| | | 4 Fred Thomas Drive, Takapuna, Auckland 0622 PO Box 100253, North Shore, Auckland 0745 | Project No: | 220372 | Page | 1 | of | 5 | | | |
|---|--|---|---------------|--------|-------|------------|------|---|--|--|--|
| RII FY | Tel: 09 489 7872 Email: riley@riley.co.nz | Project: | Southland Win | d Farm | | | | | | | |
| | | 22 Moorhouse Avenue, Addington, Christchurch 8011 PO Box 4355, Christchurch 8140 | Calc: | JLC | Date: | 27/0 | 6/25 | | | | |
| | | Tel: 03 379 4402 Email: rileychch@riley.co.nz | Check: | LG | Date: | 14/08/2025 | | | | | |
| Description: Sediment Yield Estimation – Typical Catchments | | | | | | | | | | | |

Objective

To estimate sediment yield from typical land disturbing activities included within the scope of the Southland Wind Farm development. The typical scenarios/catchments assessed include:

- Formation of wind turbine platforms.
- Formation of new access tracks.
- Formation of ancillary platforms.
- Surplus fill disposal site in head of gully
- Surplus fill disposal site shoulder fill.

Methodology

The Universal Soil Loss Equation (USLE) has been adopted to assess the 'pre-development', 'unmitigated', and 'mitigated' sediment yield.

USLE Equation: $A = R \times K \times LS \times C \times P$

A = Estimate of Sediment Generation (tonnes/ha/yr)

Where:

R = Rainfall Erosion Index (J/ha)

K = Soil Erodibility Factor (tonnes/unit of R)

LS = Slope Length and Steepness Factor

C = Ground Cover Factor

P = Roughness Factor

Design calculations and parameters are generally based on the *Auckland Regional* Council landfacts S-05: Estimating Sediment Yield Using the Universal Soil Loss Equation.

Rainfall Erosion Index (R)

R is calculated based on the 50% AEP 6-hour rainfall depth.

 $R = 0.00828 \times p^{2.2} \times 1.7$

Where:

p = 28.90mm (Hirds)

R = 23.04 J/ha

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|-------|--|---|---------------------|--------|-------|-------------|-------|----|--|
| RILEY | Tel: 09 489 7872 Email: riley@riley.co.nz | Project: | Southland Wind Farm | | | | | | |
| | | 22 Moorhouse Avenue, Addington, Christchurch 8011 PO Box 4355, Christchurch 8140 | Calc: | JLC | Date: | e: 27/06/25 | | | |
| | | Tel: 03 379 4402 Email: rileychch@riley.co.nz | Check: | LG | Date: | 14/08 | 3/20: | 25 | |
| | | | | | | | | | |

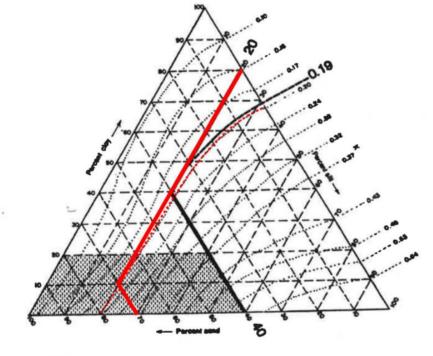
Description: Sediment Yield Estimation – Typical Catchments

Soil Erodibility Factor (K)

K is based on a typical soil composition which has been assumed as uniform across the site. Soil logs presented in the Geotechnical Report (refer to Riley Report: 220372-B) indicate an estimated 10% clay, 20% silt, and 70% sand. The nomograph shown in Figure 1 is used to determine the K value which is then multiplied by 1.32 to convert units. 4% and 0% organic content is assumed for pre-development and earthworks, respectively.

K _{pre-dev} = (0.20 - 0.10) x 1.32 = 0.13 (adjusted for 4% organic matter) K _{earthworks} = (0.20 + 0.10) x 1.32 = 0.40 (0% organic matter)

Figure 1: Triangular Nomograph for Estimating K Values (red mark-up)



Goldman et al. 1986

Slope Length and Steepness Factor (LS)

LS has been assessed based site topography and corresponding values presented in S-05 Appendix 1 – LS Values. For the earthwork's construction phase, the average slope of the pre and post earthworks landform has been calculated. For the re-establishment phase the post earthworks slope has been calculated.

Figure 2: LS Values

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|---|--|---|-------------|---------------|--------|----------|-------|----|--|--|--|--|
| | | Tel: 09 489 7872 Email: riley@riley.co.nz | Project: | Southland Win | d Farm | Farm | | | | | | |
| | | 22 Moorhouse Avenue, Addington, Christchurch 8011 PO Box 4355, Christchurch 8140 | Calc: | JLC | Date: | 27/06/25 | | | | | | |
| | | Tel: 03 379 4402 Email: rileychch@riley.co.nz | Check: | LG | Date: | 14/08 | 3/20: | 25 | | | | |
| Description: Sediment Yield Estimation – Typical Catchments | | | | | | | | | | | | |

| 1 | | | | | Slop | e Length, | m | | | | | | |
|--|---------|---------------|--------|--------|--------|-----------|--------|-------------|--------|-----------------------------|--------|--------|--------|
| Slope Ratio s,% | 10.00 | 25.00 | 50.00 | 75.00 | 100.00 | 125.00 | 150.00 | 175.00 | 200.00 | 225.00 | 250.00 | 275.00 | 300.00 |
| 0.50 | 0.08 | 0.09 | 0.11 | 0.11 | 0.12 | 0.13 | 0.13 | 0.14 | 0.14 | 0.14 | 0.15 | 0.15 | 0.15 |
| 1.00 | 0.09 | 0.12 | 0.15 | 0.17 | 0.18 | 0.20 | 0.21 | 0.22 | 0.23 | 0.23 | 0.24 | 0.25 | 0.26 |
| 2.00 | 0.14 | 0.19 | 0.23 | 0.26 | 0.29 | 0.31 | 0.32 | 0.34 | 0.35 | 0.37 | 0.38 | 0.39 | 0.40 |
| 3.00 | 0.21 | 0.27 | 0.33 | 0.38 | 0.41 | 0.44 | 0.46 | 0.48 | 0.50 | 0.52 | 0.54 | 0.56 | 0.57 |
| 4.00 | 0.26 | 0.37 | 0.49 | 0.57 | 0.64 | 0.70 | 0.76 | 0.80 | 0.85 | 0.89 | 0.93 | 0.96 | 1.00 |
| 5.00 | 0.31 | 0.48 | 0.69 | 0.84 | 0.97 | 1.08 | 1.19 | 1.28 | 1.37 | 1.45 | 1.53 | 1.61 | 1.68 |
| 6.00 | 0.39 | 0.61 | 0.86 | 1.06 | 1.22 | 1.36 | 1.49 | 1.61 | 1.72 | 1.83 | 1.93 | 2.02 | 2.11 |
| 7.00 | 0.47 | 0.75 | 1.06 | 1.29 | 1.49 | 1.67 | 1.83 | 1.98 | 2.11 | 2.24 | 2.36 | 2.48 | 2.59 |
| 8.00 | 0.57 | 0.90 | 1.27 | 1.56 | 1.80 | 2.01 | 2.20 | 2.38 | 2.54 | 2.70 | 2.84 | 2.98 | 3.11 |
| 9.00 | 0.67 | 1.06 | 1.50 | 1.84 | 2.13 | 2.38 | 2.60 | 2.81 | 3.01 | 3.19 | 3.36 | 3.53 | 3.68 |
| 10.00 | 0.78 | 1.24 | 1.75 | 2.15 | 2.48 | 2.77 | 3.04 | 3.28 | 3.51 | 3.72 | 3.92 | 4.11 | 4.30 |
| 11.00 | 0.91 | 1.43 | 2.02 | 2.48 | 2.86 | 3.20 | 3.51 | 3.79 | 4.05 | 4.29 | 4.53 | 4.75 | 4.96 |
| 12.50 | 1.10 | 1.74 | 2.46 | 3.02 | 3.48 | 3.89 | 4.26 | 4.61 | 4.92 | 5.22 | 5.51 | 5.77 | 6.03 |
| 15.00 | 1.47 | 2,32 | 3.28 | 4.02 | 4.64 | 5.19 | 5.68 | 6.14 | 6.56 | 6.96 | 7.34 | 7.69 | 8.04 |
| 16.70 | 1.74 | 2.76 | 3.90 | 4.77 | 5.51 | 6.16 | 6.75 | 7.29 | 7.79 | 8.27 | 8.71 | 9.14 | 9.55 |
| 20.00 | 2.34 | 3.70 | 5.23 | 6.40 | 7.39 | 8.26 | 9.05 | 9.78 | 10.45 | 11.09 | 11.69 | 12.26 | 12.80 |
| 22.00 | 2.73 | 4.32 | 6.11 | 7.49 | 8.65 | 9.67 | 10.59 | 11.44 | 12.23 | 12.97 | 13.67 | 14.34 | 14.98 |
| 25.00 | 3.38 | 5.34 | 7.55 | 9.25 | 10.68 | 11.94 | 13.08 | 14.12 | 15.10 | 16.01 | 16.88 | 17.70 | 18.49 |
| 30.00 | 4.56 | 7.21 | 10.19 | 12.48 | 14.41 | 16.12 | 17.65 | 19.07 | 20.39 | 21.62 | 22.79 | 23.90 | 24.97 |
| 33.30 | 5.41 | 8.55 | 12.09 | 14.80 | 17.09 | 19.11 | 20.93 | 22.61 | 24.17 | 25.64 | 27.03 | 28.34 | 29.61 |
| 35.00 | 5.86 | 9.26 | 13.10 | 16.05 | 18.53 | 20.71 | 22.69 | 24.51 | 26.20 | 27.79 | 29.30 | 30.73 | 32.09 |
| 40.00 | 7.25 | 11.47 | 16.22 | 19.86 | 22.93 | 25.64 | 28.09 | 30.34 | 32.43 | 34.40 | 36.26 | 38.03 | 39.72 |
| 45.00 | 8.71 | 13.78 | 19.48 | 23.86 | 27.55 | 30.80 | 33.74 | 36.45 | 38.96 | 41.33 | 43.56 | 45.69 | 47.72 |
| 50.00 | 10.22 | 16.15 | 22.84 | 27.98 | 32.31 | 36.12 | 39.57 | 42.74 | 45.69 | 48.46 | 51.08 | 53.57 | 55.95 |
| 55.00 | 11.74 | 18.56 | 26.25 | 32.15 | 37.13 | 41.51 | 45.47 | 49.12 | 52.51 | 55.69 | 58.71 | 61.57 | 64.31 |
| 57.00 | 12.35 | 19.53 | 27.62 | 33.83 | 39.06 | 43,67 | 47.84 | 51.68 | 55.24 | 58.60 | 61.77 | 64.78 | 67.66 |
| 60.00 | 13.27 | 20.98 | 29.67 | 36.34 | 41.96 | 46.91 | 51.39 | 55.51 | 59.34 | 62.94 | 66.35 | 69.59 | 72.68 |
| 66.70 | 15.29 | 24.18 | 34.20 | 41.88 | 48.36 | 54.07 | 59.23 | 63.98 | 68.40 | 72.55 | 76.47 | 80.20 | 83.77 |
| 70.00 | 16.27 | 25.73 | 36.39 | 44.57 | 51.46 | 57.53 | 63.03 | 68.08 | 72.78 | 77.19 | 81.37 | 85.34 | 89.13 |
| 75.00 | 17.72 | 28.03 | 39.63 | 48.54 | 56.05 | 62.67 | 68.65 | 74.15 | 79.27 | 84.08 | 88.62 | 92.95 | 97.08 |
| 80.00 | 19.13 | 30.25 | 42.78 | 52.39 | 60.50 | 67.64 | 74.10 | 80.03 | 85.56 | 90.75 | 95.66 | 100.33 | 104.79 |
| 85.00 | 20.49 | 32.39 | 45.81 | 56.11 | 64.78 | 72.43 | 79.34 | 85.70 | 91.62 | 97.18 | 102.43 | 107.43 | 112.21 |
| 90.00 | 21.79 | 34.45 | 48.72 | 59.67 | 68.90 | 77.03 | 84.38 | 91.14 | 97.43 | 103.35 | 108.94 | 114.25 | 119.33 |
| 95.00 | 23.03 | 36.41 | 51.50 | 63.07 | 72.83 | 81.42 | 89.19 | 96.34 | 102.99 | 109.24 | 115.15 | 120.77 | 126.14 |
| 100.00 | 24.21 | 38.28 | 54.14 | 66.31 | 76.57 | 85.61 | 93.78 | 101.29 | 108.29 | 114.85 | 121.07 | 126.98 | 132.62 |
| Calculated Fro | om: | | | | | | LS= | topographic | | | | | |
| (65 4 | 1 - 2 | 456ve | 1 | (1) | m | | 1- | Slope lengt | | | | | |
| LS = $\left(\frac{65.41}{s^2 + 10}\right)$ | +- | 4.50 \ 8 | +0.065 | × | | | 8 = | Slope steep | | | | | |
| s2+10 | 0,000 \ | $^{2}+10,000$ |) | (12.5) | | | m - | | | slope steep for slopes 1 | | | |

Ground Cover (C) and Roughness (P)

C and P Factors have been adopted from S-05 based on the surface type.

Figure 3: C & P Values

| Treatment | C factor | P factor |
|---------------------------------|-----------------------|----------|
| Bare Soil | | |
| - compacted and smooth | 1.0 | 1.32 |
| - track walked on contour | 1.0 | 1.2 |
| - rough irregular surface | 1.0 | 0.9 |
| - disked to 250 mm depth | 1.0 | 0.8 |
| Native vegetation (undisturbed) | 0.01 | 1.0 |
| Pasture (undisturbed) | 0.02 | 1.0 |
| Establishing grass | 0.1 | 1.0 |
| Mulch – on subsoil ² | 0.15 | 1.0 |
| | (3 month period only) | |
| Mulch – on topsoil ³ | 0.05 | 1.0 |
| • | (3 month period only) | 4 |

Ground cover for re-establishment phase (mulch on topsoil) only relates to surplus fill disposals, plus platform/road earthworks batters/berms. Platforms and roads will be stabilised with hardfill – so those areas are excluded from the re-establishment areas.

E&SC Measures



Description: Sediment Yield Estimation - Typical Catchments

E&SC factors will be incorporated into the USLE calculation to determine mitigation effectiveness before entering the receiving environment. These factors include:

Sediment Delivery Ratio (%)

Regarding the sediment delivery ratio, S-05 identifies 50% as generally accepted. However, this should be increased for steep sites (e.g., 70% where site slopes exceed 10°).

Sediment Control Measure Efficiency (%)

The effectiveness of E&SC devices. S-05 identifies 50% as a conservative value for most devices, except for Sediment Retention Pond (SRP) – where typically a min 75% efficiency is used. However, for coarse grained soils a higher efficiency can be assumed. In the case of SWF geology, the silts/sand and weathered rock matrix would constitute a coarse grained soil, therefore we have adopted the following assumptions for treatment efficiencies:

- Decanting Earth Bund (DEB) = 70%
- SRP = 85%
- Other Devices = 60%

Higher treatment efficiencies would apply for chemically treated SRPs and DEBs installed in accordance with Auckland Regional Council GD05.

Time (estimate only – to be confirmed by Contractor)

The USLE equation calculates annual sediment yield whereas, we have broken this down to months and estimated construction periods for land disturbing activities. We have assumed:

- Turbine and ancillary platforms will require up to 3-months each to form.
- New access tracks will likely be progressively constructed and covered but assume sections could be exposed for up to 3-months at a time.
- Fill disposal sites may remain active (i.e., exposed) for up to 8-months.
- Stabilisation of backfilled disposal sites and/or slopes will take 3-months.

Calculations

Calculations and catchments plans have been appended for each case study.

Commentary on Proposed Sediment Controls

For access tracks in cut or minor fill, and remote from sensitive receiving environments (such as wetlands), it is envisaged that a cut and cover technique can be applied. I.e. the trimmed subgrades will be stabilised progressively and prior to rain events, such that no

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| 4 Fred Thomas Drive, Takapuna, Auckland 0622 PO Box 100253, North Shore, Auckland 0745 | | P |
|---|---|---|
| Tel: 09 489 7872 Email: riley@riley.co.nz | | P |
| 22 Moorhouse Avenue, Addington, Christchurch 8011 PO Box 4355, Christchurch 8140 | | C |
| Tel: 03 379 4402 | Γ | |

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| Check: | LG | 14/08 | 3/20 | 25 | | | | |

Description:

Sediment Yield Estimation - Typical Catchments

Email: rilevchch@rilev.co.nz

specific sediment control devices will be required for those areas. Therefore, the cut and cover scenario has not been assessed further in terms of sediment yield calculations.

It is envisaged that Sediment Retention Ponds (SRP's) will be the primary treatment device for the Surplus Fill Disposal sites (SFD's), given the longer earthworks duration associated with the SFD's, and sloping nature of the SFD sites (particularly in the case of gully fills).

It is envisaged that the decanting earth bunds (DEB's) will be suitable as primary treatment devices for wind turbine platforms and access track fill earthworks. The turbine platforms will be formed as gently sloping/ near flat platforms, therefore these favours splitting the platforms catchment into smaller sub-catchments draining to multiple DEB's.

The ancillary platforms (site compound/ batching plant/substation etc) may utilise SRP's or DEB's, dependant on site constraints and catchment properties.

Other sediment control measures may be utilised where appropriate within the site e.g.:

- silt fences in constrained areas where these is limited space for diversion channels/DEB's, subject to wind loading conditions.
- turkeys' nests for dewatering (pump discharge) from bunded/low lying areas.
 Silt fences and turkeys nests are recognised treatment devices in GD05.

As per GD05, the DEB volumes must be min 2% of the catchment area, with recommended maximum catchment area of 3,000m2. However, given large extent of the proposed earthworks, some flexibility can be applied to allow increased catchment area for each DEB (and proportionally increase the DEB volume) and thus reduce the total number of DEB's.

The use of rain-activated chemical treatment should be considered to increase the sediment yield efficiency of sediment control devices which are in proximity (nominally within 50m) of downstream water bodies – such as bogs/wetlands, and streams. This will be subject to bench testing of site soils and preparation of Chemical Treatment Management Plan. However, for the purposes of this USLE assessment, chemical treatment has not been applied in terms of the sediment control efficiencies used.

P = Roughness Factor

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| Catchment: Exemplar Catchment - Gully Type Fill Disposal (SFD-G04) | Rainfall Depth: | 28.90 | mm | Typ. E&SC | Devices: | |
|--|---------------------------|-------|------------|-----------|--|------------|
| | R = | 23.04 | J/ha | | | Efficiency |
| USLE: A = R*K*LS*C*P | | | | N/A | Unmitigated | 0% |
| | Typ. Soil Composition: | | | 1 | Chemically Treated Sediment Retention Pond | 95% |
| A = Annual Estimated Sediment Generation, T/ha/yr | Clay = | 10% | | 2 | Standard Sediment Retention Pond | 85% |
| R = Rainfall Erosion Index, J/ha | Silt = | 20% | | 3 | Chemically Treated T-bar Decanting Earth Bunds | 85% |
| K = Soil Erodability Factor, T/Unit of R | Sand = | 70% | | 4 | Standard T-bar Decanting Earth Bunds | 70% |
| LS = Slope Length and Steepness Factor | κ _{pre-dev} = | 0.13 | 4% organic | 5 | Other (e.g., silt fencing, mulch etc.) | 60% |
| C = Ground Cover Factor | K _{earthworks} = | 0.40 | 0% organic | | | |

| Area/Activity | R | κ | Slope Length (m) | Slope Grade (%) | LS | Surface Type | С | Р | Exposed Area (ha) | Duration (months) | A (T) | Sediment Delivery Ratio (%) | E&SC Device | Sediment Control Efficiency (%) | Estimated Sediment Yield (T) |
|------------------------|--|------|---------------------|--------------------|------|------------------------------------|-------------|--------------|----------------------|----------------------|----------|-----------------------------|----------------|----------------------------------|---------------------------------|
| | | | | | | | | Pre-develo | ppment | | | | | | |
| Existing Site | 23.04 | 0.13 | 160 | 12.5% | 4.45 | Native vegetation (undisburbed) | 0.01 | 1.00 | 1.20 | 11 | 0.149 | 50% | N/A | 0% | 0.074 |
| | | | | | | | | | | | | | | Subtotal = | 0.074 |
| | Unmitigated Earthworks (Construction Period) | | | | | | | | | | | | | | |
| Gully filling | 23.04 | 0.40 | 160 | 12.5% | 4.45 | Bare Soil -rough irregular surface | 1.00 | 0.90 | 1.20 | 8 | 29.231 | 50% | N/A | 0% | 14.615 |
| Gully stabilisation | 23.04 | 0.13 | 160 | 12.5% | 4.45 | Mulch on topsoil | 0.05 | 1.00 | 1.20 | 3 | 0.200 | 50% | N/A | 0% | 0.100 |
| - | | | | | | | | | | | | | | Subtotal = | 14.715 |
| | | | | | | | Mitigated I | Earthworks (| Construction Pe | eriod) | | | | | |
| Gully filling | 23.04 | 0.40 | 160 | 12.5% | 4.45 | Bare Soil -rough irregular surface | 1.00 | 0.90 | 1.20 | 8 | 29.231 | 50% | 2 | 85% | 2.192 |
| Gully stabilisation | 23.04 | 0.13 | 160 | 12.5% | 4.45 | Mulch on topsoil | 0.05 | 1.00 | 1.20 | 3 | 0.200 | 50% | 2 | 85% | 0.015 |
| Notes: | | | | | | | | | | | | | | Subtotal = | 2.207 |

- 2) Soil Erodability Factor determined based on observed soil composition and Triangular Nomograph for Estimating K values (refer to Auckland Regional Council S-05 Figure 1).
- 3) Slope Length and Steepness Factor based on site topography and corresponding values presented in Auckland Regional Council S-05 Appendix 1.
- 4) Ground Cover and Roughness Factors based on surface cover type and corresponding values presented in Auckland Regional Council S-05 Table 2.
- 5) 50% Sediment Delivery Ratio is generally acceptable except where sites are steep (i.e., 70% for sites where slopes exceed 10-degrees (or 17.5%)).

P = Roughness Factor

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Design: AR Date: 15/08/2025 Project: Southland Wind Farm Check: LG Date: 15/08/2025



| Catchment: Exemplar Catchment - Shoulder Fill Disposal (SFD-21) | Rainfall Depth: | 28.90 | mm | Typ. E&SC | Typ. E&SC Devices: | | | |
|---|---------------------------|-------|------------|-----------|--|-------------------|--|--|
| | R = | 23.04 | J/ha | | | <u>Efficiency</u> | | |
| USLE: A = R*K*LS*C*P | | | | N/A | Unmitigated | 0% | | |
| | Typ. Soil Composition: | | | 1 | Chemically Treated Sediment Retention Pond | 95% | | |
| A = Annual Estimated Sediment Generation, T/ha/yr | Clay = | 10% | | 2 | Standard Sediment Retention Pond | 85% | | |
| R = Rainfall Erosion Index, J/ha | Silt = | 20% | | 3 | Chemically Treated T-bar Decanting Earth Bunds | 85% | | |
| K = Soil Erodability Factor, T/Unit of R | Sand = | 70% | | 4 | Standard T-bar Decanting Earth Bunds | 70% | | |
| LS = Slope Length and Steepness Factor | K _{pre-dev} = | 0.13 | 4% organic | 5 | Other (e.g., silt fencing, mulch etc.) | 60% | | |
| C = Ground Cover Factor | K _{earthworks} = | 0.40 | 0% organic | | | | | |

| Area/Activity | R | к | Slope Length (m) | Slope Grade (%) | LS | Surface Type | С | P | Exposed Area (ha) | Duration (months) | A (T) | Sediment Delivery Ratio (%) | E&SC Device | Sediment Control Efficiency (%) | Estimated Sediment Yield (T) |
|---------------------------|--|------|---------------------|--------------------|------|----------------------------------|-------------|--------------|----------------------|----------------------|----------|-----------------------------|----------------|----------------------------------|---------------------------------|
| | | | | | | | | Pre-develo | ppment | | | | | | |
| Existing Site | 23.04 | 0.13 | 125 | 9.0% | 2.38 | Native vegetation (undisburbed) | 0.01 | 1.00 | 1.43 | 11 | 0.095 | 50% | N/A | 0% | 0.047 |
| | | | | | | | | | | | | | | Subtotal = | 0.047 |
| | Unmitigated Earthworks (Construction Period) | | | | | | | | | | | | | | |
| Shoulder filling | 23.04 | 0.40 | 125 | 9.0% | 2.38 | Bare Soil - compacted and smooth | 1.00 | 1.32 | 1.43 | 8 | 27.324 | 50% | N/A | 0% | 13.662 |
| Shoulder stabilisation | 23.04 | 0.13 | 125 | 9.0% | 2.38 | Mulch on topsoil | 0.05 | 1.00 | 1.43 | 3 | 0.127 | 50% | N/A | 0% | 0.064 |
| | | | | | | | | | | | | | | Subtotal = | 13.726 |
| | | | | | | | Mitigated I | Farthworks (| Construction Pe | eriod) | | | | | |
| Shoulder filling | 23.04 | 0.40 | 125 | 9.0% | 2.38 | Bare Soil - compacted and smooth | 1.00 | 1.32 | 1.43 | 8 | 27.324 | 50% | 2 | 85% | 2.049 |
| Shoulder stabilisation | 23.04 | 0.13 | 125 | 9.0% | 2.38 | Mulch on topsoil | 0.05 | 1.00 | 1.43 | 3 | 0.127 | 50% | 2 | 85% | 0.010 |
| Notes: | | | | | | | | | | | | | | Subtotal = | 2.059 |

- 2) Soil Erodability Factor determined based on observed soil composition and Triangular Nomograph for Estimating K values (refer to Auckland Regional Council S-05 Figure 1).
- 3) Slope Length and Steepness Factor based on site topography and corresponding values presented in Auckland Regional Council S-05 Appendix 1.
- 4) Ground Cover and Roughness Factors based on surface cover type and corresponding values presented in Auckland Regional Council S-05 Table 2.
- 5) 50% Sediment Delivery Ratio is generally acceptable except where sites are steep (i.e., 70% for sites where slopes exceed 10-degrees (or 17.5%)).

P = Roughness Factor

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 Date: 15/08/2025



| Catchment: Exemplar Catchment - Turbine Platform (JED 19) | Rainfall Depth: | 28.90 | mm | Typ. E&SC | Devices: | |
|---|---------------------------|-------|------------|-----------|--|-------------------|
| | R = | 23.04 | J/ha | | | <u>Efficiency</u> |
| USLE: A = R*K*LS*C*P | | | | N/A | Unmitigated | 0% |
| | Typ. Soil Composition: | | | 1 | Chemically Treated Sediment Retention Pond | 95% |
| A = Annual Estimated Sediment Generation, T/ha/yr | Clay = | 10% | | 2 | Standard Sediment Retention Pond | 85% |
| R = Rainfall Erosion Index, J/ha | Silt = | 20% | | 3 | Chemically Treated T-bar Decanting Earth Bunds | 85% |
| K = Soil Erodability Factor, T/Unit of R | Sand = | 70% | | 4 | Standard T-bar Decanting Earth Bunds | 70% |
| LS = Slope Length and Steepness Factor | K _{pre-dev} = | 0.13 | 4% organic | 5 | Other (e.g., silt fencing, mulch etc.) | 60% |
| C = Ground Cover Factor | K _{earthworks} = | 0.40 | 0% organic | | | |

| Area/Activity | R | к | Slope Length (m) | Slope Grade (%) | LS | Surface Type | С | Р | Exposed Area (ha) | Duration (months) | А (т) | Sediment Delivery Ratio (%) | E&SC Device | Sediment Control Efficiency (%) | Estimated Sediment Yield (T) |
|--|-------|------|---------------------|--------------------|------|---------------------------------------|-----------|---------------|----------------------|----------------------|----------|-----------------------------|----------------|----------------------------------|---------------------------------|
| Pre-development | | | | | | | | | | | | | | | |
| Existing Site | 23.04 | 0.13 | 85 | 20.0% | 7.00 | Native vegetation (undisburbed) | 0.01 | 1.00 | 1.14 | 6 | 0.121 | 50% | N/A | 0% | 0.061 |
| | | | | | | | | | | | | | | Subtotal = | 0.061 |
| Unmitigated Earthworks (Construction Period) | | | | | | | | | | | | | | | |
| Platform construction | 23.04 | 0.40 | 50 | 2.0% | 0.23 | Bare Soil - compacted and smooth | 1.00 | 1.32 | 0.75 | 3 | 0.519 | 50% | N/A | 0% | 0.260 |
| Slope construction | 23.04 | 0.40 | 35 | 20.0% | 4.30 | Bare Soil -rough irregular surface | 1.00 | 0.90 | 0.39 | 3 | 3.442 | 50% | N/A | 0% | 1.721 |
| Slope stabilisation | 23.04 | 0.13 | 35 | 33.0% | 9.15 | Mulch on topsoil | 0.05 | 1.00 | 0.39 | 3 | 0.134 | 70% | N/A | 0% | 0.094 |
| | | | | | | | Mitigated | Earthworks (C | Construction Pe | eriod) | | | | Subtotal = | 2.074 |
| Platform construction | 23.04 | 0.40 | 50 | 2.0% | 0.23 | Bare Soil - compacted and smooth | 1.00 | 1.32 | 0.75 | 3 | 0.519 | 50% | 4 | 70% | 0.078 |
| Slope construction | 23.04 | 0.40 | 35 | 20.0% | 4.30 | Bare Soil -rough irregular surface | 1.00 | 0.90 | 0.39 | 3 | 3.442 | 70% | 4 | 70% | 0.723 |
| Slope stabilisation | 23.04 | 0.13 | 35 | 33.0% | 9.15 | Mulch on topsoil | 0.05 | 1.00 | 0.39 | 3 | 0.134 | 70% | 4 | 70% | 0.028 |
| Notes: | | | | | | | _ | | | | | | | Subtotal = | 0.829 |

- 3) Slope Length and Steepness Factor based on site topography and corresponding values presented in Auckland Regional Council S-05 Appendix 1.
- 4) Ground Cover and Roughness Factors based on surface cover type and corresponding values presented in Auckland Regional Council S-05 Table 2.
- 5) 50% Sediment Delivery Ratio is generally acceptable except where sites are steep (i.e., 70% for sites where slopes exceed 10-degrees (or 17.5%)).

²⁾ Soil Erodability Factor determined based on observed soil composition and Triangular Nomograph for Estimating K values (refer to Auckland Regional Council S-05 - Figure 1).

23.04

23.04

0.40

0.40

52

52

2.0%

2.0%

1) Rainfall Erosion Index is calculated based on HIRDS V4 50% AEP 6-hour rainfall depth.

0.23

Platform

Platform

construction

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Subtotal =

Subtotal =

Subtotal =

0%

70%

0.004

0.152

0.152

0.046

0.046

| Catchment: | atchment - 1 | urbine Platfori | <mark>m within Wetla</mark> n | d (JED-23 | B) R | ainfall Depth: | 28.90 | mm | | Typ. E&SC Devices: | | | | | |
|--|--------------|-----------------|-------------------------------|-------------|------|---------------------------------|---------------------------|----------|----------------------|----------------------|----------|-------------------------------|----------------|----------------------------------|---------------------------------|
| | | | | | | | R = | 23.04 | J/ha | | | | | | <u>Efficiency</u> |
| USLE: | A = R*K*LS* | *C*P | | | | | | | | | N/A | Unmitigated | | | 0% |
| | | | | | | Typ. Soil | Composition: | | | | 1 | Chemically Treated Sedim | ent Retention | n Pond | 95% |
| A = | Annual Esti | mated Sedim | ent Generatior | n, T/ha/yr | | | Clay = | 10% | | | 2 | Standard Sediment Retent | ion Pond | | 85% |
| R = Rainfall Erosion Index, J/ha | | | | | | | Silt = | 20% | | | 3 | Chemically Treated T-bar | 85% | | |
| K = Soil Erodability Factor, T/Unit of R | | | | | | | Sand = | 70% | | | 4 | Standard T-bar Decanting | 70% | | |
| LS = | Slope Lengt | th and Steepr | ess Factor | | | | K _{pre-dev} = | 0.13 | 4% organic | | 5 | Other (e.g., silt fencing, mu | 60% | | |
| C = | Ground Cov | ver Factor | | | | | K _{earthworks} = | 0.40 | 0% organic | | | | | | |
| P = | Roughness | Factor | | | | | | | | | | | | | |
| Area/Activity | R | к | Slope Length (m) | Slope Grade | LS | Surface Type | С | P | Exposed Area (ha) | Duration (months) | A (T) | Sediment Delivery Ratio (%) | E&SC Device | Sediment Control Efficiency (%) | Estimated Sediment Yield (T) |
| | | | Length (m) | (%) | | | | 0 | . , | (months) | (1) | (%) | Device | Efficiency (%) | Yield (1) |
| | | | | | | | _ | Pre-deve | opment | | | | | | |
| Existing Site | 23.04 | 0.13 | 77 | 7.0% | 1.30 | Native vegetation (undisburbed) | 0.01 | 1.00 | 0.44 | 6 | 0.009 | 50% | N/A | 0% | 0.004 |

Unmitigated Earthworks (Construction Period)

Mitigated Earthworks (Construction Period)

0.44

0.305

0.305

50%

50%

N/A

1.32

1.32

1.00

1.00

| construction | and smooth | | |
|--------------|------------|--|--|
| Notes: | | | |

Bare Soil - compacted

Bare Soil - compacted

and smooth

- 2) Soil Erodability Factor determined based on observed soil composition and Triangular Nomograph for Estimating K values (refer to Auckland Regional Council S-05 Figure 1).
- 3) Slope Length and Steepness Factor based on site topography and corresponding values presented in Auckland Regional Council S-05 Appendix 1.
- 4) Ground Cover and Roughness Factors based on surface cover type and corresponding values presented in Auckland Regional Council S-05 Table 2.
- 5) 50% Sediment Delivery Ratio is generally acceptable except where sites are steep (i.e., 70% for sites where slopes exceed 10-degrees (or 17.5%)).

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 Date: 15/08/2025



| Catchment: Exemplar Catchment - Access Track | Rainfall Depth: | 28.90 | mm | Typ. E&SC | Devices: | |
|---|---------------------------|-------|------------|-----------|--|-------------------|
| | R = | 23.04 | J/ha | | | <u>Efficiency</u> |
| USLE: A = R*K*LS*C*P | | | | N/A | Unmitigated | 0% |
| | Typ. Soil Composition: | | | 1 | Chemically Treated Sediment Retention Pond | 95% |
| A = Annual Estimated Sediment Generation, T/ha/yr | Clay = | 10% | | 2 | Standard Sediment Retention Pond | 85% |
| R = Rainfall Erosion Index, J/ha | Silt = | 20% | | 3 | Chemically Treated T-bar Decanting Earth Bunds | 85% |
| K = Soil Erodability Factor, T/Unit of R | Sand = | 70% | | 4 | Standard T-bar Decanting Earth Bunds | 70% |
| LS = Slope Length and Steepness Factor | K _{pre-dev} = | 0.13 | 4% organic | 5 | Other (e.g., silt fencing, mulch etc.) | 60% |
| C = Ground Cover Factor | K _{earthworks} = | 0.40 | 0% organic | | | |
| P = Roughness Factor | | | | | | |

| Area/Activity | R | к | Slope Length (m) | Slope Grade (%) | LS | Surface Type | С | P | Exposed Area (ha) | Duration (months) | А (т) | Sediment Delivery Ratio (%) | E&SC Device | Sediment Control Efficiency (%) | Estimated Sediment Yield (T) |
|---------------------------------|--|------|---------------------|--------------------|------|---------------------------------------|-------------|--------------|----------------------|----------------------|----------|-----------------------------|----------------|---------------------------------|---------------------------------|
| Pre-development Pre-development | | | | | | | | | | | | | | | |
| Existing Site | 23.04 | 0.13 | 26 | 20.0% | 3.70 | Native vegetation (undisburbed) | 0.01 | 1.00 | 0.25 | 6 | 0.014 | 50% | N/A | 0% | 0.0070 |
| | | | | | | | | | | | | | | Subtotal = | 0.0070 |
| | Unmitigated Earthworks (Construction Period) | | | | | | | | | | | | | | |
| Batter construction | 23.04 | 0.40 | 26 | 20.0% | 3.70 | Bare Soil -rough irregular surface | 1.00 | 0.90 | 0.25 | 3 | 1.899 | 50% | N/A | 0% | 0.9494 |
| Batter stabilisation | 23.04 | 0.13 | 26 | 33.0% | 8.55 | Mulch on topsoil | 0.05 | 1.00 | 0.25 | 3 | 0.080 | 70% | N/A | 0% | 0.0560 |
| | | | | | | | | | | | | | | Subtotal = | 1.005 |
| | | | | | | | Mitigated I | arthworks (C | Construction Pe | eriod) | | | | | |
| Batter construction | 23.04 | 0.40 | 26 | 20.0% | 3.70 | Bare Soil -rough irregular surface | 1.00 | 0.90 | 0.25 | 3 | 1.899 | 50% | 4 | 70% | 0.2848 |
| Batter stabilisation | 23.04 | 0.13 | 26 | 33.0% | 8.55 | Mulch on topsoil | 0.05 | 1.00 | 0.25 | 3 | 0.080 | 70% | 4 | 70% | 0.0168 |
| Notes: | | | | | | | | | | | | | | Subtotal = | 0.302 |

- 2) Soil Erodability Factor determined based on observed soil composition and Triangular Nomograph for Estimating K values (refer to Auckland Regional Council S-05 Figure 1).
- 3) Slope Length and Steepness Factor based on site topography and corresponding values presented in Auckland Regional Council S-05 Appendix 1.
- 4) Ground Cover and Roughness Factors based on surface cover type and corresponding values presented in Auckland Regional Council S-05 Table 2.
- 5) 50% Sediment Delivery Ratio is generally acceptable except where sites are steep (i.e., 70% for sites where slopes exceed 10-degrees (or 17.5%)).

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 220372
 Design: AR
 Date: 15/08/2025

 Project:
 Southland Wind Farm
 Check: LG
 Date: 15/08/2025



| Catchment: Exemplar Catchment - Site Facility (Overflow Storage Area) | Rainfall Depth: | 28.90 | mm | Typ. E&SC D | evices: | |
|---|---------------------------|-------|------------|-------------|--|-------------------|
| | R = | 23.04 | J/ha | | | <u>Efficiency</u> |
| USLE: A = R*K*LS*C*P | | | | N/A | Unmitigated | 0% |
| | Typ. Soil Composition: | | | 1 | Chemically Treated Sediment Retention Pond | 95% |
| A = Annual Estimated Sediment Generation, T/ha/yr | Clay = | 10% | | 2 | Standard Sediment Retention Pond | 85% |
| R = Rainfall Erosion Index, J/ha | Silt = | 20% | | 3 | Chemically Treated T-bar Decanting Earth Bunds | 85% |
| K = Soil Erodability Factor, T/Unit of R | Sand = | 70% | | 4 | Standard T-bar Decanting Earth Bunds | 70% |
| LS = Slope Length and Steepness Factor | K pre-dev = | 0.13 | 4% organic | 5 | Other (e.g., silt fencing, mulch etc.) | 60% |
| C = Ground Cover Factor | K _{earthworks} = | 0.40 | 0% organic | | | |
| P = Roughness Factor | | | | | | |

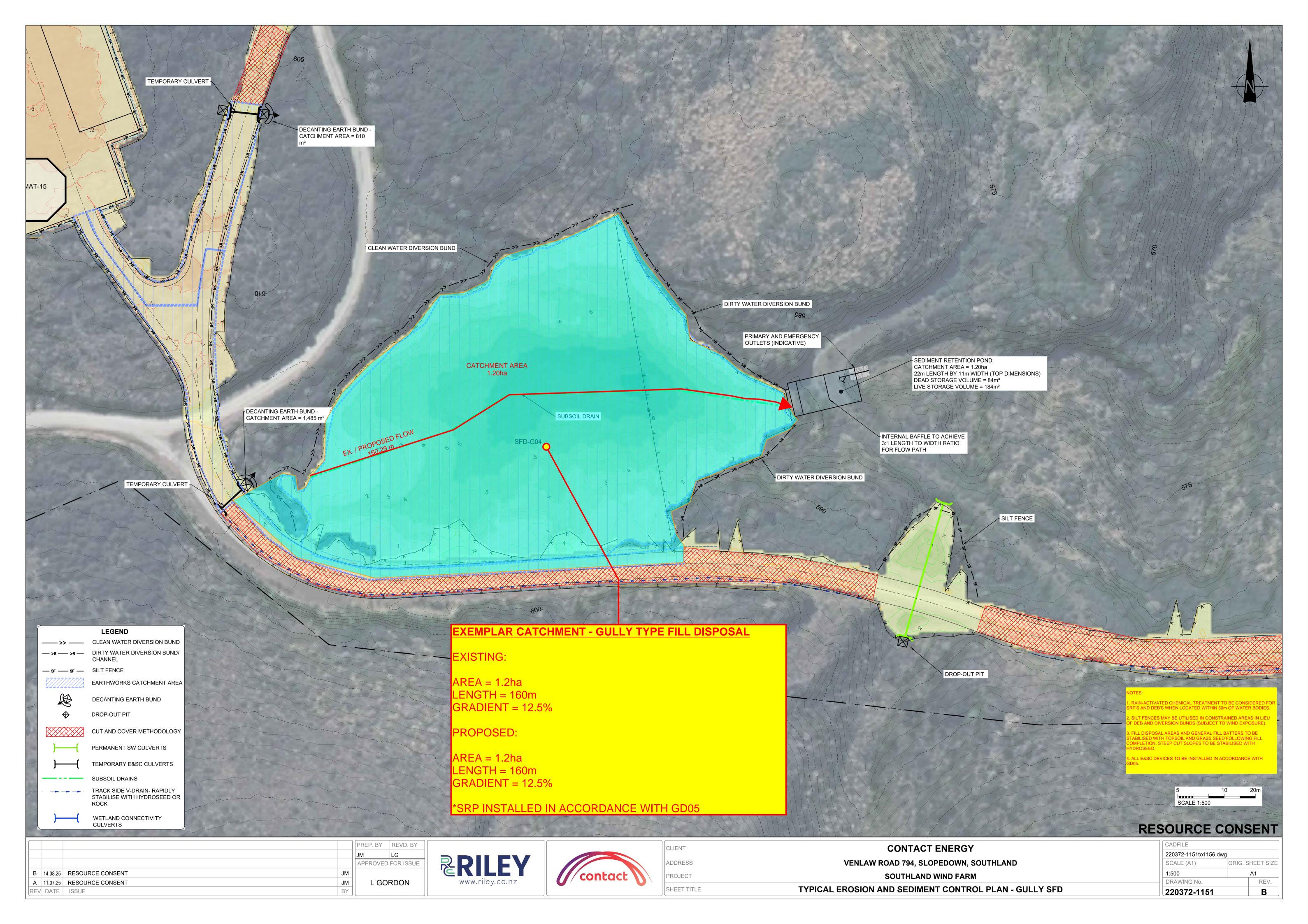
| Area/Activity | R | к | Slope Length (m) | Slope Grade (%) | LS | Surface Type | С | P | Exposed Area (ha) | Duration (months) | A (T) | Sediment Delivery Ratio (%) | E&SC Device | Sediment Control Efficiency (%) | Estimated Sediment Yield (T) |
|--|-------|------|---------------------|--------------------|------|---------------------------------------|-----------|---------------|----------------------|----------------------|----------|-----------------------------|----------------|----------------------------------|---------------------------------|
| | | | | | | | | Pre-develo | pment | | | | | | |
| Existing Site | 23.04 | 0.13 | 75 | 21.0% | 6.40 | Native vegetation (undisburbed) | 0.01 | 1.00 | 0.75 | 6 | 0.073 | 70% | N/A | 0% | 0.051 |
| | | | | | | | | | | | | | | Subtotal = | 0.051 |
| Unmitigated Earthworks (Construction Period) | | | | | | | | | | | | | | | |
| Platform construction | 23.04 | 0.40 | 50 | 10.0% | 1.75 | Bare Soil - compacted and smooth | 1.00 | 1.32 | 0.40 | 3 | 2.107 | 50% | N/A | 0% | 1.054 |
| Slope construction | 23.04 | 0.40 | 25 | 20.0% | 3.70 | Bare Soil -rough irregular surface | 1.00 | 0.90 | 0.35 | 3 | 2.658 | 50% | N/A | 0% | 1.329 |
| Slope stabilisation | 23.04 | 0.13 | 25 | 33.0% | 8.55 | Mulch on topsoil | 0.05 | 1.00 | 0.35 | 3 | 0.112 | 70% | N/A | 0% | 0.078 |
| | | | | | | | Mitigated | Earthworks (C | Construction Pe | eriod) | | | | Subtotal = | 2.461 |
| Platform construction | 23.04 | 0.40 | 50 | 10.0% | 1.75 | Bare Soil - compacted and smooth | 1.00 | 1.32 | 0.40 | 3 | 2.107 | 50% | 4 | 70% | 0.316 |
| Slope construction | 23.04 | 0.40 | 25 | 20.0% | 3.70 | Bare Soil -rough irregular surface | 1.00 | 0.90 | 0.35 | 3 | 2.658 | 50% | 4 | 70% | 0.399 |
| Slope stabilisation | 23.04 | 0.13 | 25 | 33.0% | 8.55 | Mulch on topsoil | 0.05 | 1.00 | 0.35 | 3 | 0.112 | 70% | 4 | 70% | 0.024 |
| Notes: | | | | | | | _ | | | | | | | Subtotal = | 0.738 |

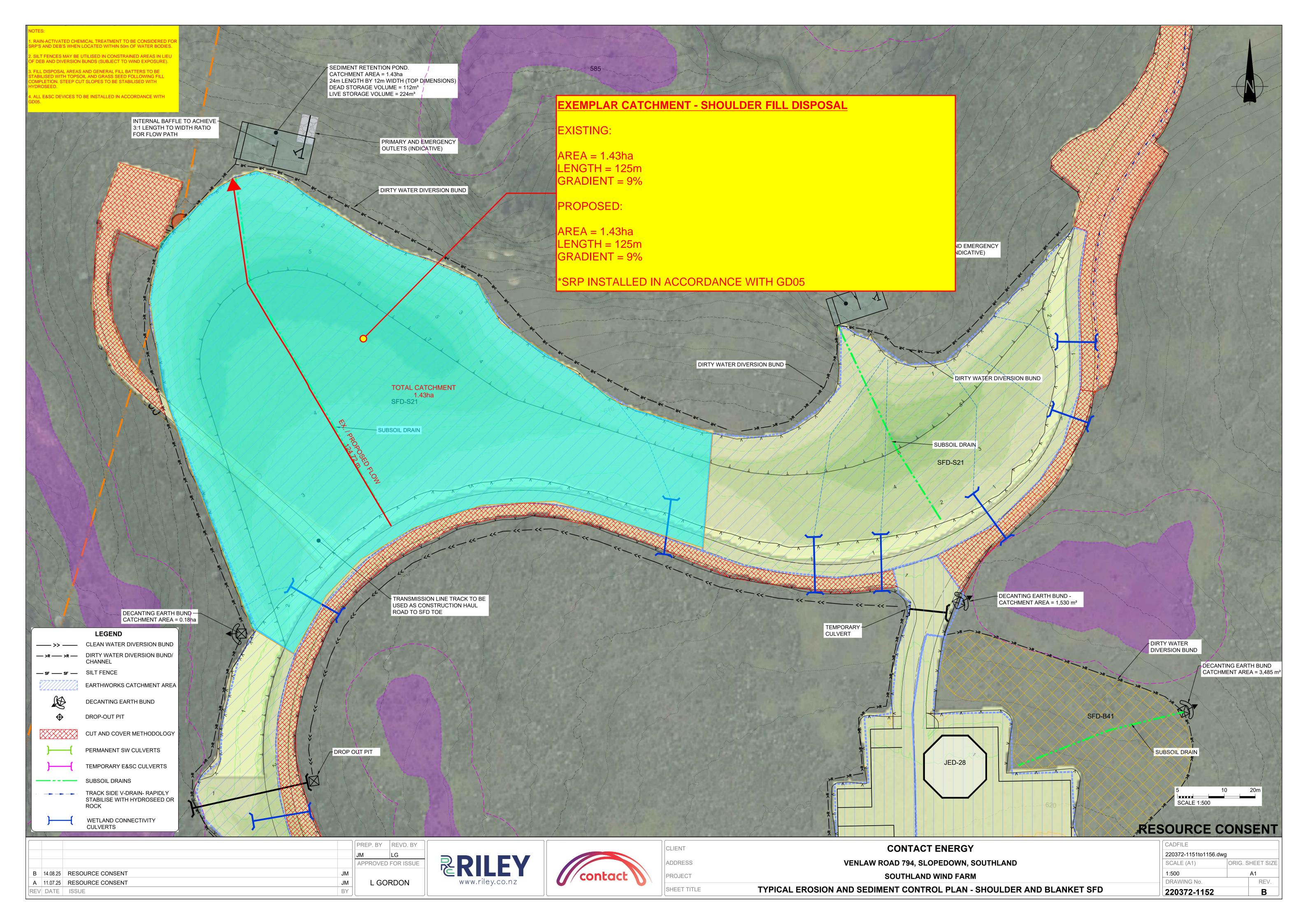
²⁾ Soil Erodability Factor determined based on observed soil composition and Triangular Nomograph for Estimating K values (refer to Auckland Regional Council S-05 - Figure 1).

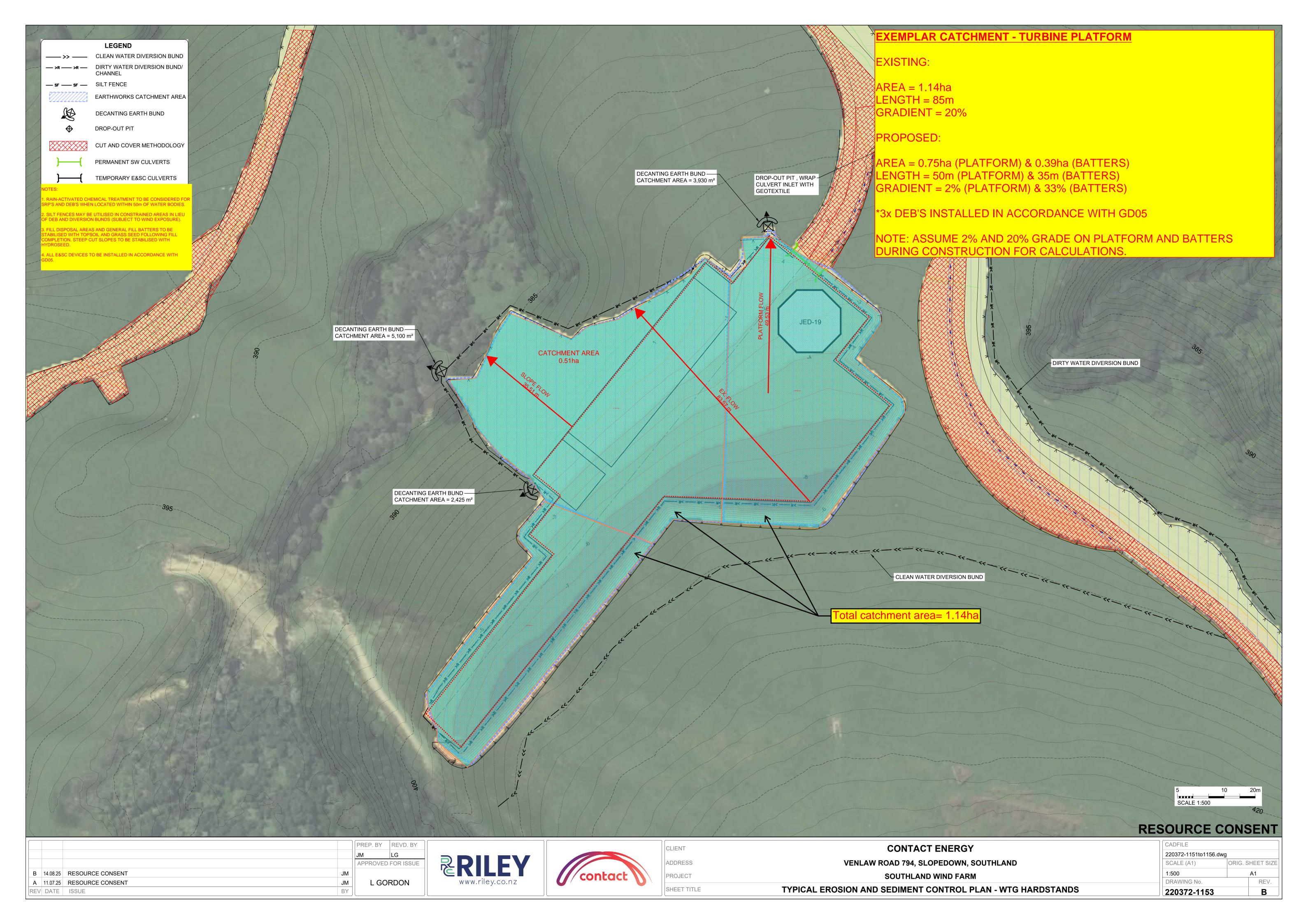
³⁾ Slope Length and Steepness Factor based on site topography and corresponding values presented in Auckland Regional Council S-05 - Appendix 1.

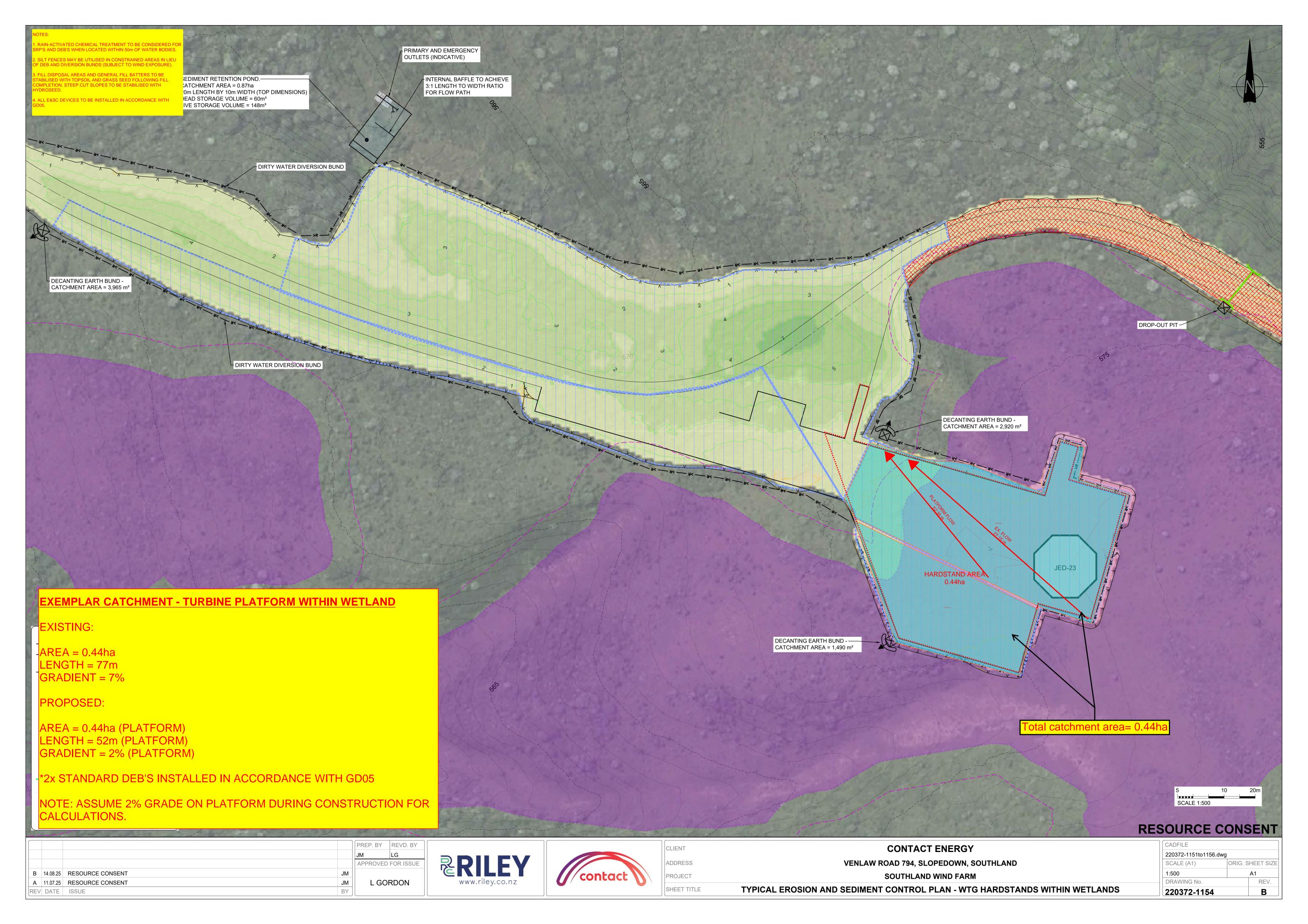
⁴⁾ Ground Cover and Roughness Factors based on surface cover type and corresponding values presented in Auckland Regional Council S-05 - Table 2.

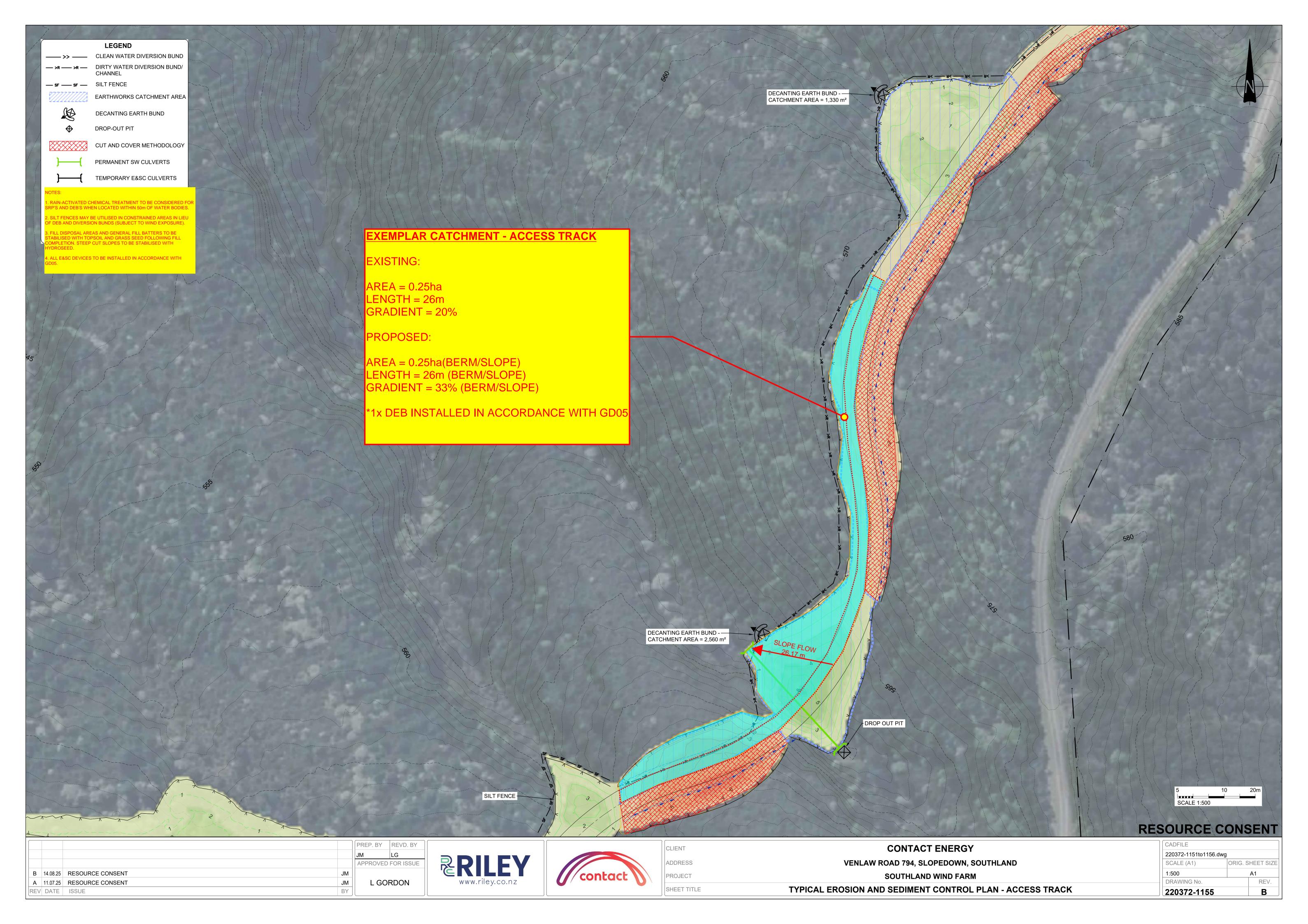
^{5) 50%} Sediment Delivery Ratio is generally acceptable except where sites are steep (i.e., 70% for sites where slopes exceed 10-degrees (or 17.5%)).

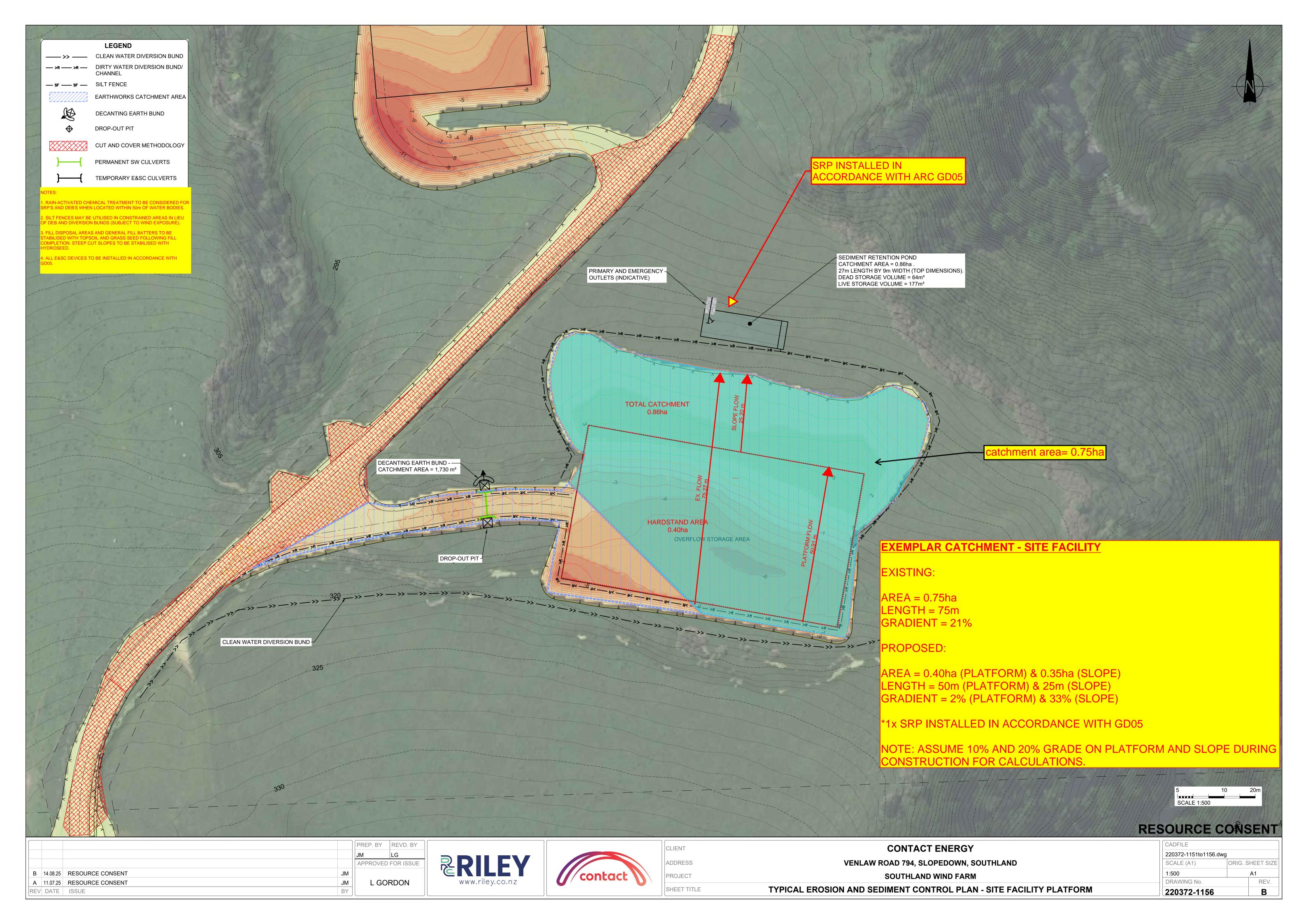












Southland Wind Farm

Job Name:



Job Number: 220372 Prepared by: Reviewed by: LG 07.08.2025 Date: SFD-G04 Fill disposal Location Catchment Area 1.2 ha Slope of earthworks 9.5 % Slope < 10% minimum volume of 2 % of the contributing catchment Slope > 10% minimum volume of 3 % of the contributing catchment 240 m³ Minimum Volume of Pond 72 m³ Dead Storage Volume 30% of minimum volume of pond 168 m³ 70% of minimum volume of pond Live Storage Volume Shape of pond 3 Inlet side slope (Spreader) 1 General side slopes 2:1 typically Length to Width ratio : Should range between 3:1 and 5:1 or utilise internal baffles Depth of Pond 2 Should range between 1 to 2m depth m 1 Depth of Dead Storage min 0.4m m Depth of Live Storage 1 m Width (top) 11 m Width (junc btw top & bottom) 7 m Length (top) 22 m Length (junc btw top & bottom) 18 m Width (bottom) 3 m Length (bottom) 14 m Freeboard dimensions Freeboard depth 0.3 m Width (top) 12.2 m Length (top) 23.5 m **Calculated Storage** 84 m³ **PASS** Dead Storage Volume 184 m³ PASS Live Storage Volume **268** m³ Total Storage Volume **PASS Forebay Design** Width 11 m = width in accordance with GD05 Depth 1 m in accordance with GD05 in accordance with GD05 Length 2 m **Decants** Max outflow rate 3 l/sec/ha (200 holes per decant) Max flow for each decant 4.5 l/sec Number of decants required 0.80 160 holes **Emergency Spillway** Base width 3 m 3m min Depth 0.3 0.3m minimum m Side slopes 3 gradient 1.03 m³/sec Flow Capacity (Qw) **PASS** $\mathbf{Q}_{(100)}$ Design Flows 0.25 m³/sec (From TP108 Calcs - upstream catchment with CN value of 91 for bare earth) Q₍₁₀₀₎



Job Name: Southland Wind Farm
Job Number: 220372
Prepared by: AR
Reviewed by: LG
Date: 07.08.2025

SFD-21 catchment 1 Location Catchment Area 1.43 ha Slope of earthworks 9.5 % Slope < 10% minimum volume of 2 % of the contributing catchment Slope > 10% minimum volume of 3 % of the contributing catchment 286 m³ Minimum Volume of Pond $85.8\ \text{m}^3$ Dead Storage Volume 30% of minimum volume of pond 200.2 m³ 70% of minimum volume of pond Live Storage Volume Shape of pond Inlet side slope (Spreader) 3 2:1 typically General side slopes Length to Width ratio 2 : Should range between 3:1 and 5:1 or utilise internal baffles 2 Depth of Pond Should range between 1 to 2m depth m Depth of Dead Storage 1 m min 0.4m Depth of Live Storage 1 m Width (top) 12 Width (junc btw top & bottom) 8 m m 20 m Length (top) 24 m Length (junc btw top & bottom) Width (bottom) 4 m Length (bottom) 16 m Freeboard dimensions 0.3 m Freeboard depth Width (top) 13.2 m Length (top) 25.5 m **Calculated Storage 112** m³ PASS Dead Storage Volume **224** m³ Live Storage Volume **PASS** 336 m³ Total Storage Volume **PASS** Forebay Design Width 12 m = width in accordance with GD05 Depth 1 m in accordance with GD05 Length 2 m in accordance with GD05 Decants Max outflow rate 3 l/sec/ha Max flow for each decant 4.5 l/sec (200 holes per decant) 0.95 191 holes Number of decants required **Emergency Spillway** Base width m 3m min

 $\mathbf{Q}_{(100)}$ Design Flows

Flow Capacity (Qw)

Depth

Side slopes

Q₍₁₀₀₎ 0.3 m³/sec (From TP108 Calcs - upstream catchment with CN value of 91 for bare earth)

0.3m minimum

gradient

PASS

0.3

3

m

1.03 m³/sec



Job Name: Southland Wind Farm
Job Number: 220372
Prepared by: AR
Reviewed by: LG
Date: 07.08.2025

Reviewed by: Date: Location SFD-21 catchment 2 Catchment Area 0.71 ha 9.5 % Slope < 10% minimum volume of 2 % of the contributing catchment Slope of earthworks Slope > 10% minimum volume of 3 % of the contributing catchment 142 m³ Minimum Volume of Pond 42.6 m³ Dead Storage Volume 30% of minimum volume of pond 99.4 m³ Live Storage Volume 70% of minimum volume of pond Shape of pond Inlet side slope (Spreader) 3 General side slopes 2:1 typically 2 2 1.1 Should range between 3:1 and 5:1 or utilise internal baffles Length to Width ratio 1 Depth of Pond Should range between 1 to 2m depth m Depth of Dead Storage m min 0.4m Depth of Live Storage 0.9 m Width (top) 9 Width (junc btw top & bottom) 5.4 m Length (top) 18 Length (junc btw top & bottom) 14.4 m m Width (bottom) 1 m Length (bottom) 10 m Freeboard dimensions 0.3 m Freeboard depth Width (top) 10.2 m Length (top) 19.5 m **Calculated Storage** 48 m³ **PASS** Dead Storage Volume 108 m³ Live Storage Volume **PASS** 156 m³ Total Storage Volume **PASS Forebay Design** 9 m = width in accordance with GD05 Width in accordance with GD05 Depth 1 m 2 m in accordance with GD05 Length Decants 3 l/sec/ha Max outflow rate Max flow for each decant 4.5 l/sec (200 holes per decant) Number of decants required 0.47 95 holes **Emergency Spillway** Base width 3 m 3m min 0.3 0.3m minimum Depth m Side slopes 3 gradient 1.03 m³/sec Flow Capacity (Qw) #REF! **Q**₍₁₀₀₎ Design Flows

0.146 m³/sec

 $Q_{(100)}$

(From TP108 Calcs - upstream catchment with CN value of 91 for bare earth)



Southland Wind Farm Job Name: Job Number: 220372 Prepared by: AR Reviewed by: LG Date: 07.08.2025

Q₍₁₀₀₎ Design Flows

 $Q_{(100)}$

Location SFD near JED 23 Hardstand Catchment Area 0.87 ha Slope of earthworks 9.5 % Slope < 10% minimum volume of of the contributing catchment Slope > 10% minimum volume of 3 % of the contributing catchment 174 m^3 Minimum Volume of Pond 52.2 m³ Dead Storage Volume 30% of minimum volume of pond 121.8 m³ Live Storage Volume 70% of minimum volume of pond Shape of pond Inlet side slope (Spreader) 3 General side slopes 2:1 typically 2 Length to Width ratio Should range between 3:1 and 5:1 or utilise internal baffles Depth of Pond m Should range between 1 to 2m depth Depth of Dead Storage m min 0.4m Depth of Live Storage m Width (top) 10 m Width (junc btw top & bottom) 6 m Length (top) 20 m Length (junc btw top & bottom) 16 m Width (bottom) 2 m 12 Length (bottom) m Freeboard dimensions 0.3 m 11.2 m Freeboard depth Width (top) 21.5 m Length (top) **Calculated Storage** 60 m³ Dead Storage Volume PASS 148 m³ Live Storage Volume **PASS** 208 m³ **PASS** Total Storage Volume **Forebay Design** 10 m = width in accordance with GD05 Width in accordance with GD05 Depth 1 m in accordance with GD05 Length 2 m Decants 3 l/sec/ha Max outflow rate Max flow for each decant 4.5 l/sec (200 holes per decant) Number of decants required 116 holes 0.58 **Emergency Spillway** Base width 3m min m Depth 0.3 0.3m minimum m Side slopes 3 gradient 1.03 m³/sec Flow Capacity (Qw) PASS

0.182 m³/sec

(From TP108 Calcs - upstream catchment with CN value of 91 for bare earth)



Job Name: Southland Wind Farm
Job Number: 220372
Prepared by: AR
Reviewed by: LG
Date: 07.08.2025

Location Overflow storage area 0.8614 ha Catchment Area Slope of earthworks 9.5 % Slope < 10% minimum volume of 2 % of the contributing catchment Slope > 10% minimum volume of 3 % of the contributing catchment 172.28 m³ Minimum Volume of Pond 51.684 m³ Dead Storage Volume 30% of minimum volume of pond 120.596 m³ Live Storage Volume 70% of minimum volume of pond Shape of pond Inlet side slope (Spreader) 3 General side slopes 2:1 typically Length to Width ratio Depth of Pond Should range between 3:1 and 5:1 or utilise internal baffles 3 : 1 2 Should range between 1 to 2m depth m Depth of Dead Storage m min 0.4m Depth of Live Storage 1 m Width (top) 9 Width (junc btw top & bottom) m 5 m 27 m Length (top) Length (junc btw top & bottom) 22 m Width (bottom) m Length (bottom) 17 m Freeboard dimensions Freeboard depth 0.3 m Width (top) 10.2 m Length (top) 28.5 m **Calculated Storage 64** m³ **PASS** Dead Storage Volume 177 m³ PASS Live Storage Volume **240** m³ Total Storage Volume **PASS** Forebay Design Width 9 m = width in accordance with GD05 Depth in accordance with GD05 1 m 2 m in accordance with GD05 Length **Decants** Max outflow rate 3 l/sec/ha Max flow for each decant (200 holes per decant) 4.5 l/sec Number of decants required 0.57 115 holes **Emergency Spillway** 3 m Base width 3m min Depth 0.3 m 0.3m minimum Side slopes 3 gradient 1.03 m³/sec Flow Capacity (Qw) **PASS** $\mathbf{Q}_{(100)}$ Design Flows

0.18 m³/sec

 $Q_{(100)}$

(From TP108 Calcs - upstream catchment with CN value of 91 for bare earth)