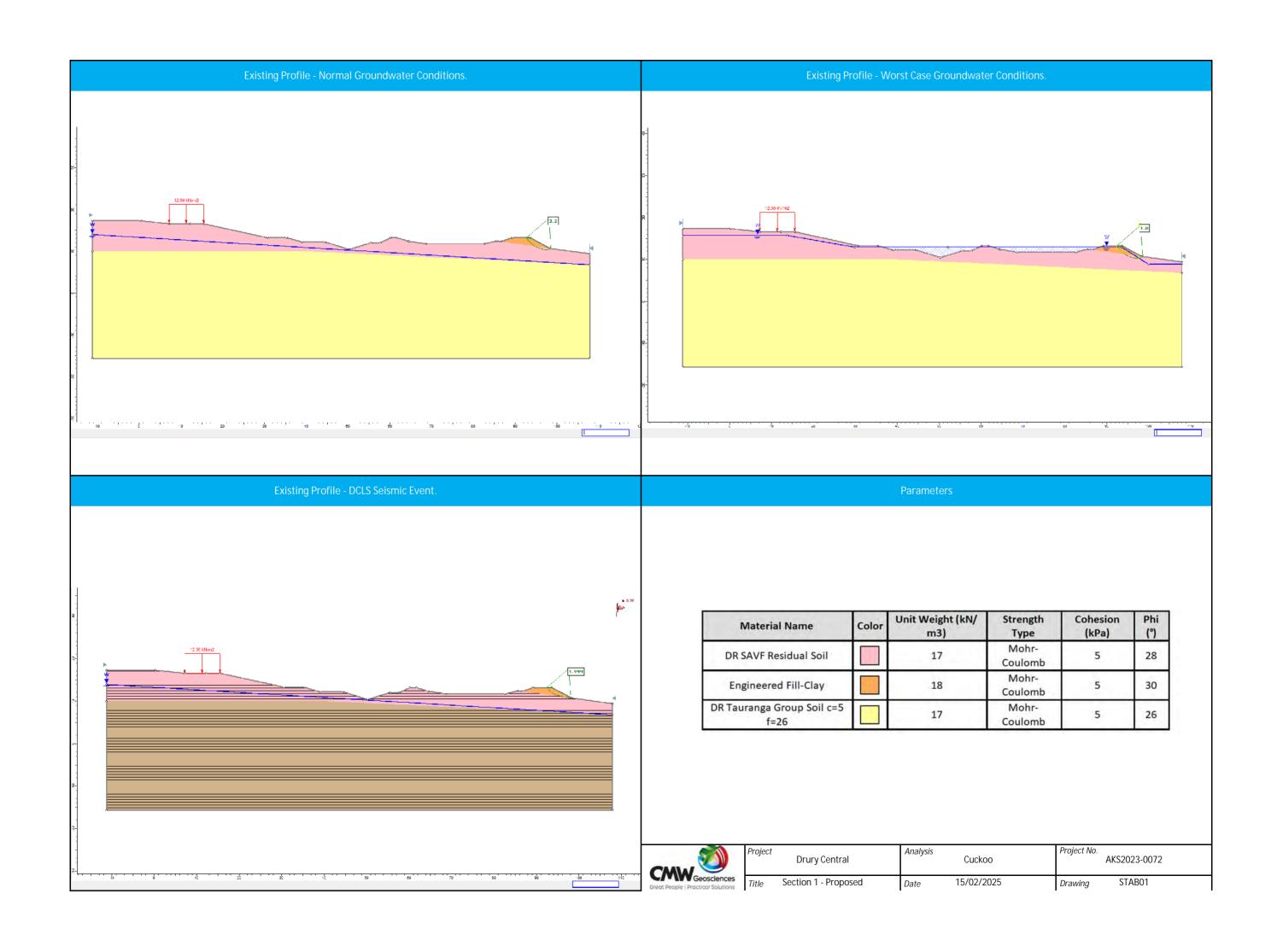
**TP028** 

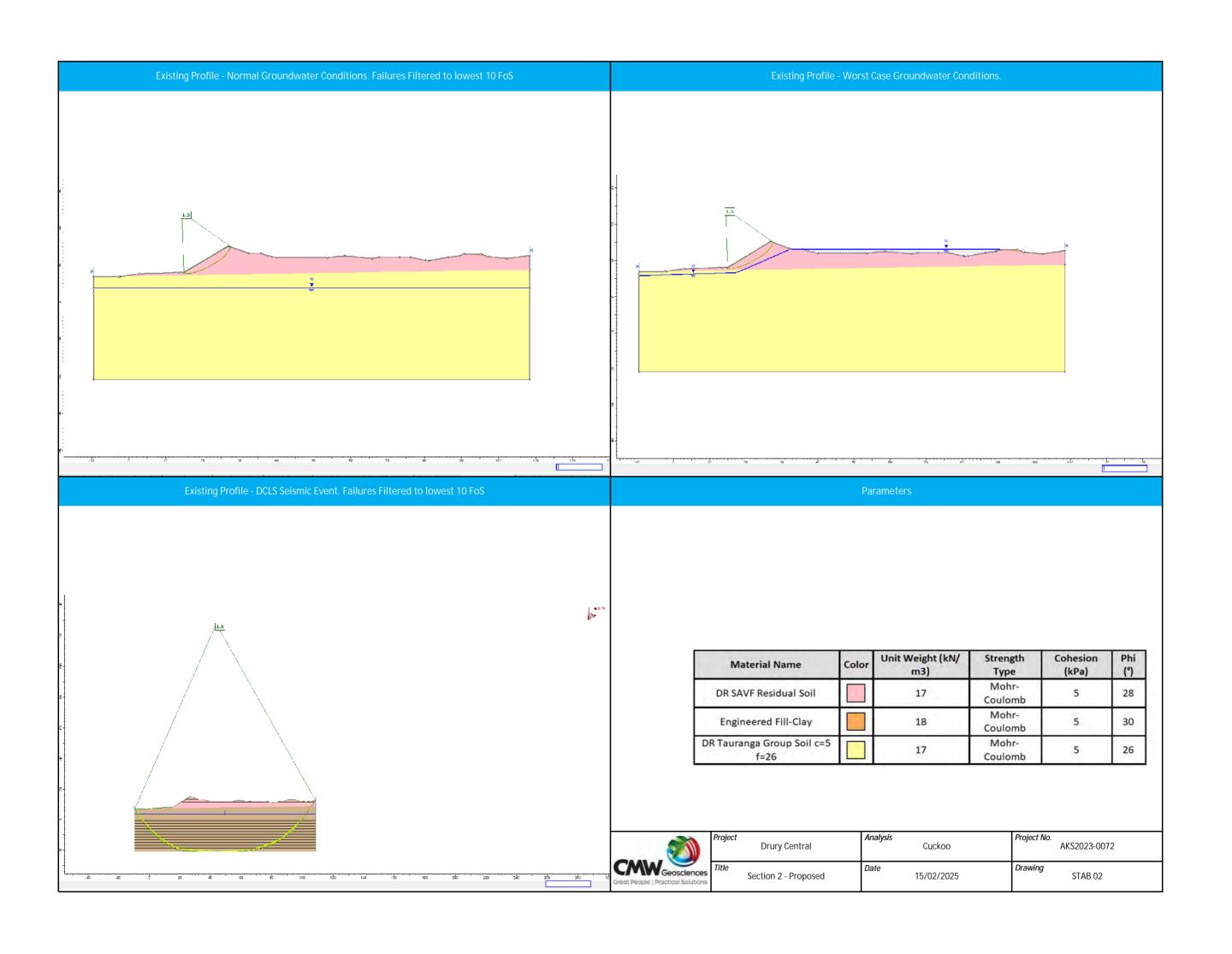
Sheet 1 of 1

Logged by: STH Input by: STH Checked by: GO Verified by: JM TRIAL PIT INFORMATION CO-ORDINATES: Mt Eden 2000 **DIMENSIONS AND ORIENTATION** Excavated by: LCS Ltd Easting: 416477m Width: 2m Excavator type:
Date started:
Date completed: 774604m 10.00m 13t Excavator 10/12/2020 Northing: B 🖒 180 (Deg) Length: 3m Ground level: (NZVD2016) 10/12/2020 Code Graphic Log Depth (m) Ξ Soil Description Testing Additional Observations Layer ( RL 0m: SILT with some day, organics and trace sand; brownish black. Very stiff, dry, non-plastic. 0m: TOPSOIL × Organics, rootlets. Sand, fine to medium. × 0.25m: SOUTH AUCKLAND VOLCANIC FIELD 0.25m: Clayey SILT; dark brown. Very stiff, moist, high plasticity. 0.5m: ISHSV 188/30 kPa **0.65m**: Highly weathered, brownish red, moderately vesicular BASALT; extremely weak. [Silty fine to coarse GRAVEL with minor cobbles; brownish red, loosely packed]. 9 1m: ISHSV 197/46 kPa 1.5m: ISHSV 143/27 kPa 8 2m: ISHSV 179/36 kPa 2.8m: Moderately weathered, black, moderately vesicular BASALT; very weak. 2.8m: Small amount of recovery from bottom of the test pit, not enough for photo of lithology Terminated at 3m (Target depth reached) Water Level Readings 1. Investigation collar is recorded to an accuracy of ±10 m horizontal and ±1 m vertical. Date Time | Hole Depth | Water Level No water level recorded 2. TP028 backfilled upon completion. HSV Serial No: DR4938 Correction Factor: 1.519



# APPENDIX D Slope Stability Analysis







# **APPENDIX G**

Stage 1 Subdivision Report



26 February 2025 Document Ref: AKS2023-0072AT | Rev 1

Kiwi Property Holdings No.2 Limited c/- Woods 6 Nugent Street
Newmarket, Auckland

Attention: Colin Dryland

# RE: GEOTECHNICAL REVIEW 133 FITZGERALD ROAD, DRURY

## 1.0 INTRODUCTION

CMW has been engaged by Kiwi Property Holdings No.2 Limited to undertake a review of plans (Consent number: BUN60490224, LUC60414878, SUB60414913), which depict the subdivision of several superlots created as Stage 1 of the Drury Central development into individual residential lots. Aurecon has monitored the underlying earthworks of the subject Stage 1 superlots and CMW have produced a Geotechnical Completion Report (GCR) following the completion of the bulk earthworks.

This report summarises the recommendations of that GCR in respect to the residential subdivision.

## 2.0 REFERENCES

# 2.1 Geotechnical Completion Report

 Geotechnical Completion Report for the Drury Stage 1 earthworks dated 2 July 2024 AKS2023-0072AJ Rev 1. Produced by CMW Geosciences.

The GCR can be found in Appendix B.

# 2.2 Supplied Drawings

- Drawings of the proposed subdivision supplied by Woods dated February 2025 and referenced P24-646-01-2000-2004.
- These drawings show the subdivision of existing superlots Lot 10 22 which results in the formation 292 new residential lots, 13 jointly owned access lots (JOALS) and footpaths.
- It is understood that no additional earthworks are to be carried out on the lots.

These drawings can be found in Appendix A.

## 3.0 GEOTECHNICAL COMPLETION REPORT REVIEW

The following section summarises the CMW Geosciences Geotechnical Completion Report (GCR) prepared for Stage 1 of the development. This document provides engineered fill certification in accordance with NZS4431:1986 for fills suitable for development as per NZS 3604, subject to any restrictions in the GCR.

The following key clauses / restrictions from the statement of professional opinion include:



- 4 (a) The completed earthworks take into account land slope and foundation stability considerations on the building platform areas.
- 4(b) A geotechnical ultimate bearing capacity of 300 kPa may be assumed for shallow foundation design on the building platforms of Lots 10 to 22 inclusive.
- 4(c) The site (seismic) subsoil class for each lot has been assessed in accordance with NZS1170.5:2004
  Clause 3.1.3 from borelogs that included measurements of geotechnical properties. Our assessment is
  that lots 10 to 22 are Class C- shallow soil.
- 4 (d) An AS2870 expansive soil class of H1 has been assumed for all lots.

In addition, the GCR also summarises key geohazards as below.

- Liquefaction- The liquefaction risk for the lots on this development has been assessed as low.
- Uncertified Temporary Filling- At the time of completing this GCR all Residential Lots have environmental
  clean water diversion control bunds constructed on the perimeter of the Lots. For Lots 12 to 14,
  temporary staging for topsoil screening had been taking place with a number of topsoil stockpiles
  present on the Lots.
- Fill Induced Settlement- The majority of the filling on this stage of the development was placed between December 2023 and February 2024. A series of settlement markers was installed in areas of deeper fill at its completion and have been periodically monitored for both horizontal and vertical movements. Horizontal changes have been noted to be within the survey accuracy limits, while vertical movements are depicting seasonal shrink/ swell variations as anticipated. The results show show a plateauing of readings, on the basis of the relatively minor magnitude of fill depths on this site, together with the elapsed time since it was placed, it is considered that remaining post-construction settlements will be within NZS3604 limits.

# 4.0 RECOMMENDATIONS AND FURTHER WORK

Given that there are no additional fills to be placed on the subject lots, it can be expected that these will be suitable for residential development in respect to NZS3604 provided the following recommendations are carried out:

- All unsuitable stockpiles must be removed. The subgrade must then be inspected and checked by shallow boreholes to ensure this has not softened over time due to the presence of the stockpile.
- Expansive soil class testing for the GCR was carried out in respect to large superlot development, and therefore was limited in its scope. Additional expansive soil testing should be carried out at a greater frequency given the number of individual lots present.

Following completion of the works a GCR should be completed describing the further works completed and providing a statement of professional opinion for the newly created lots.

### 5.0 LIMITATIONS

Additional important information regarding the use of your CMW report is provided in the 'Using your CMW Report' document attached to this report.

This report has been prepared for use by Kiwi Property Holdings No.2 Limited, Auckland Council and their professional advisers in relation to the Drury Centre Stage 2 project in accordance with the scope, proposed uses and limitations described in the report. Should you have further questions relating to the use of your report please do not hesitate to contact us.



Where a party other than Kiwi Property Holdings No.2 Limited seeks to rely upon or otherwise use this report, the consent of CMW should be sought prior to any such use. CMW can then advise whether the report and its contents are suitable for the intended use by the other party.

#### For and on behalf of CMW Geosciences

Prepared by: Reviewed and authorised by:

(Light)

Tasneem Khan Chris Ritchie
Geotechnical Engineer Principal Engineering Geologist, PEngGeol

Distribution: 1 electronic copy to Kiwi Property Holdings No.2 Limited c/- Woods via email

Original held at CMW Geosciences





#### USING YOUR CMW GEOTECHNICAL REPORT

Geotechnical reporting relies on interpretation of facts and collected information using experience, professional judgement, and opinion. As such it generally has a level of uncertainty attached to it, which is often far less exact than other engineering design disciplines. The notes below provide general advice on what can be reasonably expected from your report and the inherent limitations of a geotechnical report.

#### Preparation of your report

Your geotechnical report has been written for your use on your project. The contents of your report may not meet the needs of others who may have different objectives or requirements. The report has been prepared using generally accepted Geotechnical Engineering and Engineering Geology practices and procedures. The opinions and conclusions reached in your report are made in accordance with these accepted principles. Specific items of geotechnical or geological importance are highlighted in the report.

In producing your report, we have relied on the information which is referenced or summarised in the report. If further information becomes available or the nature of your project changes, then the findings in this report may no longer be appropriate. In such cases the report must be reviewed, and any necessary changes must be made by us.

#### Your geotechnical report is based on your project's requirements

Your geotechnical report has been developed based on your specific project requirements and only applies to the site in this report. Project requirements could include the type of works being undertaken; project locality, size and configuration; the location of any structures on or around the site; the presence of underground utilities; proposed design methodology; the duration or design life of the works; and construction method and/or sequencing.

The information or advice in your geotechnical report should not be applied to any other project given the intrinsic differences between different projects and site locations. Similarly geotechnical information, data and conclusions from other sites and projects may not be relevant or appropriate for your project.

#### Interpretation of geotechnical data

Site investigations identify subsurface conditions at discrete locations. Additional geotechnical information (e.g. literature and external data source review, laboratory testing etc) are interpreted by Geologists or Engineers to provide an opinion about a site specific ground models, their likely impact on the proposed development and recommended actions. Actual conditions may differ from those inferred to exist due to the variability of geological environments. The actual interface between materials may be far more gradual or abrupt than assumed based on the facts obtained. Nothing can be done to change the actual site conditions which exist, but steps can be taken to reduce the impact of unexpected conditions. Interpretation of factual data can be influenced by design and/or construction methods. Where these methods change review of the interpretation in the report may be required.

#### Subsurface conditions can change

Subsurface conditions are created by natural processes and then can be altered anthropically or over time. For example, groundwater levels can vary with time or activities adjacent to your site, fill may be placed on a site, or the consistency of near surface conditions might be susceptible to seasonal changes. The report is based on conditions which existed at the time of investigation. It is important to confirm whether conditions may have changed, particularly when large periods of time have elapsed since the investigations were performed.

#### Interpretation and use by other design professionals

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a geotechnical report. To help avoid misinterpretations, it is important to retain the assistance of CMW to work with other project design professionals who are affected by the contents of your report. CMW staff can explain the report implications to design professionals and then review design plans and specifications to see that they have correctly incorporated the findings of this report.

#### Your report's recommendations require confirmation during construction

Your report is based on site conditions as revealed through selective point sampling. Engineering judgement is then applied to assess how indicative of actual conditions throughout an area the point sampling might be. Any assumptions made cannot be substantiated until construction is complete. For this reason, you should retain geotechnical services throughout the construction stage, to identify variances from previous assumption, conduct additional tests if required and recommend solutions to problems encountered on site.

A Geotechnical Engineer, who is fully familiar with the site and the background information, can assess whether the report's recommendations remain valid and whether changes should be considered as the project develops. An unfamiliar party using this report increases the risk that the report will be misinterpreted.

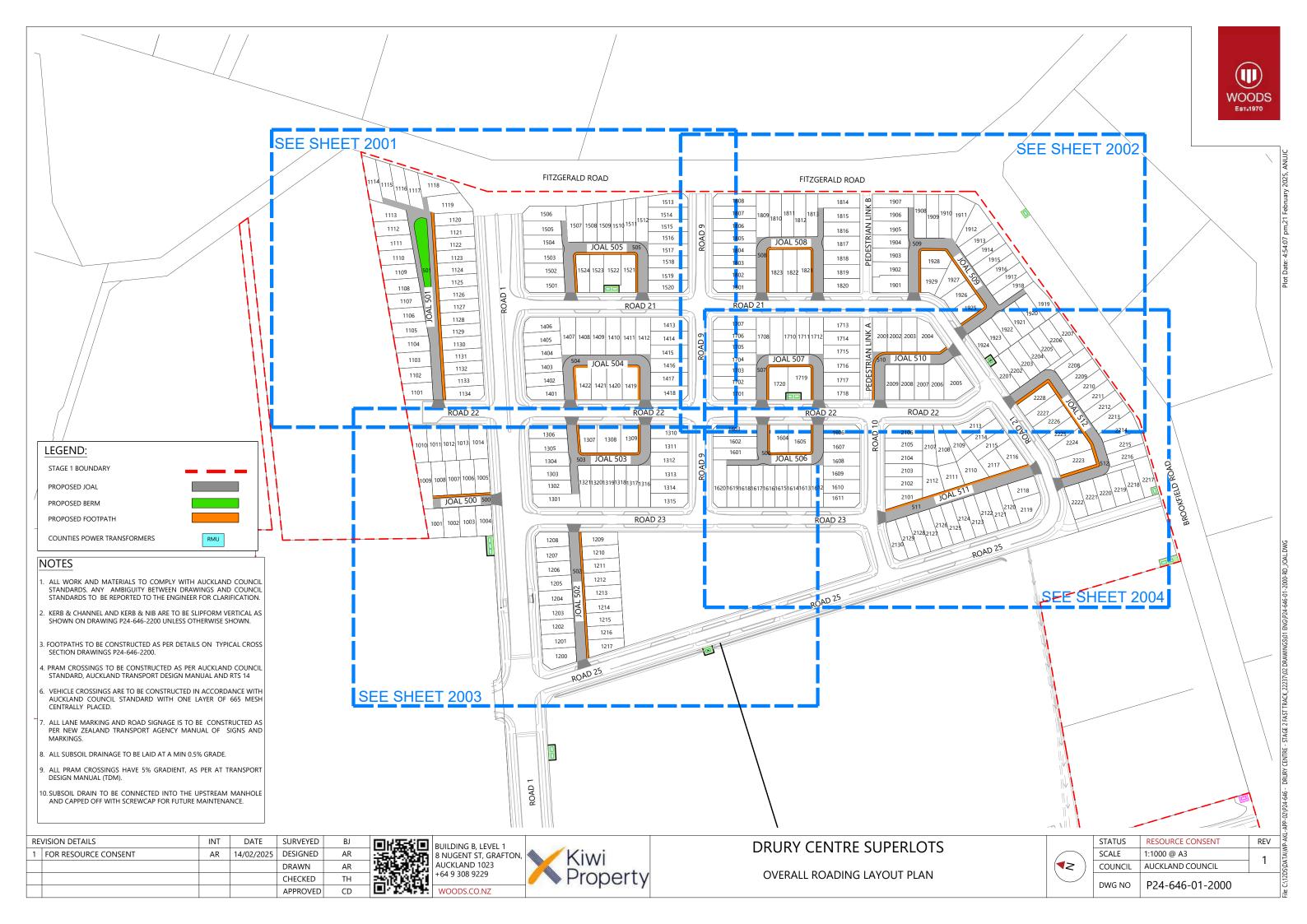
#### **Environmental matters are not covered**

Unless specifically discussed in your report environmental matters are not covered by a CMW Geotechnical Report. Environmental matters might include the level of contaminants present of the site covered by this report, potential uses or treatment of contaminated materials or the disposal of contaminated materials. These matters can be complex and are often governed by specific legislation.

The personnel, equipment, and techniques used to perform an environmental study can differ significantly from those used in this report. For that reason, our report does not provide environmental recommendations. Unanticipated subsurface environmental problems can have large consequences for your site. If you have not obtained your own environmental information about the project site, ask your CMW contact about how to find environmental risk-management guidance.

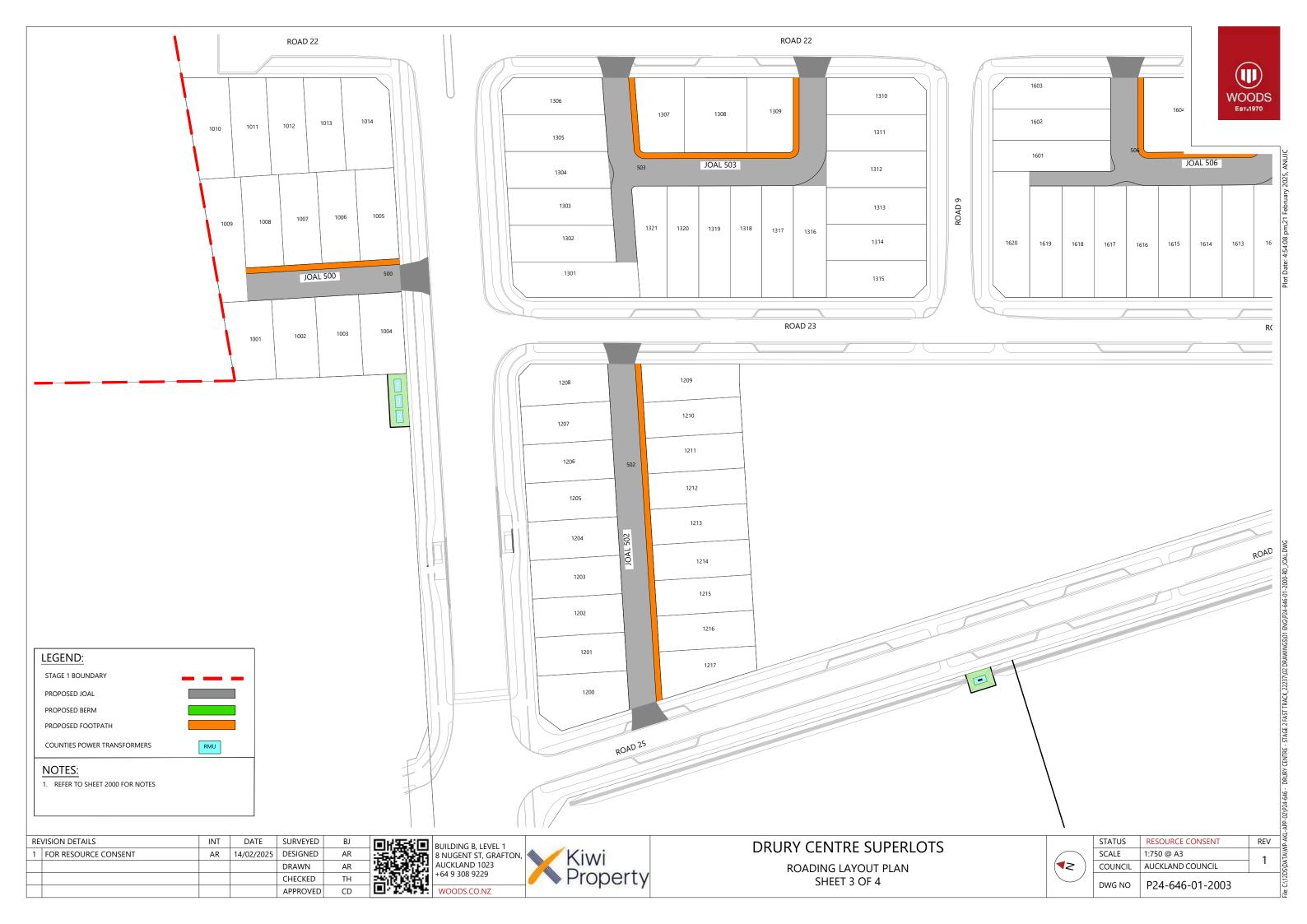


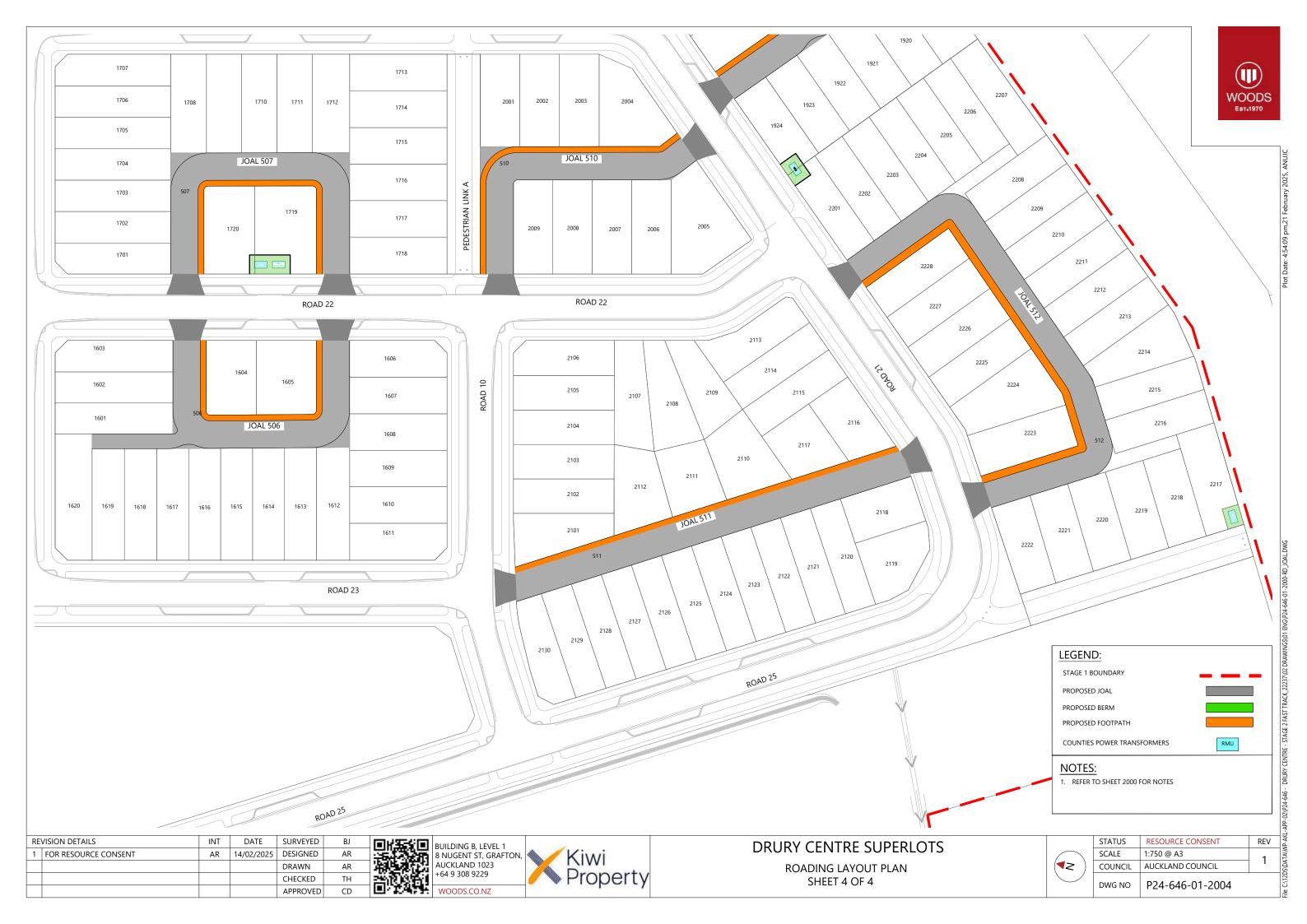
# APPENDIX A DEVELOPMENT PLANS

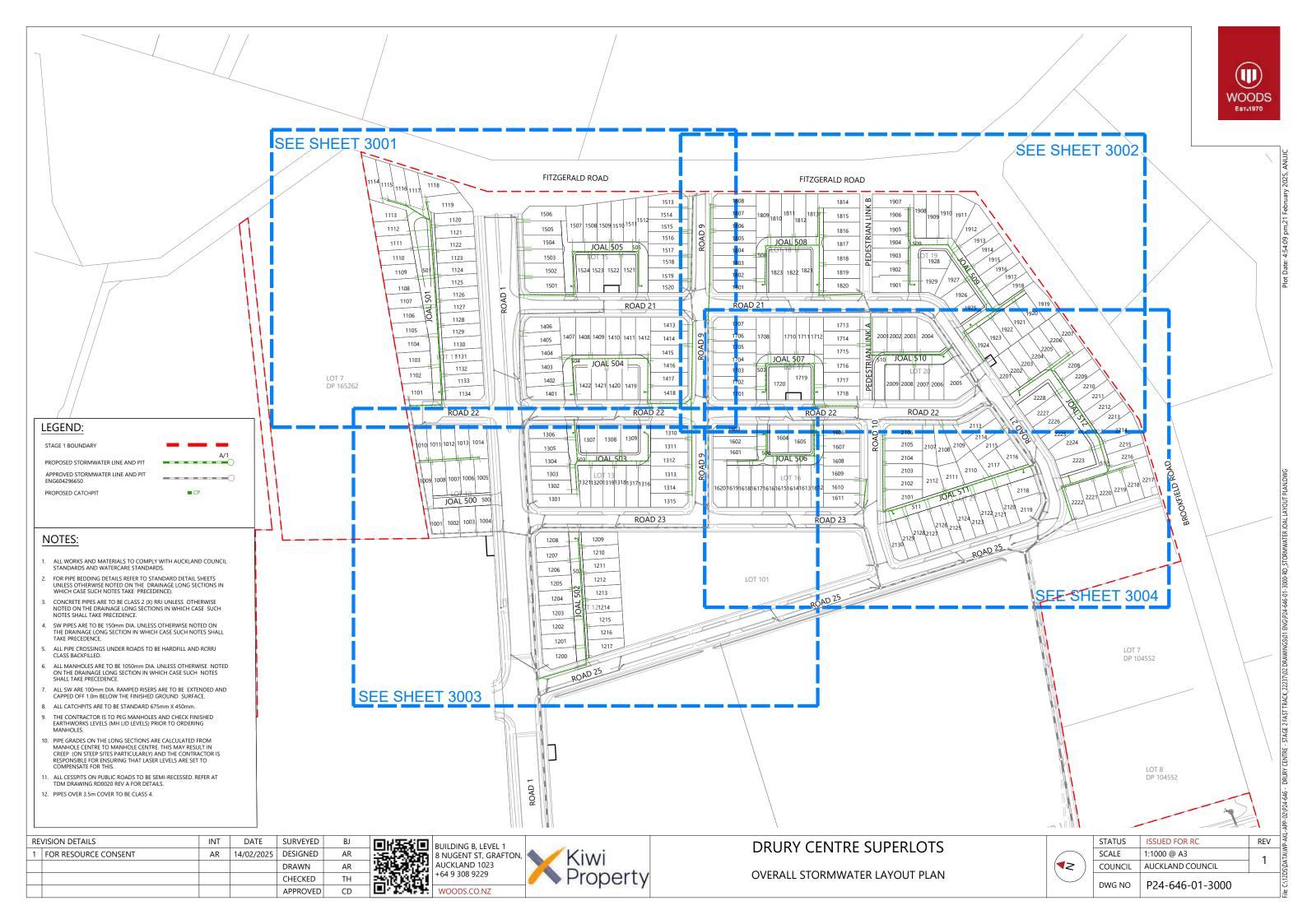


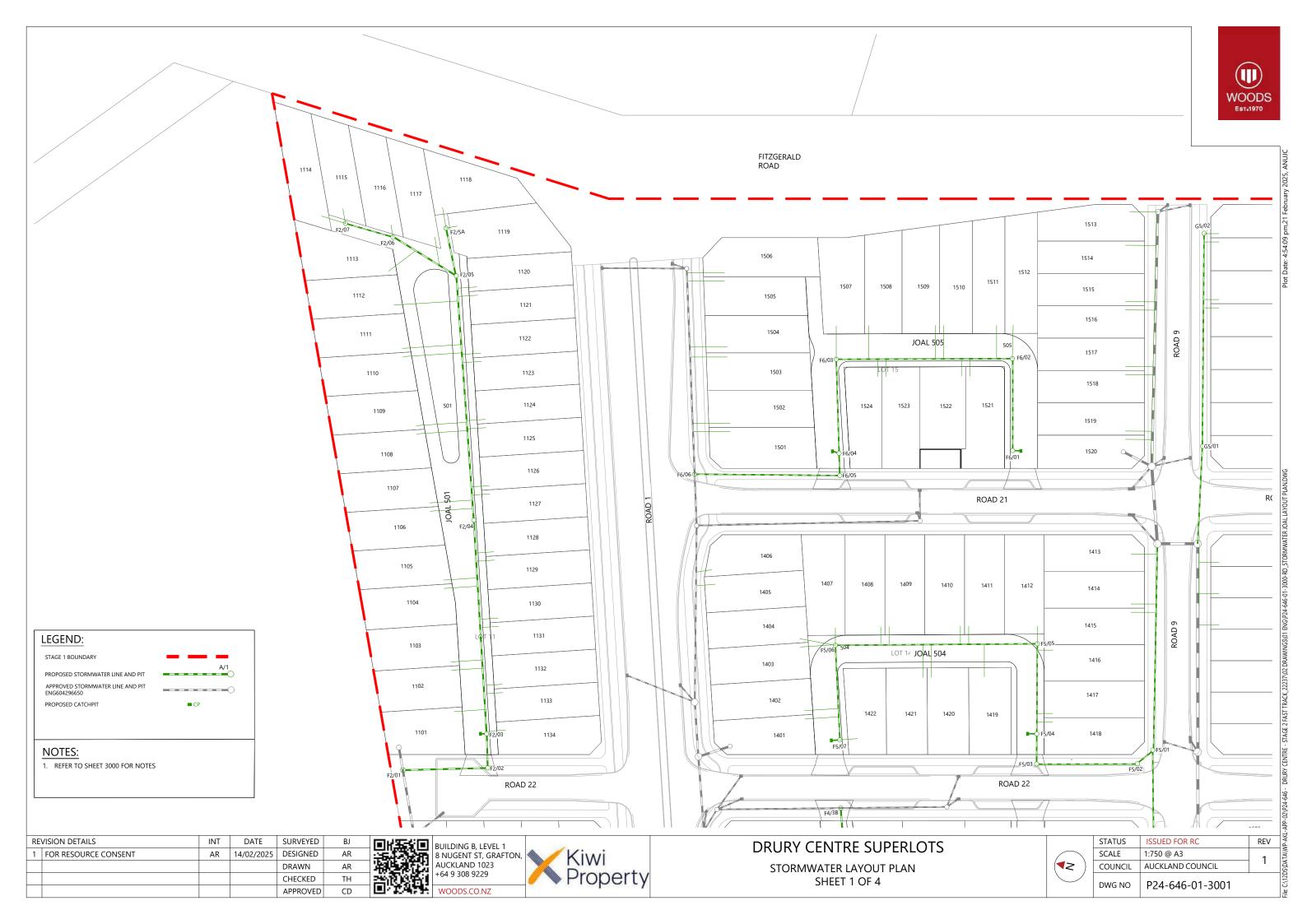


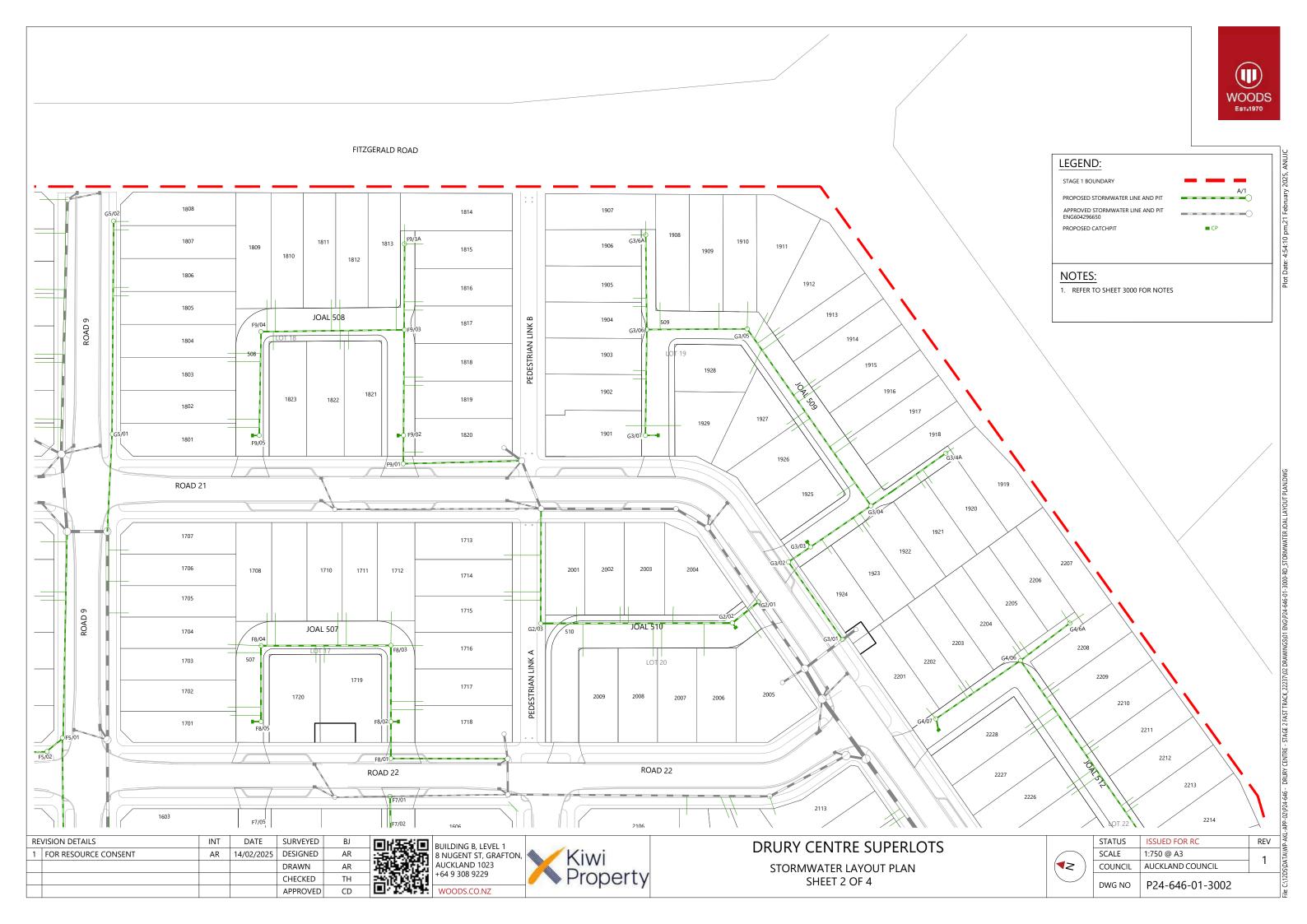


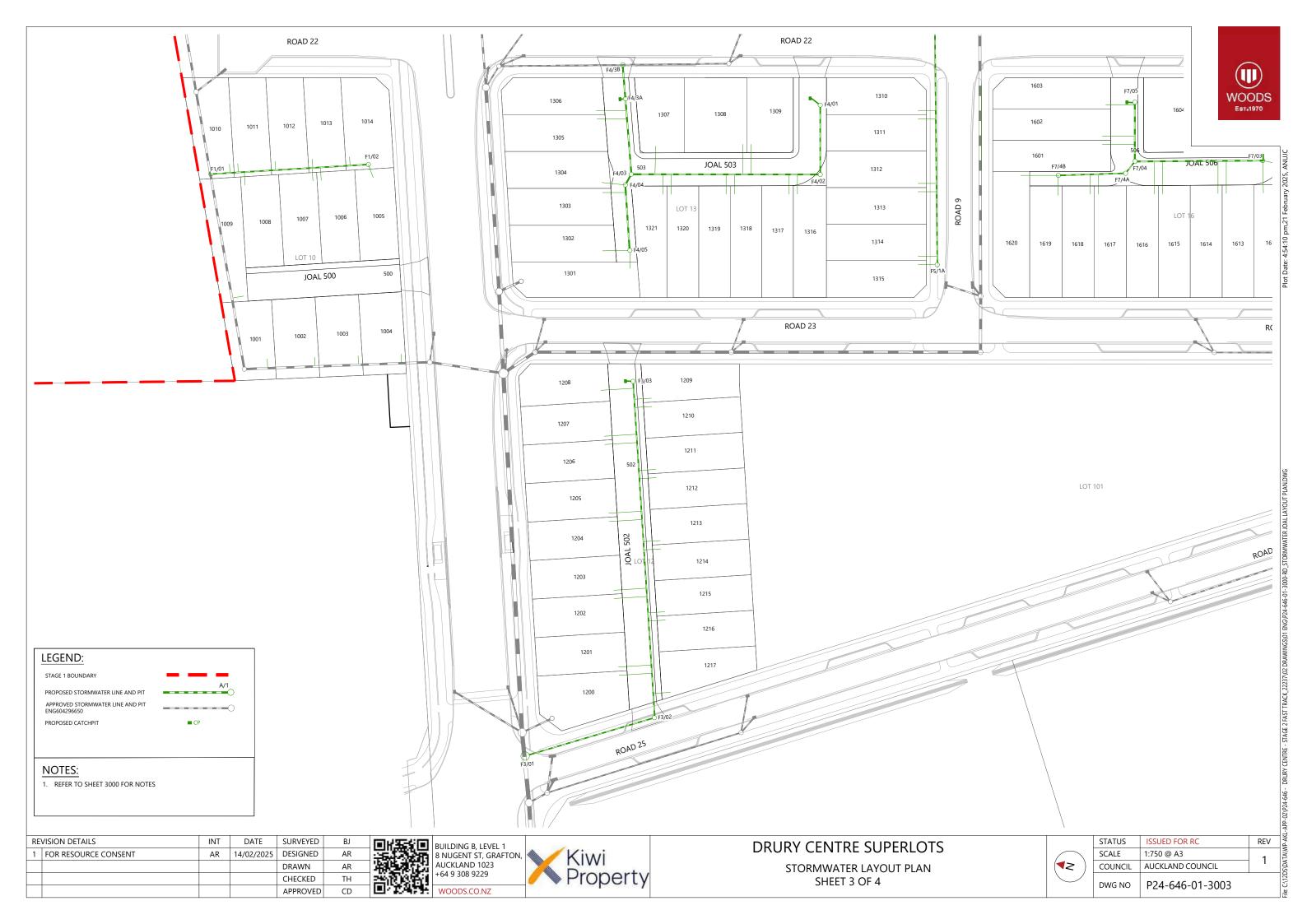


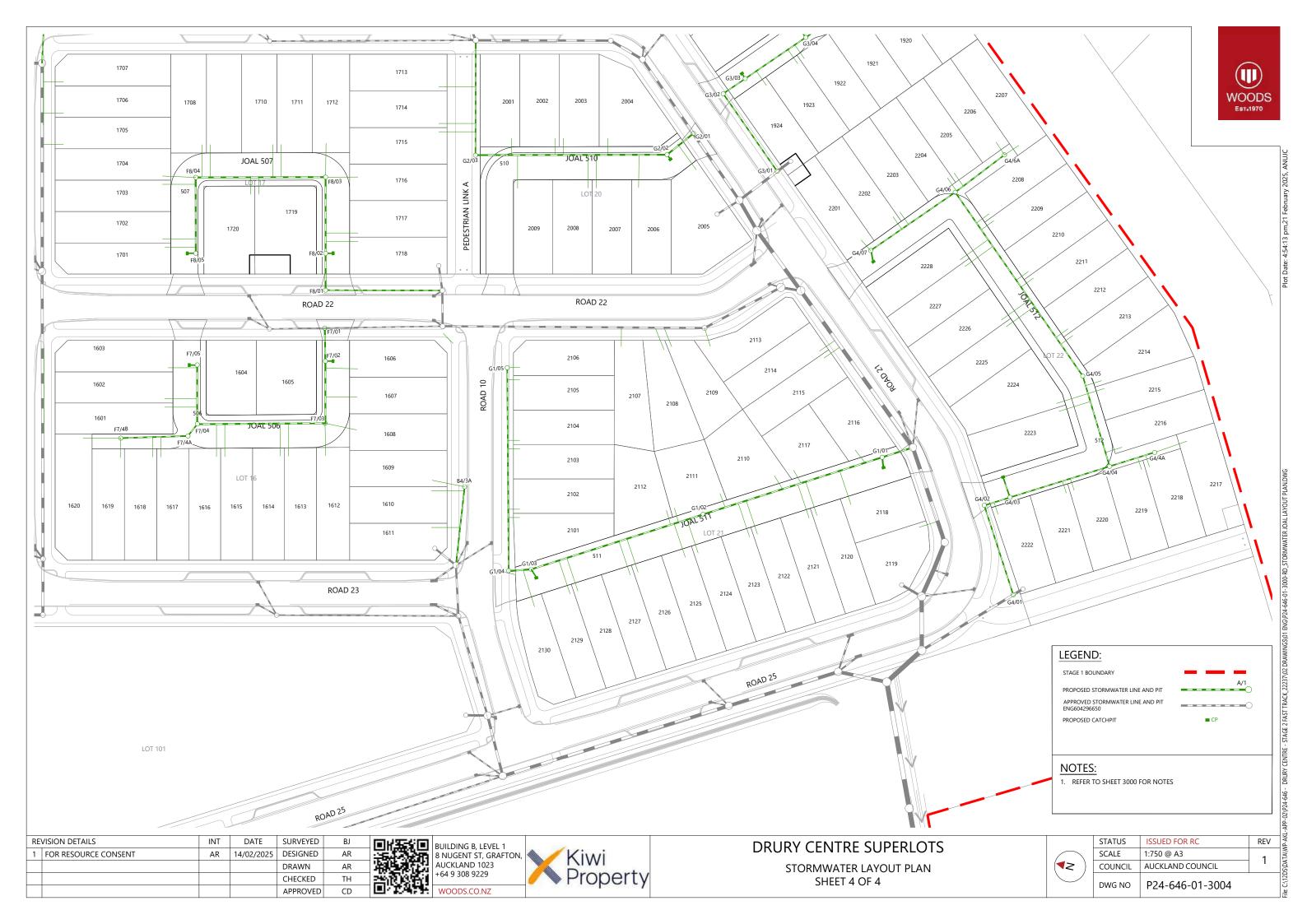


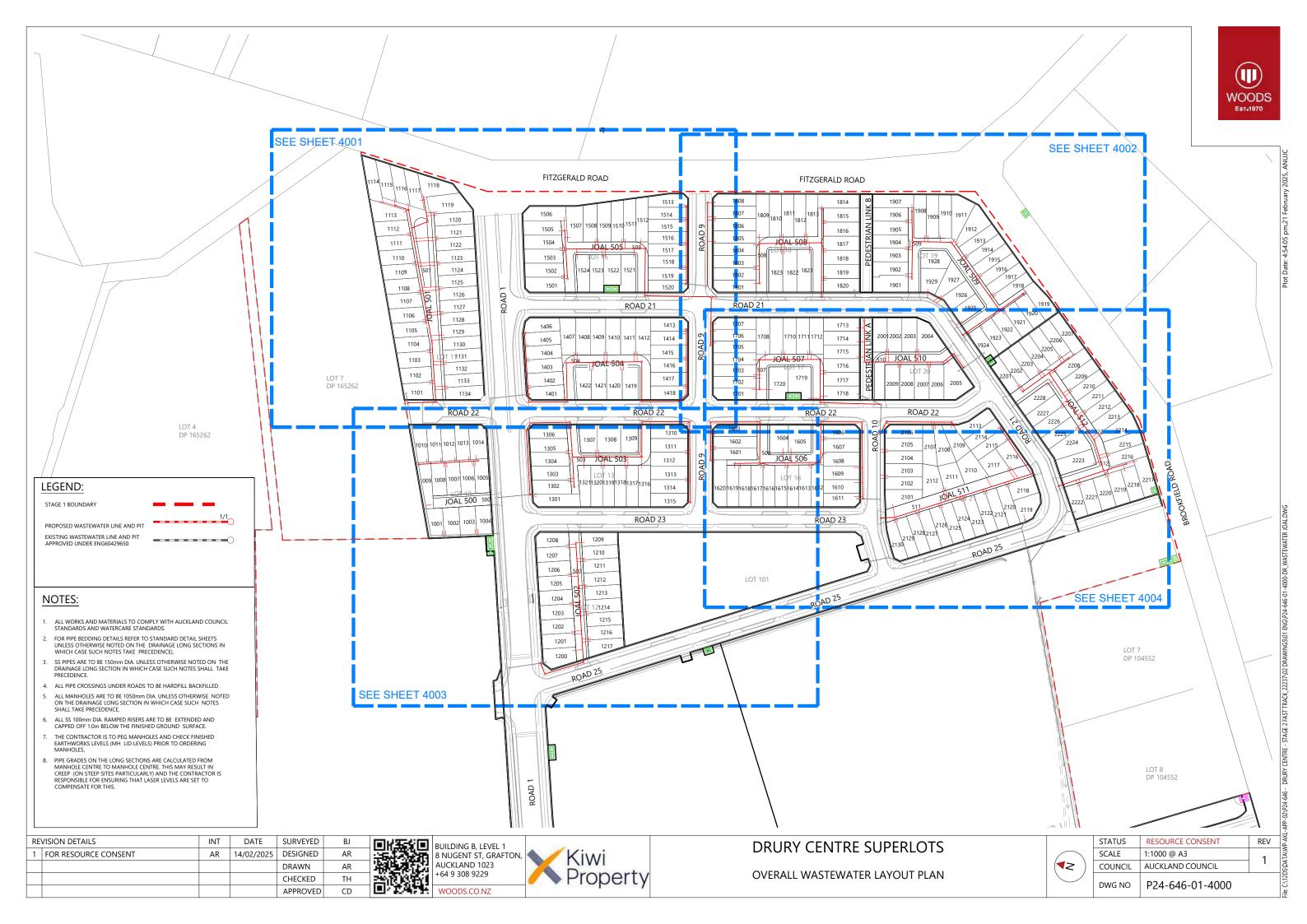




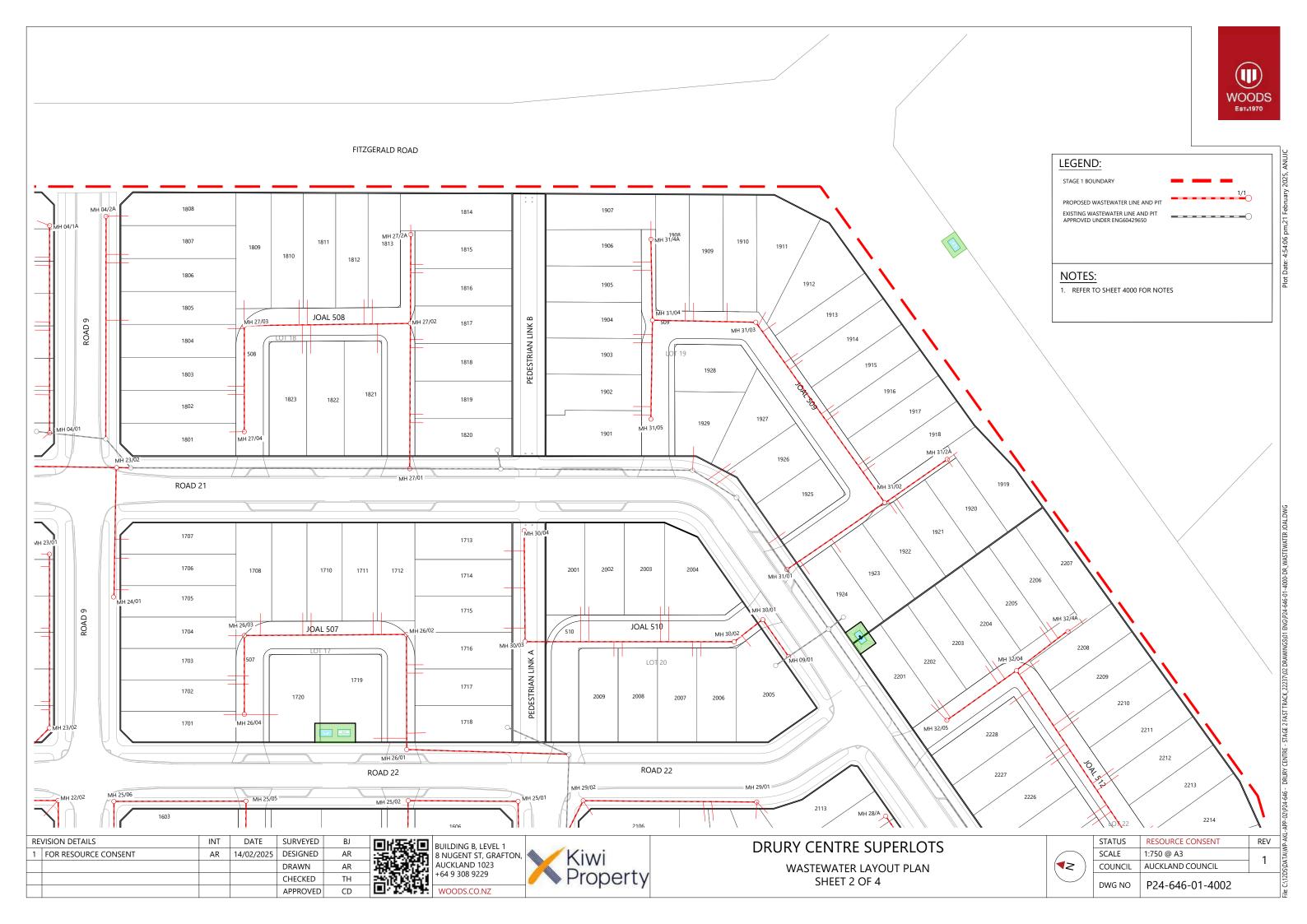


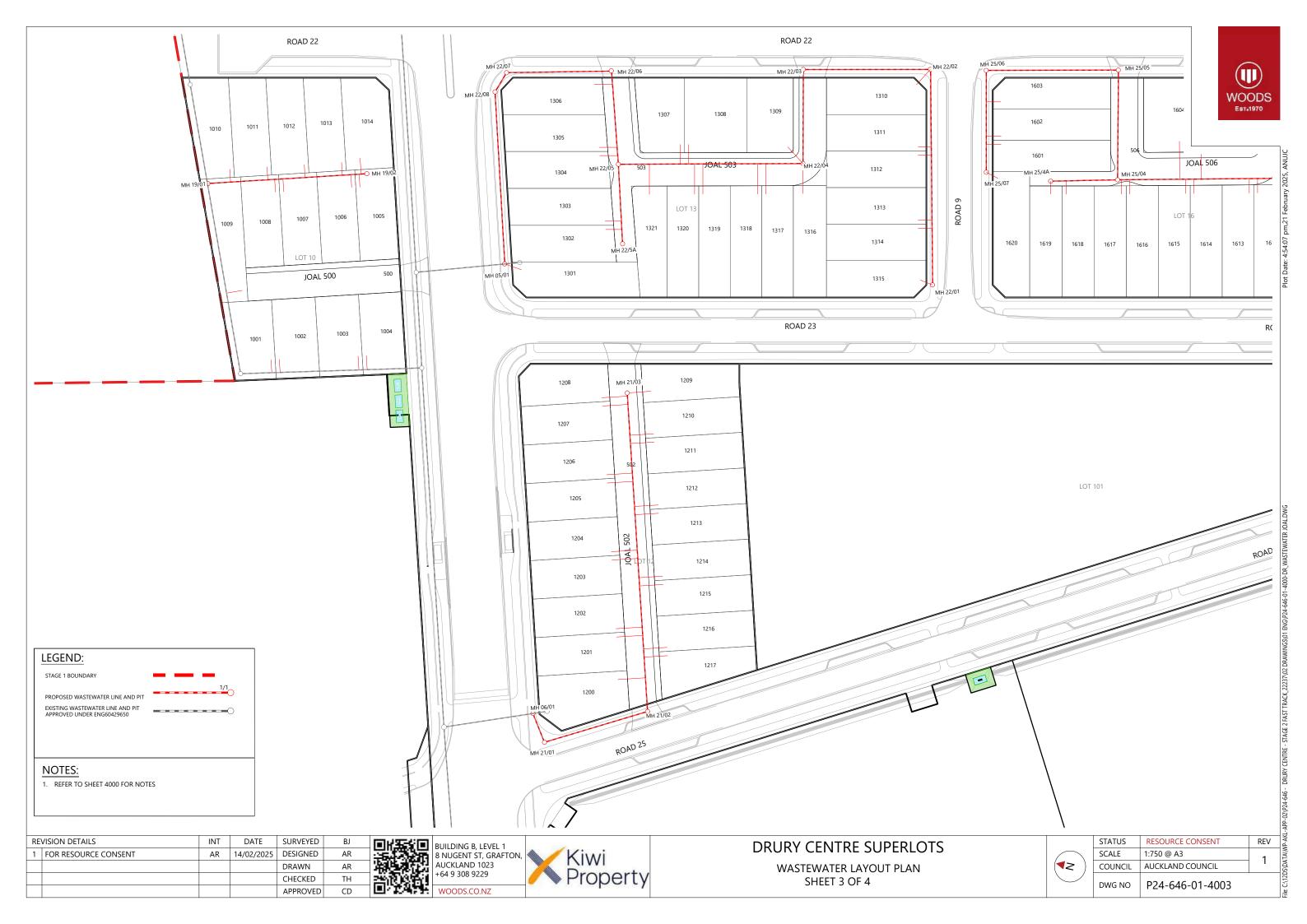


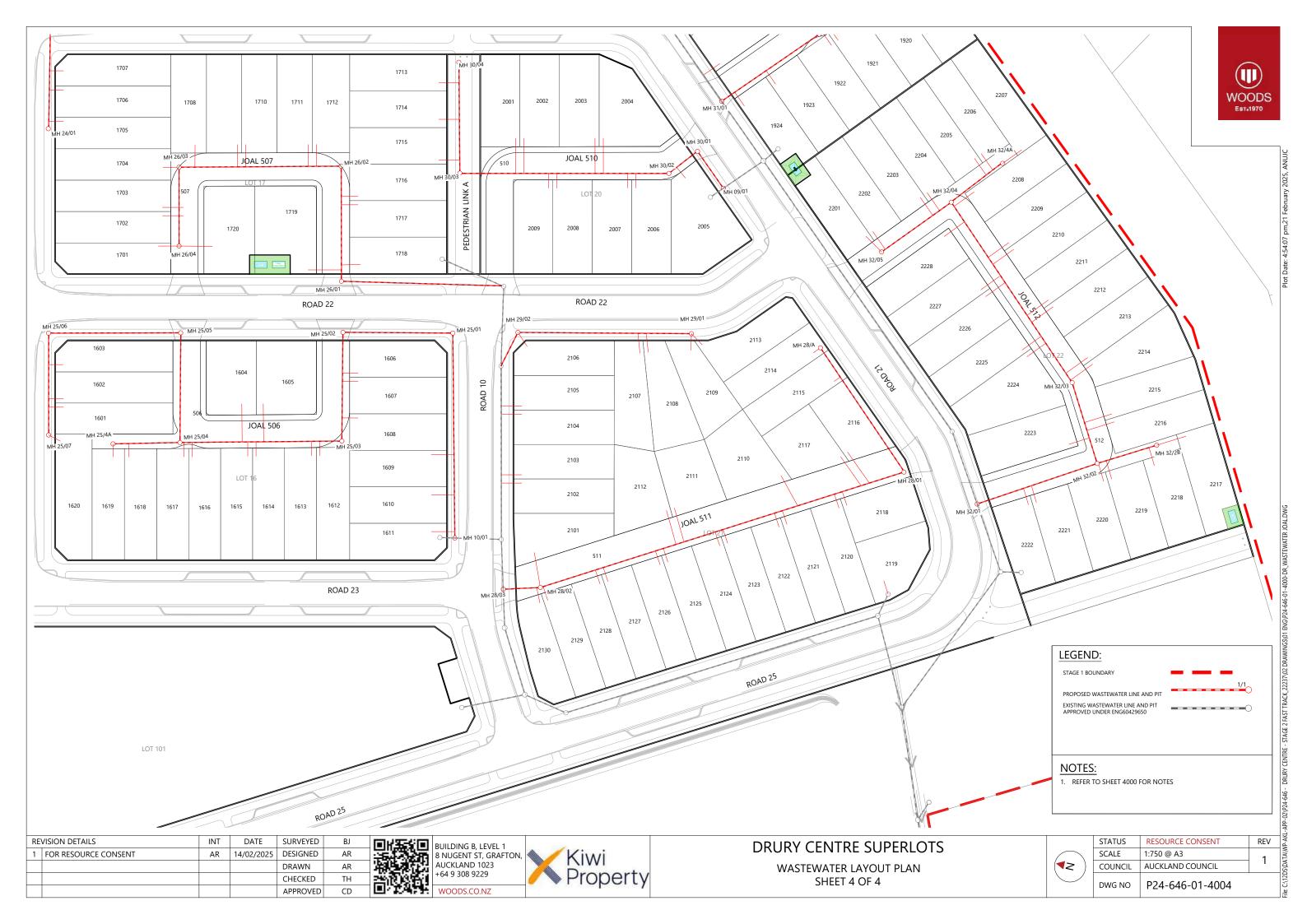














# APPENDIX B GEOTECHNICAL COMPLETION REPORT



2 July 2024

DRURY CENTRE – STAGE 1 EARTHWORKS 133 FITZGERALD ROAD, DRURY

# GEOTECHNICAL COMPLETION REPORT

Kiwi Property Holdings No. 2 Limited

AKS2023-0072AJ Rev 1



AKS2023-0072AJ		
Date	Revision	Comments
01 May 2024	Α	Initial draft for internal review
03 May 2024	В	Final draft for client review
13 May 2024	0	Issued to Client
2 July 2024	1	Issued to Client

	Name	Signature	Position
Prepared by	Shirantha Amarasekera	E Luke	Associate Engineering Geologist
Reviewed by	Larry Goldfarb	Kany Goldfail	Principal Geotechnical Engineer CMEngNZ, CPEng
Authorised by	Sam Gibb	S. G. LL	Principal Geotechnical Engineer CMEngNZ, CPEng







ii



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#### **APPENDICES**

Appendix A: Statement of Professional Opinion on Suitability of Land for Building Construction

Appendix B: Statement of Suitability of Engineered Fill for Lightweight Structures

Appendix C: As-Built Drawings

Appendix D: Aurecon Earthworks QA AND CERTIFICATION

Appendix E: Field Test Data

Appendix F: Inspection Records

Appendix G: Laboratory Test Data

Appendix H: Geotechnical Monitoring Report

Appendix I: Earthworks Practical Completion And Certification Lot 1



#### 1 INTRODUCTION

In accordance with our instructions, this Geotechnical Completion Report (GCR) has been prepared for Kiwi Property Holdings No. 2 Limited as part of the documentation to be submitted to Auckland Council following earthworks to form the residential lots for Stage 1 of the Drury Centre development.

This report covers the construction period from earthworks season 2021 and 2022 through to practical completion of the lots to March 2024. This report is intended to be used for certification purposes for the new lots (listed below):

- 13 new residential lots numbered Lot 10 to Lot 22;
- 6 new roads numbered Road 9, 10, 21 to 23 and 25;
- 1 reserve numbered Lot 101

Stage 1 of the Drury Centre Development is located off 133 Fitzgerald Road, Drury. As can be seen from the asbuilt plans Appendix C, 13 of the lots have been affected by filling as part of the earthworks operations to a maximum depth of approximately 8 metres.

Construction of this subdivision has been undertaken in general accordance with;

- Auckland Council's Resource Consent number BUN60390224 and Engineering Approval letter dated 13 April 2022
- NZS4431:1986 (consent predates 2022 update)
- Auckland Council's Code of Practice for Land Development and Subdivision, Chapter 2 Earthworks and Geotechnical, Version 2.0, May 2023
- Aurecon consented drawing set referenced 510611-0100-DRG-CC-0000, dated 21 May 2021



#### The following project related reports:

Project Documentation - ACCoP		
Report Type	Reference and/or Comments	
Geotechnical Interpretative Report	Aurecon Geotechnical Interpretative Report – 510611- 002-REP-GG-001.Rev5	
Geotechnical Works Specification (earthworks)	Aurecon Standard Earthworks Specification – 510611 Drury Centre Earthworks Specification.Rev1	
Geotechnical Supplementary Report	AKS2023-0071 AG Earthworks Practical Completion and Certification Lot 1 Rev 0	

For the construction of these stages of the development, the following roles were fulfilled as defined in NZS 4431:1986 and the Ministry for the Environment Contaminated Land Management Guidelines:

• Earthworks Designer: Aurecon Ltd (2021 to 2023) & Woods Partners Ltd (2023 to 2024)

Geotechnical Designer & Certifier: Aurecon Ltd (2021 to 2023) & CMW Geotechnical NZ Limited (2023 to

2024)

Recognised Laboratory: Road TestContractor: Ross Reid

As CMW has the role of earthfill Certifier this report has been prepared to cover that aspect of the project work.

#### 1.1 Commercial Lot

At the time of writing this GCR, commercial lot (1) was still currently being finalised with the construction of reinforced earth retaining walls along the eastern property boundary and a segmental retaining wall on the property boundary with 105 Brookfield Road still to be completed. This area of the project and commercial lot will be addressed in a separate GCR upon completion of all retaining structure earthworks associated with commercial lot 1. CMW has completed an Earthworks Practical Completion and Certification for Lot 1, AKS2023-0072AJ, dated 2 July 2024 in which it confirms that all cut to fill earthworks associated to Lot 1 has been completed in accordance with the Earthworks Specification and has provided preliminary foundation design parameters for any future developments for the lot. Practical completion and certification for Lot 1 and the Earthworks Specification has been appended to this GCR for reference.

#### 2 DESCRIPTION OF WORKS

The main bulk earthworks operations commenced between May 2022 and December 2023 by Ross Reid Contractors Ltd. This generally consisted of cutting into the existing land within Lots 10 to 19 and filling in within Lots 20 to 22.

The cut and fill Layout Plan in *Appendix* A shows that cuts of up to 5.5m and fills of up to 3.0m were required to achieve the necessary design levels for the proposed lots. All residential lots have been topsoiled and grassed.

The extent of Earthworks undertaken to date, and that covered by this GCR are shown on the Cut-Fill Surface, located in Appendix A.

Majority of the site works for the residential lots were carried out before CMW were engaged with only minor works carried out around Lot 19. The previous consultant, Aurecon who oversaw the earthworks certification



onsite till May 2023 have provided a Geotechnical Review Report of these works of which CMW have reviewed as part of this GCR.

During the course of the site works the Contractor has submitted all QA testing conducted by RoadTest of the engineered fill (NDM and shear vane testing), which were reviewed and certified by Aurecon and CMW have accepted. Further intrusive investigations comprising top-down hand auger testing were conducted on each residential lot to evaluate the bearing capacity of each lot. The hand augers are presented in *Appendix E* and *Appendix G* as part of the QA testing for the GCR.

#### 3 GEOTECHNICAL QUALITY CONTROL

#### 3.1 Site Observations

During the works, site visits were typically undertaken several times each week to assess compliance with NZS 4431 and project specific design recommendations and specifications.

Site visits were carried out to observe and confirm compliance relating to:

- Adequate topsoil stripping;
- Fill areas prior to the placement of fill materials to ascertain that all mullock, and soft inorganic subsoils had been removed:
- Placement and compaction of engineered fills.

#### 4 QUALITY ASSURANCE TESTING

Quality assurance testing of materials was completed as required by the Geotechnical Works Specification presented in Aurecon's Earthworks Specification, 510611 Drury Centre Earthworks Spec Rev 1, 3 December 2021, presented in *Appendix D*. Test results are presented in Appendix E and Appendix G.

Cohesive Materials (Soil Fill and Soil/ Rock Blended Fill) Compaction Test Criteria for Engineered Filling						
Fill Typo	Air Vo	oids <sup>(1)</sup> Vane Shear Strength <sup>(2)</sup>		Moisture Content <sup>(3)</sup>	Dry Density <sup>(3)</sup>	
Fill Type	Average	Maximum Single Value	Average	Minimum Single Value	Maximum	Minimum
Earth Fill	10%	12%	150 kPa	110 kPa	40%	1.3 t/m <sup>3</sup>
Landscape Fill	TBC by Geotechnical Engineer of case-by-case basis					

<sup>(1)</sup> Air Voids Percentage (as defined in NZS 4402:1986)

While these tests showed on occasions that the contractor was struggling to achieve the required compaction standards with the prevailing site and soil conditions, to the best of our knowledge, all areas of fill were reworked as necessary. Subsequent testing confirmed compliance with the specification.

<sup>(2)</sup> Undrained Shear Strength (Measured by hand shear vane – calibrated using NZGS 2001 method)

<sup>(3)</sup> Moisture content and minimum dry density non-compliance may be accepted on site by the Geotechnical Engineer on a case-by-case basis depending on the nature of the material and the other criteria results.



#### 5 EVALUATION OF COMPLETED EARTHWORKS

#### 5.1 Liquefaction

The liquefaction risk for the lots on this development has been assessed as follows:

- Review of Aurecon's Geotechnical Interpretive Report and Auckland Council GIS maps confirms the damage category to be: Very Low Vulnerability
- In accordance with MBIE/NZGS guidance<sup>1</sup> the liquefaction susceptibility of the soils at this site was assessed with respect to geological age and compositional (soil fabric and density) criteria during initial investigations by Aurecon. Liquefaction assessment was described in the Geotechnical Interpretative Report referenced in Section 5.4 and found a very low risk.

Investigations and analysis by Aurecon were completed in accordance with the Guidance. As a result of that work, the earthworks carried out to date, particularly areas where there has been cut, the earthworks surface has remained within the South Auckland Volcanic Formation (SAVF) and therefore liquefaction is unlikely.

#### 5.2 Land Stability and Erosion

The residential lots have been developed from cutting away a hill on an existing plateau landform to form an earthwork surface that is relatively flat to gently sloping to Fitzgerald Road, the western boundary. As such, the potential for unstable conditions for finished ground profile is negligeable and satisfy ultimate limit state design criteria. The soil parameters for stability analysis were selected from extensive investigation undertaken at the site and from experience in this terrain.

The subdivision scheme layout includes a series of batter slopes to form level terraces for building platforms. The batters include portions of the residential lots with maximum gradients of 1(v) in 3(h. We consider the conditions to be satisfactory for all building platform areas, and we are therefore satisfied that these areas are not subject to the natural stability hazards described in the Building Act.

Along Lot 19, the northwestern boundary (corner of Fitzgerald and Brookfield Road), the finished surface beneath the two roads has resulted in a cut slope varying in height from 1.0m to 2.0m. We consider this stability of the cut to be negligeable based on the soil conditions seen and experience with stability in this terrain. On all steep land, including on engineered batter slopes, surface stability can be compromised by indiscriminate disposal of stormwater onto the ground surface and/ or by removal of vegetation.

Building and landscape designers must ensure that all runoff from solid surfaces is directed into the stormwater system. It is also important that care is paid to the disposal of stormwater during construction so that concentrated discharges (e.g. from unconnected spouting) are not directed towards steep ground.

Depths of mulch and topsoil applied to sloping areas should be limited to less than 150mm to minimise the risks of saturation leading to localised slumping on batter face. Wherever practical on such land, and particularly on steep batters, existing vegetation and grass cover should be well maintained. Any vegetation cleared beyond the immediate area of building platforms for temporary construction purposes should be replanted or replaced as soon as possible. The roots of an established vegetation cover can serve to bind the surface soils while the foliage can reduce rain infiltration and soil saturation, resulting in better resistance to erosion and shallow slumping.

#### 5.3 Uncertified Temporary Filling

At the time of completing this GCR all Residential Lots have environmental clean water diversion control bunds constructed on the perimeter of the Lots. For Lots 12 to 14, temporary staging for topsoil screening had been

<sup>1</sup> Earthquake Geotechnical Engineering Practice, Module 3: Identification, assessment and mitigation of liquefaction hazards", (November 2021)



taking place with a number of topsoil stockpiles present on the Lots. It is anticipated that all uncertified filling will be removed from the Lots prior to hand over to the residential builder and in such a case a certified Geotechnical Engineer will need to confirm Lots are cleared in accordance with the requirements of NZS 3604 and ACCoPs, and the anticipated final levels are met as shown in drawing P23-315-01-1100-EW, *Appendix C*.

The areas containing these deposits are covered by the Specific Design Zone (uncertified fill) check this is listed in SOPO and descriptions of the restrictions are contained in our Opinion on Suitability in *Appendix A*.

#### 5.4 Fill Induced Settlement

The majority of the filling on this stage of the development was placed between December 2023 and February 2024. A series of settlement markers was installed in areas of deeper fill at its completion and have been periodically monitored for both horizontal and vertical movements. Horizontal changes have been noted to be within the survey accuracy limits, while vertical movements are depicting seasonal shrink/ swell variations as anticipated. Results of the monitoring are provided in *Appendix E* and generally show a plateauing of results.

On the basis of the relatively minor magnitude of fill depths on this site, together with the elapsed time since it was placed, we consider that remaining post-construction settlements will be within code limits.

#### 5.5 Service Line Trenches

At the time of writing this GCR civil works, sanitary sewer and stormwater services have not been constructed including the service trenching required for installation of these services.

As is normal on all subdivisions, building developments involving foundations within a 45-degree zone of influence from pipe inverts will require engineering input. The Auckland Council drawing referenced SW22 provided in *Appendix B* extracted from Chapter 4 of the Auckland Council Code of Practice for Land development and Subdivision depicts their requirements for stormwater pipes. Details for water and wastewater pipes are available in the Watercare COP1 - General Requirements and Procedures. It is anticipated that the majority of lots will have service trenches within the lots. The resulting restrictions are presented in our Opinion on Suitability in *Appendix A*.

#### 5.6 Groundwater

The extensive investigation carried out prior to any earthworks encountered groundwater within the basalt layer, at depths that would unlikely affect the bulk earthworks. This was confirmed in our observation records along with Aurecon's as groundwater was not encountered during the bulk earthworks.

Based on our work to date we anticipate groundwater levels remaining well below the depth of influence of anticipated earthworks and foundation works for NZS 3604 type dwellings.

#### 5.7 Design of Shallow Foundations

#### 5.7.1 Bearing Capacity

Once bulk earthworks and top-soiling of the building platforms had been completed, our staff drilled hand auger boreholes on platforms in natural ground to determine representative finished ground conditions and hence evaluate likely foundation options for future building development. Our assessments of bearing capacity for the design of shallow foundations on each building platform are contained in our Opinion on Suitability in *Appendix A*.

As detailed in our Opinion on Suitability, in general the residential lots have a bearing capacity of 300kPa. Under AS2870, the material is considered H1 due to shrinkage limit.

If higher geotechnical ultimate bearing capacities are required than have been specified, further specific site investigation and design of foundations should be carried out prior to Building Consent application.



#### 5.7.2 Foundation Settlements

At the bearing pressures specified in *Appendix A* and subject to the design requirements for soil expansiveness provided below, differential settlement of shallow foundations for buildings designed in accordance with NZS 3604 (including the 600mm subfloor fill depth limit) should be within code limits.

#### 5.7.3 Soil Expansiveness Classification

Seasonal soil moisture variations within most clay-rich soils typically result in the soil swelling during winter months and then shrinking during summer months. These seasonal movements can cause issues such as cracking of concrete floors, brittle cladding and masonry walls or distortion of building frames causing doors and windows to jam from differential settlement. The effects are further compounded by local influences that worsen differential movements. These may include growth of high demand trees and shrubs that cause localised soil drying or either leaking pipes or tree root removal, leading to localised wetting.

The potential effects need to be managed in a combination of appropriate:

- classification of the level of risk
- design of foundations
- management of soil moisture conditions by contractors during construction
- management of landscaping and plantings by homeowners throughout a building's lifetime

Testing on 4 samples was completed in accordance with the requirements of NZS 3604 and ACCoPs. All testing is currently being performed by Construction Science, a testing laboratory accredited by IANZ for the tests undertaken.

The purpose for the testing will confirm:

- The extent of the soils tested are expansive in terms of the NZS 3604 definition and whether therefore outside the definition of "good ground".
- The samples tested demonstrated a range of expansivity characteristics.

Results of our assessment of the maximum characteristic surface movement (ys) for each lot are contained in our Statement of Opinion on Suitability of Land in *Appendix A*.

#### 5.7.4 Site (Seismic) Class

Our assessments of NZS 1170.5 site Class(es) is provided in our Opinion of Suitability and the Summary Table, both in *Appendix A*.

#### 5.8 Topsoil Depths

Topsoil depths have been checked by the drilling of a borehole in the approximate centre of the building platform on each lot. The results are considered indicative for each lot, but may be subject to variations. Topsoil depths are between 100 and 400mm on these stages of the development.

Site specific findings are contained in our Opinion on Suitability Summary in *Appendix A*. It is possible that further levelling works have been undertaken since the investigations and accordingly, we strongly recommend that lot purchasers complete their own checks of topsoil depths.

#### 5.9 Site Preparation During Construction

Foundation contractors need to be aware of the extreme damage potentially caused by expansive soils and the imperativeness of maintaining optimum moisture contents in all footing excavations and across building platform subgrades between the time of excavation and the pouring of concrete. Pouring foundations on dry, desiccated ground in summer months can lead to heaving and cracking, requiring extensive repairs or even



complete house re-builds. Similarly, where perimeter foundations have been treated but floor slabs have been poured on dry ground, infiltration of moisture via pipe bedding can lead to localised heave, uplift and significant slab damage.

Remedial actions that may be appropriate include combinations of platform protection with a hard fill layer, pouring of a blinding layer of concrete in footing bases and soaking of the building platform with sprinklers for an extended period.

#### 5.10 Site Maintenance and Landscaping

Due to potential soil expansivity, landowners must be mindful of the potential impacts of planting or removal of high water demand plants. Where their roots may extend close to footings (i.e. within a lateral distance of 1.5 times the mature tree height), these actions can lead to significant settlement or heave damage.

For a comprehensive understanding of the potential effects of expansive soils, maintenance recommendations and vegetation management information, we strongly recommend that land owners obtain a copy of CSIRO publication BTF 18 (Foundation Maintenance and Footing Performance – A Homeowners Guide) that is available online.

#### 6 CLOSURE

Additional important information regarding the use of your CMW report is provided in the 'Using your CMW Report' document attached to this report.

This report has been prepared for use by Kiwi Property Holdings No. 2 Limited in relation to the Drury Centre – Stage 1 Earthworks 133 Fitzgerald Road, Drury project in accordance with the scope, proposed uses and limitations described in the report. Should you have further questions relating to the use of your report please do not hesitate to contact us.

Although regular site visits have been undertaken for observation, for providing guidance and instruction and for testing purposes, the geotechnical services scope did not include full time site presence. To this end, our Opinion on Suitability in *Appendix A* and our Suitability Statement in *Appendix B* also rely on the Contractors' work practices and assumes that when we have not been present to observe the work, it has been completed to high standards and in accordance with the drawings, instructions and consent conditions provided to them.

Similarly, we assume that all as-built information and other details provided to the Client and/ or CMW by other members of the project team are accurate and correct in all respects.

Where a party other than Kiwi Property Holdings No. 2 Limited seeks to rely upon or otherwise use this report, the consent of CMW should be sought prior to any such use. CMW can then advise whether the report and its contents are suitable for the intended use by the other party.



#### USING YOUR CMW GEOTECHNICAL REPORT

Geotechnical reporting relies on interpretation of facts and collected information using experience, professional judgement, and opinion. As such it generally has a level of uncertainty attached to it, which is often far less exact than other engineering design disciplines. The notes below provide general advice on what can be reasonably expected from your report and the inherent limitations of a geotechnical report.

#### Preparation of your report

Your geotechnical report has been written for your use on your project. The contents of your report may not meet the needs of others who may have different objectives or requirements. The report has been prepared using generally accepted Geotechnical Engineering and Engineering Geology practices and procedures. The opinions and conclusions reached in your report are made in accordance with these accepted principles. Specific items of geotechnical or geological importance are highlighted in the report.

In producing your report, we have relied on the information which is referenced or summarised in the report. If further information becomes available or the nature of your project changes, then the findings in this report may no longer be appropriate. In such cases the report must be reviewed, and any necessary changes must be made by us.

#### Your geotechnical report is based on your project's requirements

Your geotechnical report has been developed based on your specific project requirements and only applies to the site in this report. Project requirements could include the type of works being undertaken; project locality, size and configuration; the location of any structures on or around the site; the presence of underground utilities; proposed design methodology; the duration or design life of the works; and construction method and/or sequencing.

The information or advice in your geotechnical report should not be applied to any other project given the intrinsic differences between different projects and site locations. Similarly geotechnical information, data and conclusions from other sites and projects may not be relevant or appropriate for your project.

#### Interpretation of geotechnical data

Site investigations identify subsurface conditions at discrete locations. Additional geotechnical information (e.g. literature and external data source review, laboratory testing etc) are interpreted by Geologists or Engineers to provide an opinion about a site specific ground models, their likely impact on the proposed development and recommended actions. Actual conditions may differ from those inferred to exist due to the variability of geological environments. The actual interface between materials may be far more gradual or abrupt than assumed based on the facts obtained. Nothing can be done to change the actual site conditions which exist, but steps can be taken to reduce the impact of unexpected conditions. Interpretation of factual data can be influenced by design and/or construction methods. Where these methods change review of the interpretation in the report may be required.

#### Subsurface conditions can change

Subsurface conditions are created by natural processes and then can be altered anthropically or over time. For example, groundwater levels can vary with time or activities adjacent to your site, fill may be placed on a site, or the consistency of near surface conditions might be susceptible to seasonal changes. The report is based on conditions which existed at the time of investigation. It is important to confirm whether conditions may have changed, particularly when large periods of time have elapsed since the investigations were performed.

#### Interpretation and use by other design professionals

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a geotechnical report. To help avoid misinterpretations, it is important to retain the assistance of CMW to work with other project design professionals who are affected by the contents of your report. CMW staff can explain the report implications to design professionals and then review design plans and specifications to see that they have correctly incorporated the findings of this report.

#### Your report's recommendations require confirmation during construction

Your report is based on site conditions as revealed through selective point sampling. Engineering judgement is then applied to assess how indicative of actual conditions throughout an area the point sampling might be. Any assumptions made cannot be substantiated until construction is complete. For this reason, you should retain geotechnical services throughout the construction stage, to identify variances from previous assumption, conduct additional tests if required and recommend solutions to problems encountered on site.

A Geotechnical Engineer, who is fully familiar with the site and the background information, can assess whether the report's recommendations remain valid and whether changes should be considered as the project develops. An unfamiliar party using this report increases the risk that the report will be misinterpreted.

#### **Environmental Matters Are Not Covered**

Unless specifically discussed in your report environmental matters are not covered by a CMW Geotechnical Report. Environmental matters might include the level of contaminants present of the site covered by this report, potential uses or treatment of contaminated materials or the disposal of contaminated materials. These matters can be complex and are often governed by specific legislation.

The personnel, equipment, and techniques used to perform an environmental study can differ significantly from those used in this report. For that reason, our report does not provide environmental recommendations. Unanticipated subsurface environmental problems can have large consequences for your site. If you have not obtained your own environmental information about the project site, ask your CMW contact about how to find environmental risk-management guidance.



# APPENDIX A: STATEMENT OF PROFESSIONAL OPINION ON SUITABILITY OF LAND FOR BUILDING CONSTRUCTION



## STATEMENT OF PROFESSIONAL OPINION ON SUITABILITY OF LAND FOR BUILDING CONSTRUCTION

Development: Stage 1 of the Drury Centre Development Developer: Kiwi Property Holdings No. 2 Limited

Location: Drury

I, Larry Goldfarb, of CMW Geotechnical NZ Limited, Auckland, hereby confirm that:

- 1. As a Chartered Professional Engineer experienced in the field of geotechnical engineering, I am a Geoprofessional as defined in clause 1.2.2 of NZS 4404:2010 and was retained by the Developer as the geoprofessional on the above development.
- 2. The extent of preliminary investigations carried out to date are described in the Aurecon Geotechnical Interpretative Report referenced 510611-002-REP-GG-001.Rev5, dated 4 October 2022. The conclusions and recommendations of those documents have been re-evaluated in the preparation of this report. The extent of my inspections and those under my auspices during construction, and the results of all tests and/ or evaluations carried out are as described in my Geotechnical Completion Report dated 1 May 2024.
- 3. I have relied on the Earthworks QA and Certification by Aurecon provided in *Appendix B* that confirms that the earth fills shown in *Appendix C*, drawing number P23-315-01-1270-AB for Lots 12, 13 and 16 to 22 have been placed in compliance with the requirements of Auckland Council and my specification. Further to the above by Aurecon, my certification of the earth fills placed on this site for Lot 10, 11, 14

and 15 is contained in *Appendix B* and have been placed in general compliance with the requirements of Auckland Council and my specification.

- 4. In my professional opinion, not to be construed as a guarantee, I consider that:
  - a. The completed earthworks take into account land slope and foundation stability considerations on the building platform areas-
  - b. A geotechnical ultimate bearing capacity of 300 kPa may be assumed for shallow foundation design on the building platforms of Lots 10 to 22 inclusive.
  - c. The site (seismic) subsoil class for each lot has been assessed in accordance with NZS1170.5:2004 Clause 3.1.3 from borelogs that included measurements of geotechnical properties. Our assessment is that lots 10 to 22 are Class C- shallow soil.

d.

Assessr	Assessment of Characteristic Surface Movements and Design Classes for NZS 3604 Compliant Buildings				
Lots	Assessed Maximum Characteristic Surface Movement (Ys) for 500 Year Design (mm)	Suitable NZBC B1/AS1 Expansivity Class for Design	Suitable AS2870-2015 Class for Design		
10 to 22	67	H (highly)	H1		

#### Notes:

B1/AS1 design applies to a limited range of building sizes, shapes and materials within the scope of NZS3604 and applies only to floor design with strip footings. In all other cases, AS2870 design or specific design should be adopted.



Prior to the introduction of the B1/AS1 design information in November 2019, minimum foundation depths recommended as appropriate by geotechnical consultants in Auckland for shallow footing design under AS2870 were typically of the order of 750mm for Class H1.

- e. No building development should take place within the 45-degree zone of influence of stormwater or sewer line or manhole inverts unless endorsed by specific design and by construction inspections undertaken by a Chartered Professional Engineer experienced in geomechanics to ensure that lateral stability and differential settlement issues are addressed and that building loads are transferred beyond the influence of pipes and trench backfills. A copy of drawing SW22 extracted from Chapter 4 of the Auckland Council Code of Practice for Land development and Subdivision this document is provided in *Appendix B* for clarification. Details for water and wastewater pipes are available in the Watercare COP1 General Requirements and Procedures.
- f. On the basis of the earth fill certification and subject to the geotechnical limitations, restrictions and recommendations contained in clauses 4(a), 4(b), 4(c), 4(d) and 4(e) above:
  - The filled and natural ground is generally suitable for buildings constructed in accordance with NZS 3604 and the requirements of either NZBC Clause B1/AS1 where appropriate, or AS2870 for the expansive soil class associated with the characteristic surface movement. Alternatively, a specific foundation and structural design may be undertaken by a Chartered Professional Engineer.
  - Specific site investigations, design modifications and construction inspections should be carried out as necessary by a Chartered Professional Engineer, experienced in geomechanics, for all buildings exceeding these limitations, but in any event, we consider it prudent for all land owners to engage a Chartered Professional Engineer to undertake site specific investigation and foundation design with a view to optimising bearing capacities, design loads, earthworks and retaining walls.
- 5. Road subgrades have been formed with appropriate regard for slope stability and settlement risks.
- 6. Reserve areas have been formed with appropriate regard for slope stability and seepage risks.

The following table summarises the conditions on each of the residential lots.

For and on behalf of CMW Geosciences

Kary Goldfarl

Larry Goldfarb

Principal Geotechnical Engineer CMEngNZ, CPEng



	Table 1: GCR Summary Table					
Condition	Geotechnical Ultimate Bearing Capacity (kPa)	NZS 1170.5 Site (seismic) Class	AS2870 Expansive Class	Service Lines Restrictions	Indicative Topsoil Depth (mm)	Specific Design Zone (uncertified fill)
GCR SOPO Clause	4(b)	4(c)	4(d)	4(e)		
Lot number						
10	300	С	H1	<b>~</b>	400	<b>~</b>
11	300	С	H1	~	300	<b>~</b>
12	300	С	H1	~	-	<b>~</b>
13	300	С	H1	<b>~</b>	100	<b>~</b>
14	300	С	H1	~	-	<b>~</b>
15	300	С	H1	<b>~</b>	0	<b>~</b>
16	300	С	H1	<b>~</b>	150	<b>~</b>
17	300	С	H1	<b>~</b>	150	<b>~</b>
18	300	С	H1	~	150	<b>~</b>
19	300	С	H1	<b>~</b>	200	<b>~</b>
20	300	С	H1	~	150	<b>~</b>
21	300	С	H1	~	250	<b>~</b>
22	300	С	H1	~	300	<b>~</b>



# APPENDIX B: STATEMENT OF SUITABILITY OF ENGINEERED FILL FOR LIGHTWEIGHT STRUCTURES



# STATEMENT OF SUITABILITY OF ENGINEERED FILLS FOR LIGHTWEIGHT STRUCTURES

To: Auckland Council

Development: Stages 1 of the Drury East Development

Land Title(s): Lot 1, Lot 3, Lot 4 DP 57466, Lot 1 DP 101367 & Lot 1 DP 87159

Location: 133 Fitzgerald Road, Drury

Resource Consent Nos: BUN60390224

Developer: Kiwi Property Holdings No. 2 Limited

Geotechnical Designer: Dr Jan Kupec of Aurecon

Certifier: Larry Goldfarb of CMW Geotechnical NZ Limited

This Statement of Suitability is provided as an appendix to the CMW Geosciences Geotechnical Completion Report referenced in the page footer below, that also contains all as-built plans, inspection and test plan, geotechnical works specification, test results and test inspection records relevant to the work completed.

- 1. I, Larry Goldfarb, confirm that I am qualified as a certifier as defined in NZS4431:1986.
- 2. During this work, I was retained as certifier and I or my certifier's representative undertook inspections and testing as documented in the Geotechnical Completion Report.
- 3. I am satisfied that the engineered fill shown in the attached as-built survey was placed, compacted and tested in accordance with the attached specification and that all variations and non-compliances have been documented in the Geotechnical Completion report.
- 4. Based on the information available, I certify that, to the best of my knowledge, the intent of the geotechnical designer (as presented in the design, drawings and Geotechnical Works Specification) has been achieved.
- 5. The fill areas shown on the Wood Partners Ltd as-built cut and fill plan(s) attached are considered suitable for development as per NZS 3604 subject to any other restrictions described in the Geotechnical Completion Report by the Geotechnical Designer.
- 6. This certification does not remove the necessity for normal inspection and design of foundations as would be made in natural ground.

For and on behalf of CMW Geosciences

Lary Goldfarl

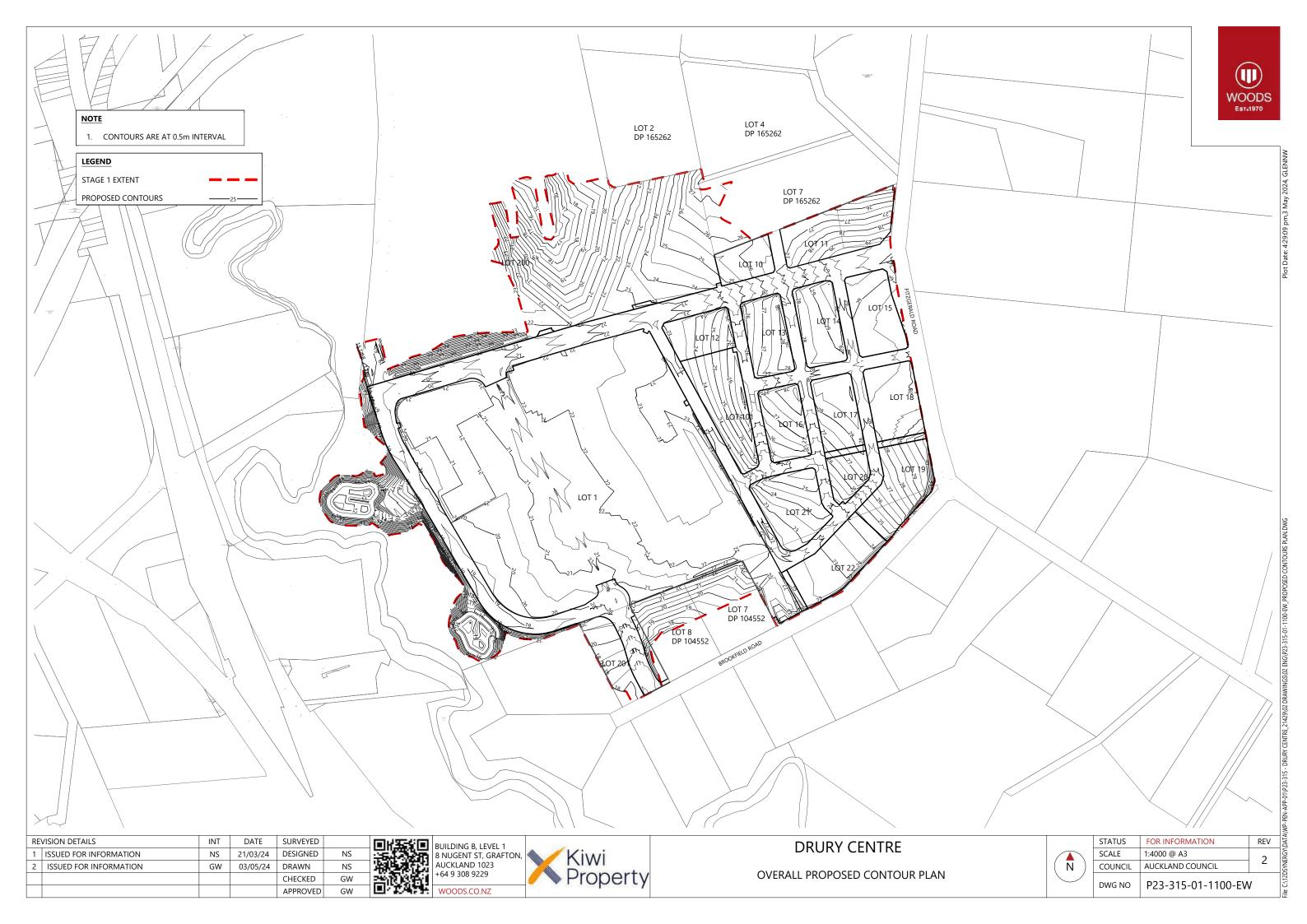
Larry Goldfarb

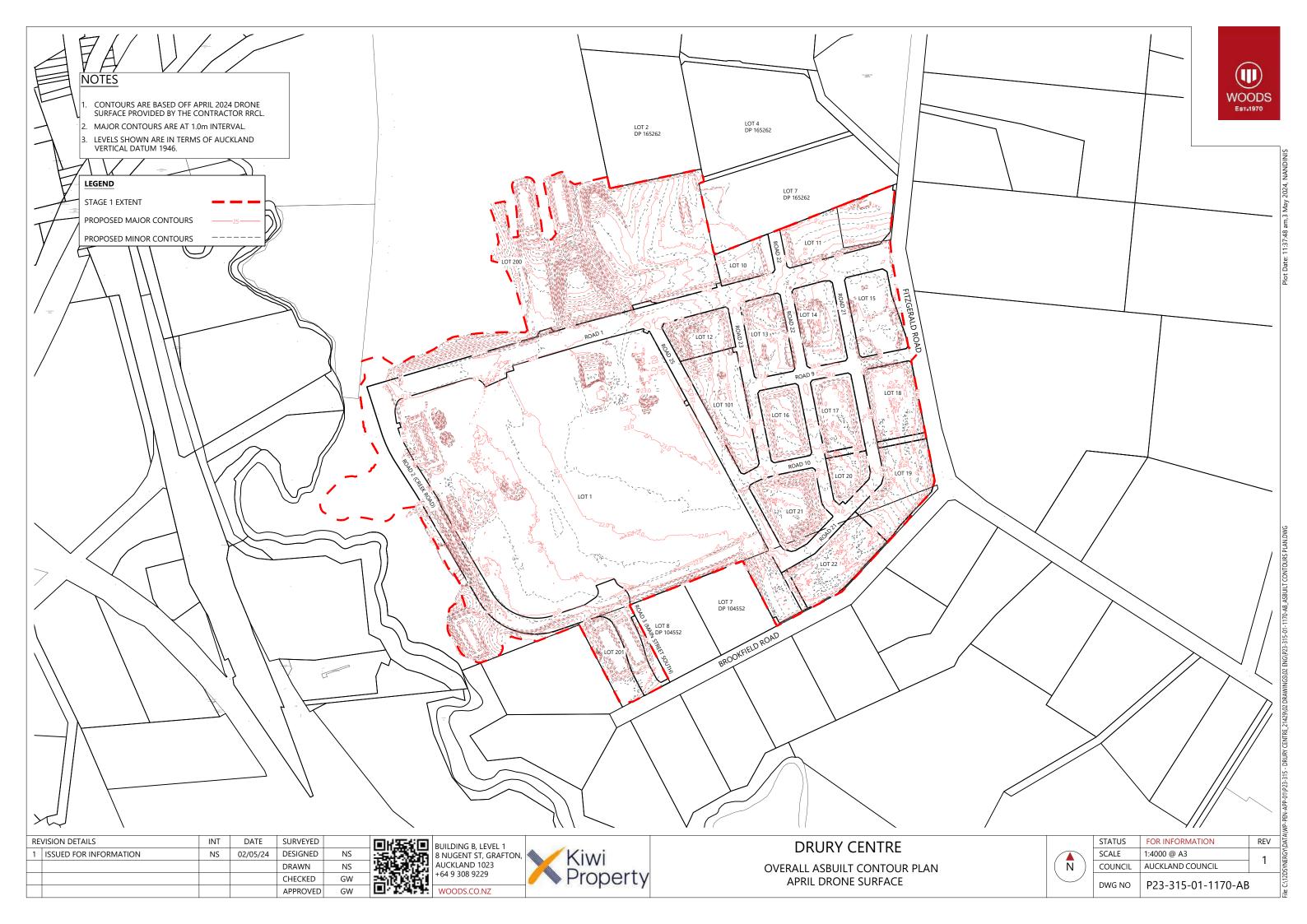
Principal Geotechnical Engineer CMEngNZ, CPEng

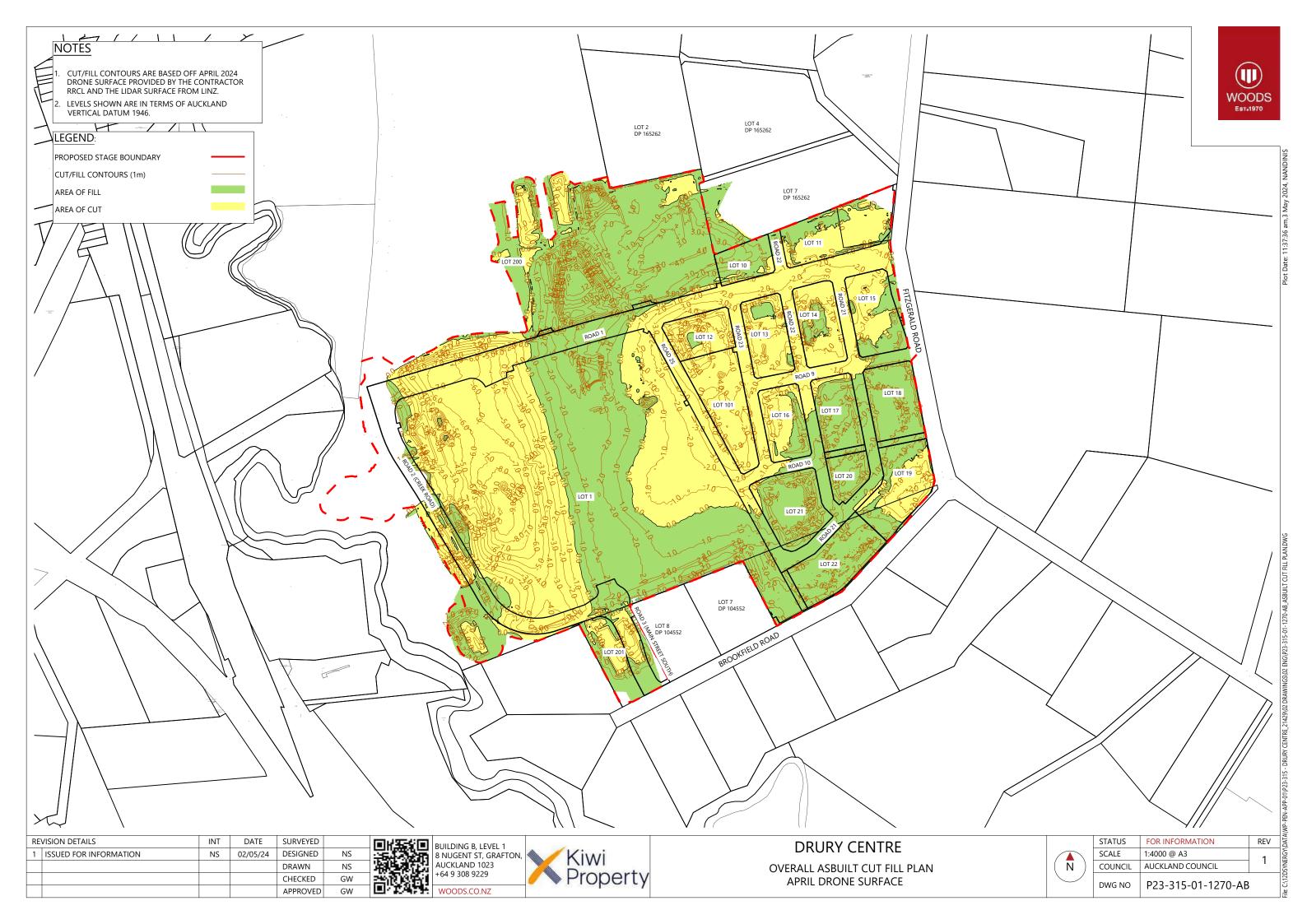


### APPENDIX C: DRAWINGS

Title	Reference No.	Date	Revision
Overall AsBuilt Contour Plan – April Drone Surface	P23-315-01-1170-AB	02/05/24	1
Overall AsBuilt Cut Fill Plan – April Drone Surface	P23-315-01-1270-AB	02/05/24	1
Overral Proposed Contour Plan	P23-315-01-1100-EW	03/05/24	2
Hand Auger Locations	P23-315-01-9105-SK	03/04/24	1











# APPENDIX D: AURECON EARTHWORKS QA AND CERTIFICATION

Aurecon New Zealand Limited Level 3, Te Tihi 110 Carlton Gore Road, Newmarket, Auckland 1023 PO Box 9762, Newmarket, Auckland 1149, New Zealand New Zealand T +64 9 520 6019E auckland@aurecongroup.comW aurecongroup.com



2023-09-22

David Schwartfeger Project Manager Kiwi Property Group PO Box 2071 Auckland 1140

Dear David

Re: Drury Centre Project – Earthworks QA and Certification up to May 2023 – Geotechnical Review, Our Ref 501611

#### 1 Introduction

Aurecon New Zealand Ltd (Aurecon) was engaged by Kiwi Property Holdings No.2 Limited to provide earthworks compaction control and geotechnical earthworks certification for a residential and commercial development located at 133 Fitzgerald Road, Drury (herein referred to as the 'Project').

The works done at the Project through to May 2023 has included large scale earthworks over the southern part of the site, which have been undertaken during the later part of the 2021 to 2022 earthworks season and the 2022 to 2023 earthworks season. Earthworks are still ongoing; however, the Client has engaged other consultants and Aurecon will not be involved in the project going forward. Therefore, this letter has been prepared to provide an overview of the earthworks undertaken up to May 2023.

The earthworks design undertaken by Aurecon is presented in the approved resource consent drawings (Resource Consent BUN60390224) in Appendix A. The extent of earthworks covered by this letter, up to May 2023, is shown on the Ross Reid Contractors Ltd Cut Fill As-Built Surface Drawing in Appendix B.

The purpose of this letter is to detail the earthworks undertaken at the site and present the earth fill compaction results and confirm the suitability of the engineered fill including certification of the filling works conducted in the 2021/2022 and 2022/2023 earthworks seasons.

It is understood that this document will be superseded by a Geotechnical Completion Report (GCR) that will be prepared by others that meets the requirements of the Auckland Council Code of Practice for Land Development and Subdivision, NZS4431:1989¹, the consent conditions outlined in consent BUN60390224 and the stamped consented drawings, upon completion of the project.

#### 2 Geotechnical Reports

In preparation of this letter, we have reviewed the following, previously issued documents, pertaining to the Earthworks aspects of the project:

 Aurecon Geotechnical Investigation Report (GIR) Drury Centre Geotechnical Investigation Report, Ref: 510611, Rev 5. Dated, 4 October 2022.

<sup>&</sup>lt;sup>1</sup> At the time of resource consenting the earthworks were designed in accordance with NZS4431:1989, which has since been superseded by NZS4431:2022.



- Aurecon Report, Section 7: Drury Centre Bulk Earthworks: Earthworks Specifications, Ref. 510611, Revision 1, Dated 3 December 2021.
- Aurecon Letter Drury Bulk Earthworks Stage 1 Separable Portion 1: Completion Certificate 2023
   Geotechnical Review, dated 15 May 2023.

A copy of the Practical completion letter and Earthworks Specifications are presented in Appendix C, for ease of reference.

#### 3 Earthworks Operations

Erosion and sediment control works, and some minor filling commenced on the 11 April 2022 with the main bulk earthworks operations undertaken between May 2022 and 15 May 2023, by Ross Reid Contractors Ltd.

The proposed earthworks are presented on the approved set of resource consent Earthworks Drawings in Appendix A. The cut and fill Layout Plan shows that cuts of up to 9m and fills of up to 8m are required to achieve the necessary design levels of the proposed future lots. This has only been achieved in part at the time of writing this letter.

The extent of Earthworks undertaken to date, and that covered by this letter are shown on the Ross Reid Contractors Ltd, Cut Fill As-Built Surface, located in Appendix B.

#### 3.1 Quantities

The quantities of cuts and fill placed during the 2022/2023 earthworks period, as part of the Stage 1 Earthworks, covered in this letter are presented in Table 1.

Table 1: Summary of the Stage 1 cut to fill quantities.

Item*	Quantity (m³)**
Imported Fill (Certifiable)	165.2
Cut to Certified Fill (Excluding Top Loading)	243,573.36
Cut to certified Fill (Top Loading)	20,570.51
Stockpiled Organic Material for respreading or removal.	8,887.54
Unsuitable Material Removed from Site	6,425.76

<sup>\*</sup>Excluding topsoil volumes

The surface level achieved by the filling works outlined above is presented on the Ross Reid Contractors Ltd Cut Fill Surface Drawing Located in Appendix B.

#### 4 Quality Assurance and Controls

#### 4.1 Laboratory Testing

Laboratory testing was conducted on the site won and imported fill materials prior to their use. Testing was conducted by IANZ accredited facilities, and the results evaluated by an Aurecon Engineering Geologist, who provided confirmation of their suitability for use as bulk fill.

The requirements for laboratory testing and minimum testing frequencies, as defined in the Earthworks Specification, and are presented in Table 2.

<sup>\*\*</sup>Quantities as per Ross Reid Progress Payment Schedule #12 - May 2023.



Table 2: Source suitability testing

Test Type/Requirement	Test Method	Test Frequency
Standard Compaction with Air Voids	NZS 4402:1986, Test 4.1.1	3 tests per site-won fill material for each source location.
Water Content (In-situ)	NZS 4402:1986, Test 2.1	3 tests per site-won fill material for each source location.
Shear Strength	NZGS Guideline for Hand Held Shear Vane Test 2001	3 tests per site-won fill material for each source location, undertaken on a compacted mould sample, which shall be measured and reported for every point on each compaction curve.
Particle Size Distribution	NZS 4402:1986, Test 2.8.1	3 tests per site-won fill material for each source location.
Plasticity Index	NZS 4402:1986, Test 2.2, 2.3 & 2.4	3 tests per site-won fill material for each source location.

The results of the Laboratory testing received from the Contractor is presented in Appendix D.

#### 4.2 Site Monitoring Inspections

During the earthworks season site monitoring inspections were undertaken on a regular basis by an Aurecon Engineer, to assess general compliance with NZS4431:1989 and the Earthworks Specification and monitoring schedule. The inspections included stripping of topsoil, removal of noncertified fill and the benching of the ground prior to the placement of fill.

During earthworks we observed the cut to fill material being placed and assessed its suitability for use as engineered fill prior, including proof rolling of subgrade for soft spots prior to fill placement, observing the fill being compacted and insitu testing of the fill.

Site Inspection Reports (SIR) are presented in Appendix E.

#### 4.3 Quality Control Criteria

The quality control criteria were set out in Earthworks Specification, a summary of which is presented in Table 3. A copy of the full Earthworks Specification is included in Appendix C.

Table 3: Summary of testing requirements

Material	Criteria	Method
Earth fill	Top 1m	Preferred
	98% of Maximum Dry Density (MDD)	Beneath Roads
	Greater than 1m Depth	Nuclear Density Meter (NDM) test at a rate of 1 test per
	95% of Maximum Dry Density (MDD)	20m in each traffic lane
	All	All other earthworks areas
	Moisture content +/- 2% of Optimum Moisture Content (OMC).	Nuclear Density Meter (NDM) test at a rate of 1 test per 500m <sup>3</sup> , or, a minimum of 1 test per 0.5m thickness of fill is being placed. Whichever is greater.
	<pre><or=10% 10<="" air="" average="" over="" pre="" voids=""></or=10%></pre>	31
	tests with a maximum of 12% for any	
	individual test. Air voids to be	



Material	Criteria	Method
	calculated based on laboratory solid density test.  Vane shear strength. Minimum average of 150kPa for 10 tests.  Minimum of 110kPa for any one test.	Each NDM test shall comprise 2 measurements using the same probe hole but orientated at 90 degrees to each other.  Shear vane test at a rate of 2 tests per 500m³, or, a minimum of 1 test per 0.5m thickness of fill is being placed. Whichever is greater.  Undrained shear strength of the compacted soil at any test location shall be taken as the mean of a set of tests, comprising 3 tests undertaken within an area of 0.5m² of each other.  Alternative  New Zealand standard compaction test (NZS4402, Test 4.1.1).
Subgrade	CBR	Dynamic Cone Penetrometer test (NZS 4402, Test 6.5.2)
Subgrade	On-site inspection with Engineer	Proof roll on site - Two axle truck with twin tyres on rear axle, loaded to eight tonnes on the rear axle
Sub-base	Mean > 98% of Max. Dry Density (MDD)  Min > 95% of MDD	Roads Nuclear Density Meter test at a rate of 1 test per 20m in each traffic lane  Building platforms or other hardstand areas Nuclear Density Meter test at a rate of 1 test per 10m²  Alternative  MDD to be the greater of:  New Zealand vibrating hammer compaction test (NZS4402, Test 4.1.3).  Plateau Density Test on a test strip of approx. 50m and at an appropriate water content
Sub-base	CBR > 40%	Dynamic Cone Penetrometer test (NZS 4402, Test 6.5.2)
Base course	Mean > 98% of MDD  Min > 95% of MDD	Preferred Roads  Nuclear Density Meter test at a rate of 1 test per 20m in each traffic lane  Building platforms or other hardstand areas  Nuclear Density Meter test at a rate of 1 test per 100m²  Alternative  MDD to be the greater of:  New Zealand vibrating hammer compaction test (NZS4402, Test 4.1.3).  Plateau Density Test on a test strip of approx. 50m and at an appropriate water content



Material	Criteria	Method
Base course	95% of the deflections measured shall not exceed:  • 0.8mm for Principal and Collector Streets • 1.0mm local streets • 1.3mm for short local streets and cul-de-sacs With no measurement exceeding 25% of the above for the particular category.	Benkelman Beam test

It is noted that as only bulk earthworks have been undertaken to date and the testing requirements which are relevant from the table are the first row – Earth Fill.

#### 4.4 Quality Assurance Testing

In-situ density monitoring was carried out on the general fill areas, to check air voids, water content and undrained shear strengths (Su). Testing was conducted by an independent IANZ endorsed laboratory, engaged by the Contractor. Results of the Nuclear Densometer (NDM) and shear vane testing were submitted to Aurecon for review. Areas that did not meet the standard for engineered fill, set out in Table 2, were reworked and retested until they met the requirements.

The testing was evaluated holistically, with more importance that air voids, shear vane and NDM results pass, noting that moisture content is used by the Contractor to evaluate and optimise to reach the compaction requirements (moisture content provided as guideline).

Testing was conducted at or greater frequency than that recommended by NZS4431:1989, and the Earthworks Specification. The testing results are presented in Appendix E. It is understood that final as-builts will be provided at the completion of the earthworks in accordance with the Earthworks Specification.

#### 4.4.1 Hand Augers

A series of top-down testing was conducted on the lots that had received Practical Completion as Drury Bulk Earthworks Stage 1 Separable Portion 1: Completion Certificate 2023— Geotechnical Review to evaluate the bearing capacity of each lot. The testing comprised the drilling of a series of hand augers at discrete locations across the lots. Due to works ceasing on the project the bearing capacity was not evaluated as part of this letter, it is understood that lot specific testing and evaluation will be conducted as part of the Geotechnical Completion Report, upon completion of the project.

The hand augers are presented as part of the QA Testing in Appendix E.

#### 4.5 Settlement Monitoring Summary

As part of the site work, the Contractor installed and monitored settlement plates and pins. The locations of these are shown in Appendix F. Aurecon supervised and reviewed the settlement monitoring data received from the Contractor for the period covering 26 October 2022 to 28 June 2023. The processed data has been presented in Appendix F. We note the following about the settlement data to date.

- Observed settlement is generally similar to the calculated settlements.
- The settlement data over the past three months indicates a general plateauing of results.



- There is some variability in the readings due to the following reasons:
  - Survey accuracy.
  - Nature of the plastic soils (shrinkage and swelling depending on moisture levels)
  - Heaving of the material due to machinery working close by the pins and plates to achieve compaction.
  - Damage to the monitoring pins, for example the sudden drop in the reading for Plate 3 was due
    to the plate being bumped by a machine so the readings were reset following the incident.

At the time of writing, it is understood that settlement monitoring is ongoing and will be managed by a newly appointed Geotechnical Engineer to the project.

#### 5 Summary

Based on the information provided by the Contractor, our site observations and testing we consider that the engineered fill placed across the site over the 2022/2023 Earthworks seasons meets the requirements for Engineered fill in accordance with NZS4431:1989.

#### 6 Limitations

This Letter has been prepared in accordance with the brief provided to us, the contents of the letter are understood to be used as part of a Geotechnical Completion Report that will be prepared by a Client appointed third-party Geotechnical Engineer in the future, when the works are complete. The Certifying Engineer will still need to satisfy themselves as to the quality of the earthworks for land development and subdivision, Aurecon New Zealand Ltd accepts no liability for the use of the data, opinions and recommendations given in this letter by a third-party.

Subsurface conditions, such as groundwater levels, can change over time, as earthworks stabilise, and static groundwater conditions equilibrate. This should be borne in mind, particularly if this letter is referred to after a protracted delay. Additionally, as earthworks are still on-going, ground conditions are likely to change from the time of preparation of this letter, therefore it is recommended that the recommendations provided in the original geotechnical reports are revised in a Geotechnical Completion Report upon completion of the project.



Yours sincerely

Letter prepared by

Reviewed by:

**David Bosse** 

Senior Engineering Geologist

James Muirson

Lead Engineering Geologist

Verified by:

Wilhelm Nel

Land Infrastructure Practise Lead.



Appendix A
Consented Drawings

#### BUN60390224

Approved Resource Consent Plan

13/04/2022

#### **DRAWING LIST**

COVER SHEET	С
EXISTING SITE LAYOUT PLAN	В
CUT AND FILL LAYOUT PLAN	С
DESIGN CONTOUR LAYOUT PLAN	С
EROSION AND SEDIMENT CONTROL DETAIL - SHEET 1	В
EROSION AND SEDIMENT CONTROL DETAIL - SHEET 2	В
EROSION AND SEDIMENT CONTROL PLAN STARTING SEQUENCE - SHEET 1	В
EROSION AND SEDIMENT CONTROL PLAN SEQUENCING SECOND PHASE - SHEET 2	В
EROSION AND SEDIMENT CONTROL PLAN SEQUENCING FINAL PHASE - SHEET 3	В
EROSION AND SEDIMENT CONTROL PLAN CLOSE-UP AREAS	Α
TRANSMISSION POWERLINE PLAN AND SECTIONS	С
EXISTING UTILITIES LAYOUT PLAN - SHEET 1	В
	EXISTING SITE LAYOUT PLAN CUT AND FILL LAYOUT PLAN DESIGN CONTOUR LAYOUT PLAN  EROSION AND SEDIMENT CONTROL DETAIL - SHEET 1 EROSION AND SEDIMENT CONTROL DETAIL - SHEET 2  EROSION AND SEDIMENT CONTROL PLAN STARTING SEQUENCE - SHEET 1 EROSION AND SEDIMENT CONTROL PLAN SEQUENCING SECOND PHASE - SHEET 2 EROSION AND SEDIMENT CONTROL PLAN SEQUENCING FINAL PHASE - SHEET 3 EROSION AND SEDIMENT CONTROL PLAN CLOSE-UP AREAS





LOCALITY PLAN

#### ABN: 54 005 139 873

A person using the Aurecon drawings and other data accepts the risk of using the drawings and other data:

1. In electronic form without requesting and checking them for accuracy against the original hard copy versions;

2. For any purposes not agreed to in writing by Aurecon.

Wherever a discrepancy in the contract documents is found and unless directed otherwise by the Principal/Engineer, the contractor shall adopt, at their own cost the greater quantum, class of finish, grade, or specification where applicable.

### FOR CONSENT



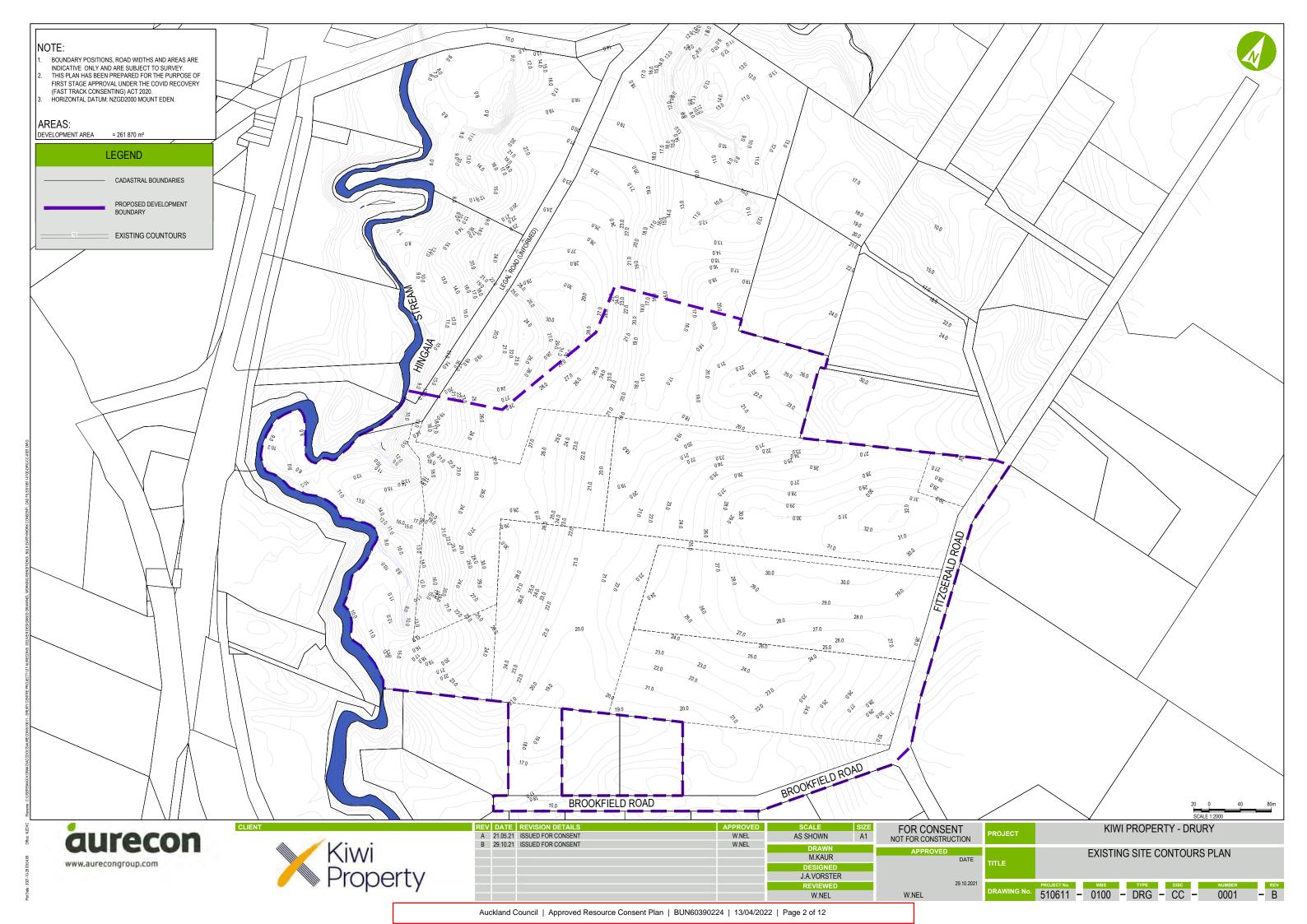


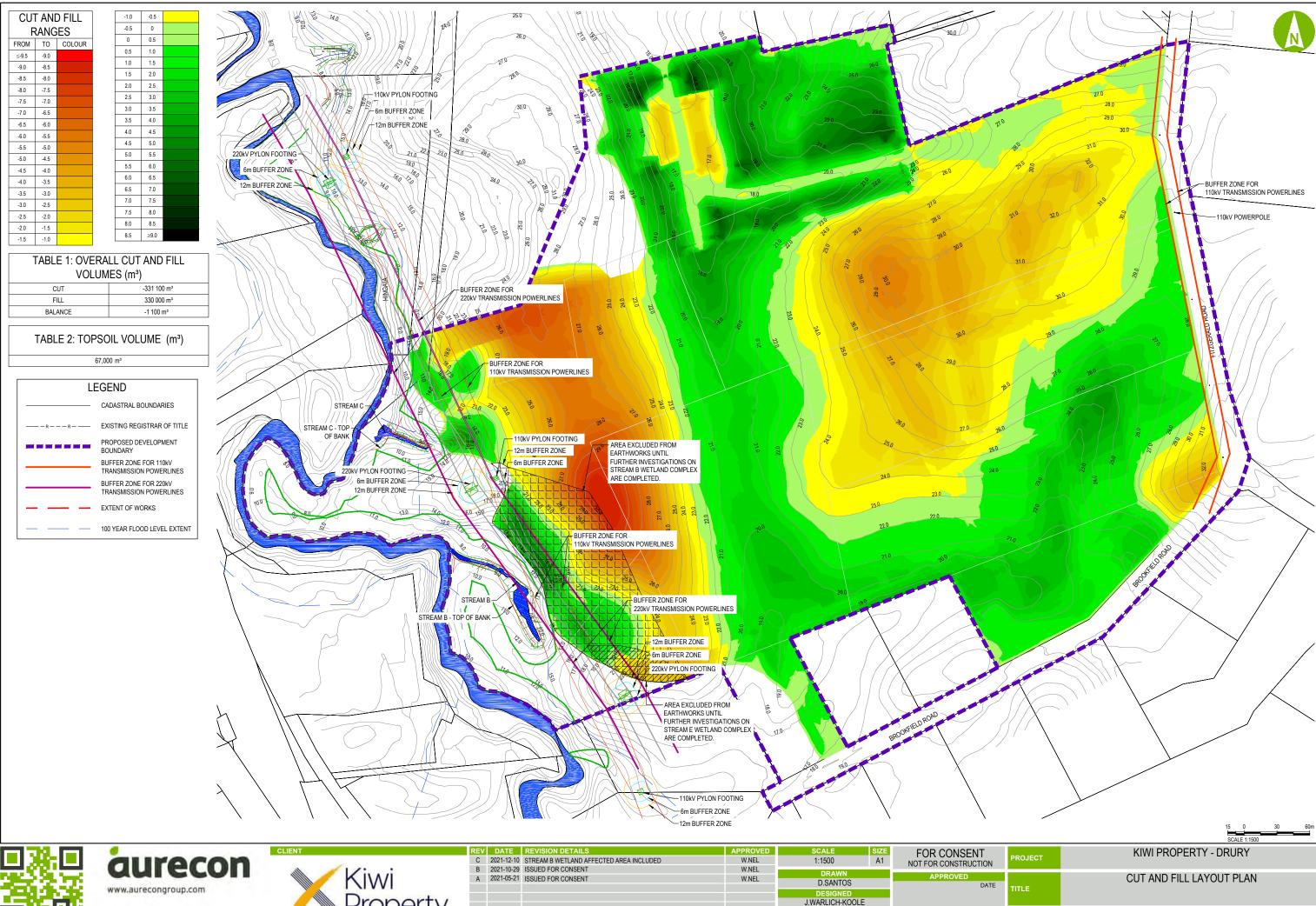


₹EV [	DATE	REVISION DETAILS	APPROVED	SCALE
С	2021-12-10	ISSUED FOR CONSENT: REVISED CONTENT	W.NEL	AS SHOWN
В	2021-10-29	ISSUED FOR CONSENT	W.NEL	DRAWN
Α	2021-05-21	ISSUED FOR CONSENT	W.NEL	
/ (	2021 00 21	ISSUED I SIT SONGERI	Winter	D.SANTOS
				DESIGNED
				J.A.VORSTER
				REVIEWED

E	FOR CONSENT NOT FOR CONSTRUCTION	
	APPROVED	
	DATE	Т
	2021-12-10	L
_	2021-12-10	D

	PROJECT	KIWI PROPERTY - DRURY			
	TITLE	COVER SHEET			
10	DRAWING No.	PROJECT No.         AREA         TYPE         DISC         NUMBER         RE           510611         — 0100         — DRG         — CC         — 0000         — 0			









KEV	DATE	REVISION DETAILS	APPROVED	
С	2021-12-10	STREAM B WETLAND AFFECTED AREA INCLUDED	W.NEL	
В	2021-10-29	ISSUED FOR CONSENT	W.NEL	
Α	2021-05-21	ISSUED FOR CONSENT	W.NEL	

W.NEL

J.A.VORSTER

