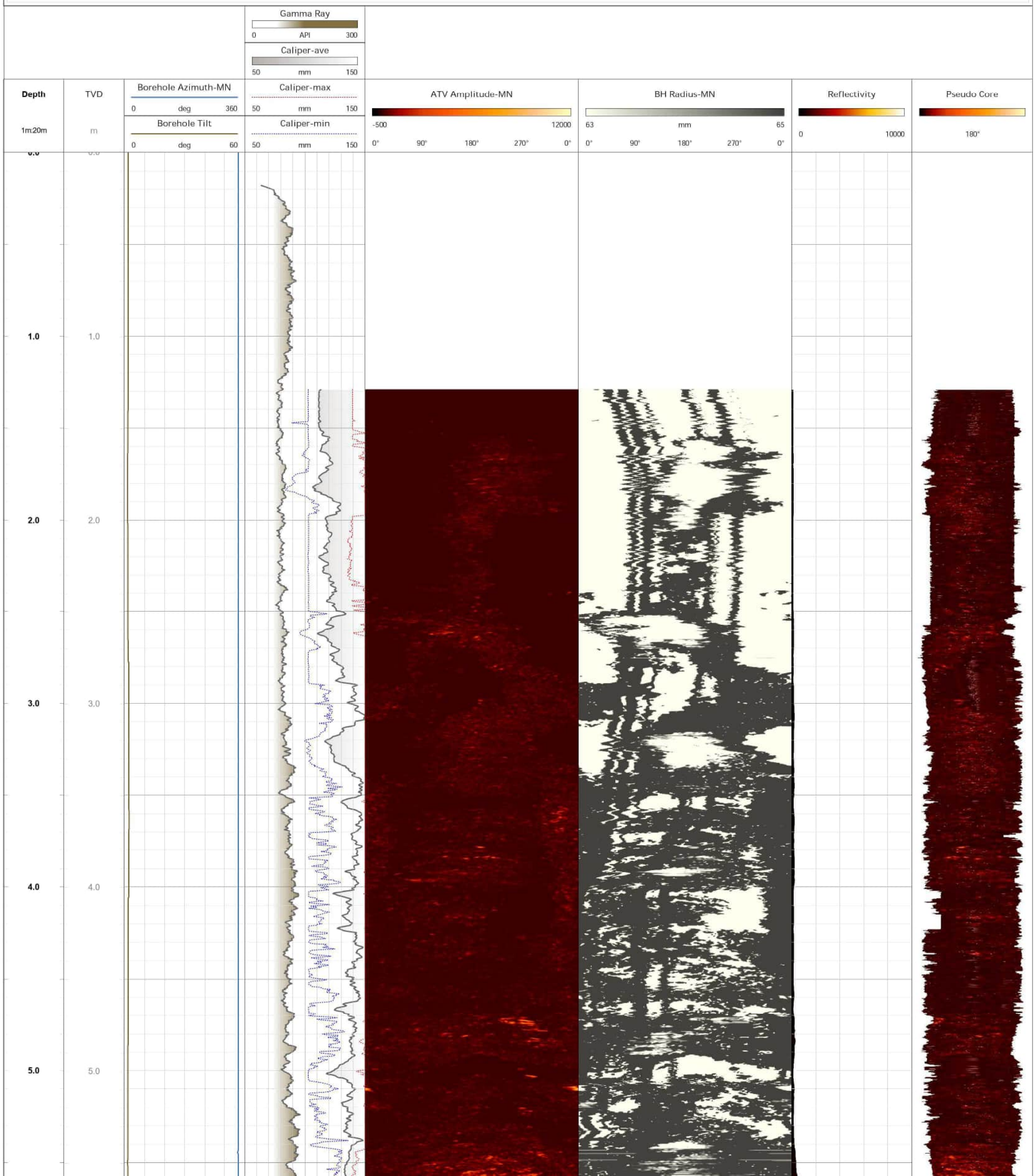
Well Name:	MDD333
Surveys:	ATV (Pre-Processing Plot)
Location:	
Company:	

Service Company:	SPEIGHT DRILLING LTD	Log Measured From:	Ground Level		
Operator:	Gareth	Drilling Measured From:	Ground Level		
Date Logged:	15 June 2024	Driller Depth:		Logger Depth:	
Drilling Company:		Inclination:	-88.7°	Heading:	324.4° (MN)
Date Drilled:		Easting:		Northing:	
Field:		Elevation:		Grid:	
County / Township:		Log Top:	0.0	Log Bottom:	43.75
State / Province:					
Country:		Depth unit:	Meters	Scale ratio:	1 : 20

Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
						334970	334G-042
						Wireline Length:	Depth Factor:
						1800	10501/1m

Remarks:



6.0

7.0

8.0

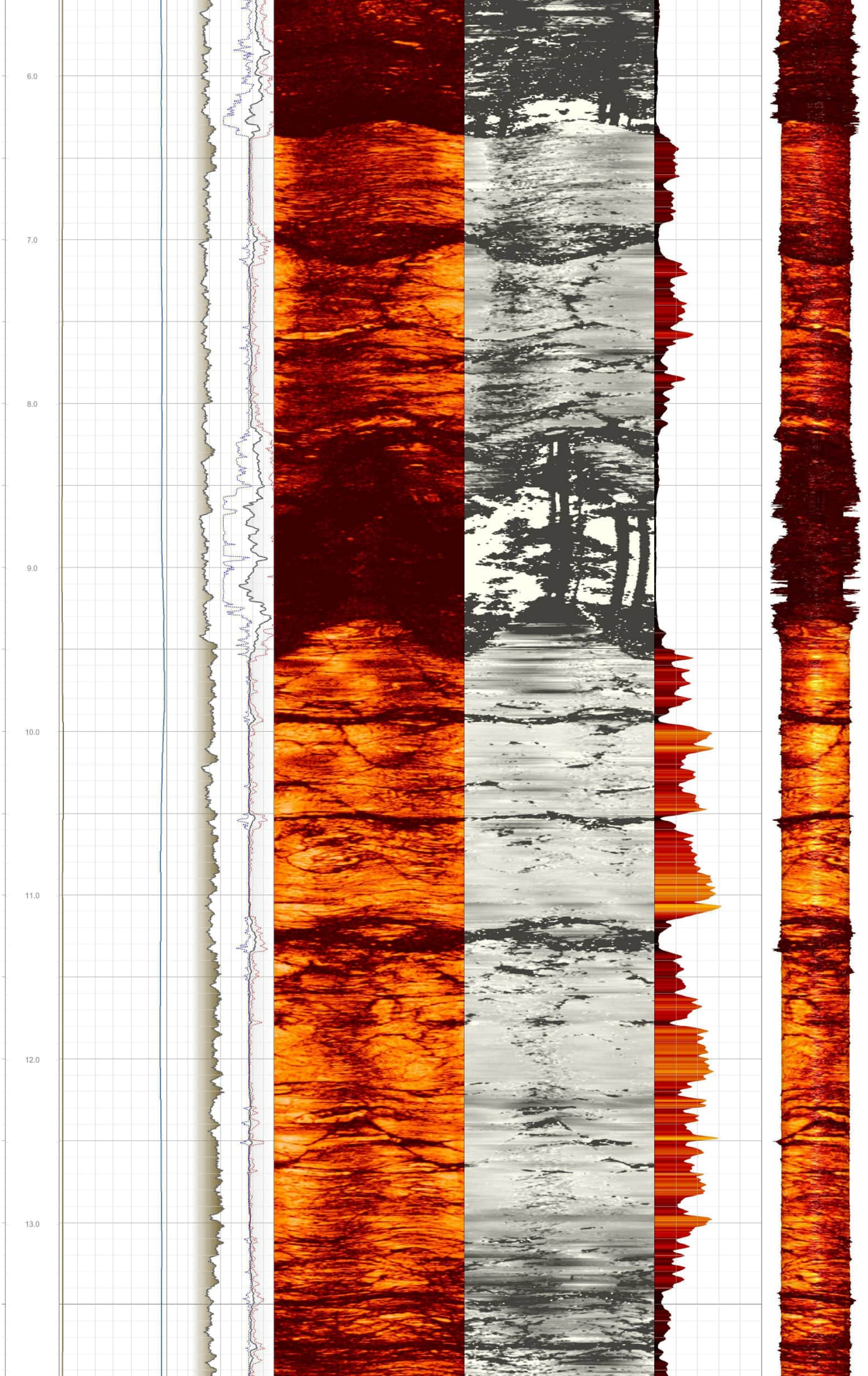
9.0

10.0

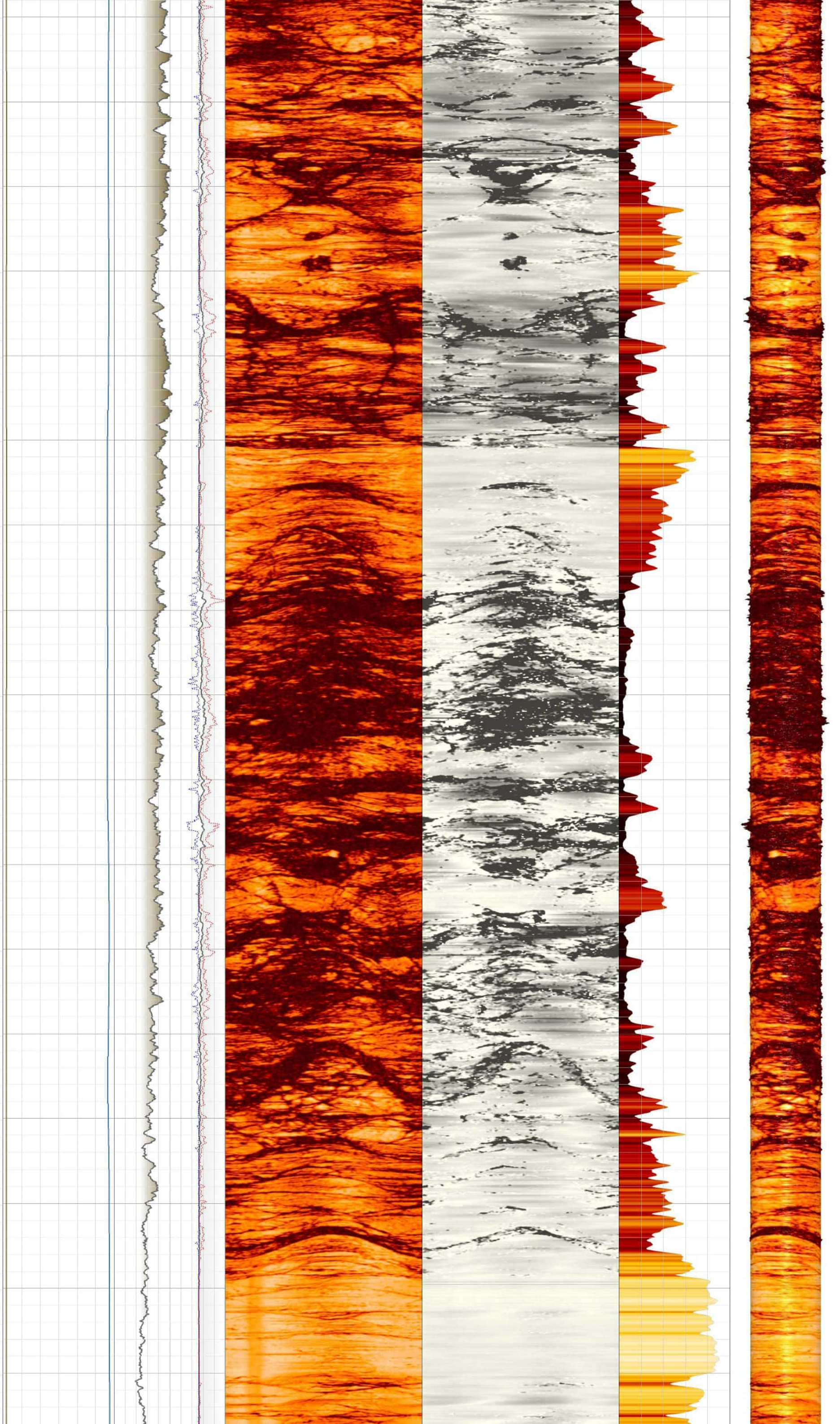
11.0

12.0

13.0



14.0
15.0
16.0
17.0
18.0
19.0
20.0
21.0
22.0



23.0

24.0

25.0

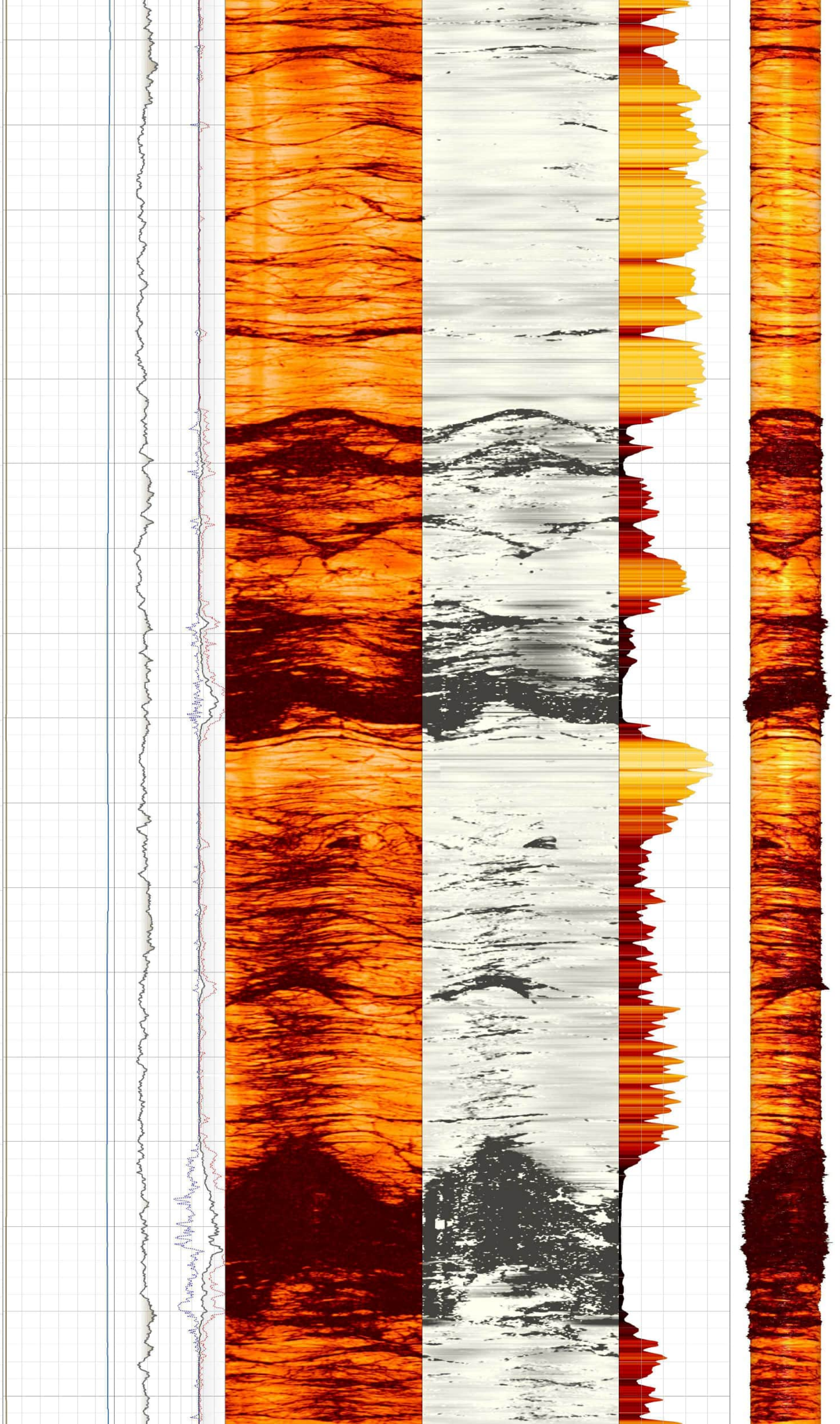
26.0

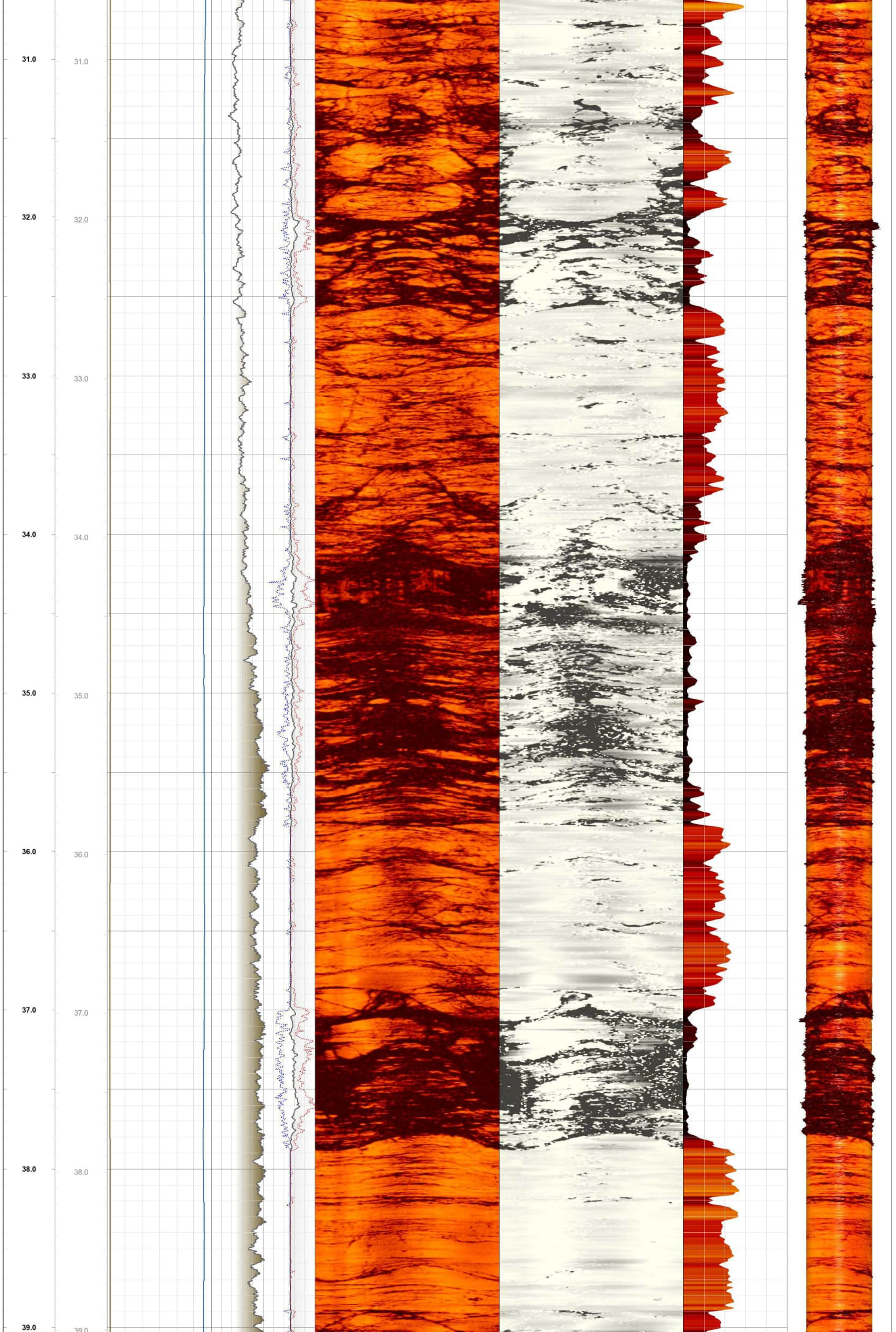
27.0

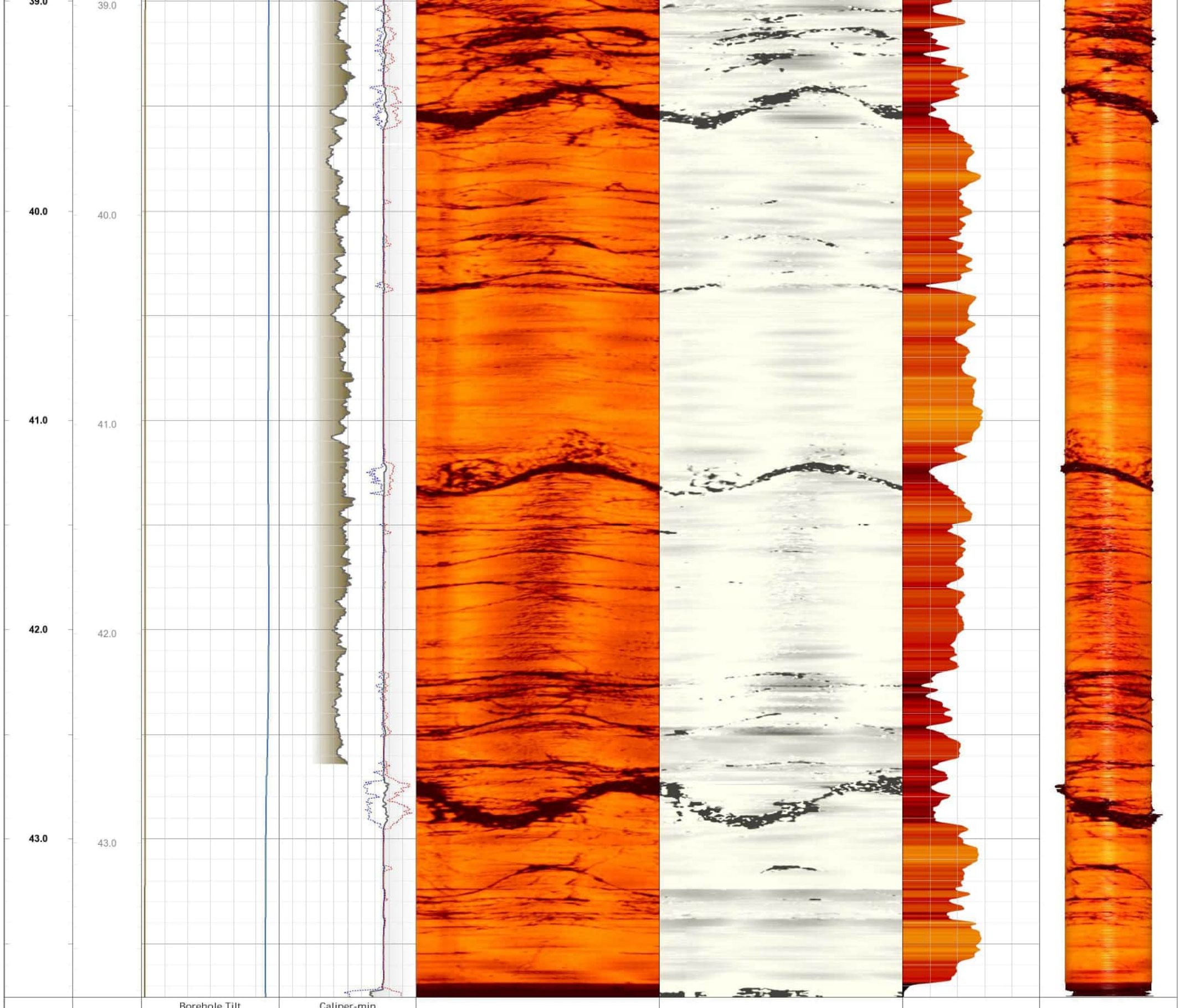
28.0

29.0

30.0




31.0
31.0
32.0
32.0
33.0
33.0
34.0
34.0
35.0
35.0
36.0
36.0
37.0
37.0
38.0
38.0
39.0
39.0


39.0
40.0
41.0
42.0
43.0
Depth
TVD
1m:20m
m
Borehole Tilt
0 deg 60
Borehole Azimuth-MN
0 deg 360
Caliper-min
50 mm 150
Caliper-max
50 mm 150
Caliper-ave
50 mm 150
Gamma Ray
0 API 300
ATV Amplitude-MN
-500 12000
0° 90° 180° 270° 0°
BH Radius-MN
63 mm 65
0° 90° 180° 270° 0°
Reflectivity
0 10000
Pseudo Core
180°

Well Name:	MDD394
Surveys:	ATV, OTV, GR
Location:	Bendigo
Company:	Santana

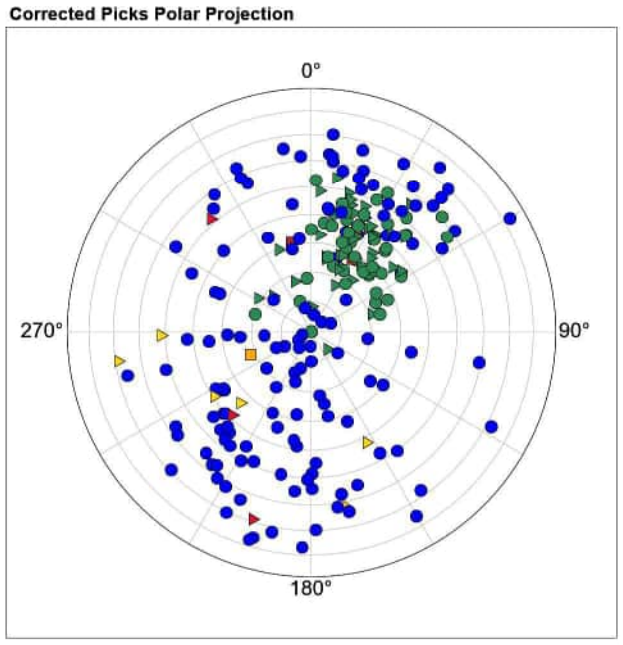
Service Company:	SPEIGHT DRILLING
Operator:	Gareth Speight
Date Logged:	10/12/2024
Drilling Company:	SPEIGHT DRILLING
Date Drilled:	
Field:	
County / Township:	
State / Province:	
Country:	

Log Measured From:	Ground Level		
Drilling Measured From:	Ground Level		
Driller Depth:		Logger Depth:	30.4
Inclination:	-88°	Heading:	053° (TN)
Easting:		Northing:	
Elevation:		Grid:	True North (22.5°)
Log Top:	1.4	Log Bottom:	30.4
Depth unit:	Meters	Scale ratio:	1 : 20

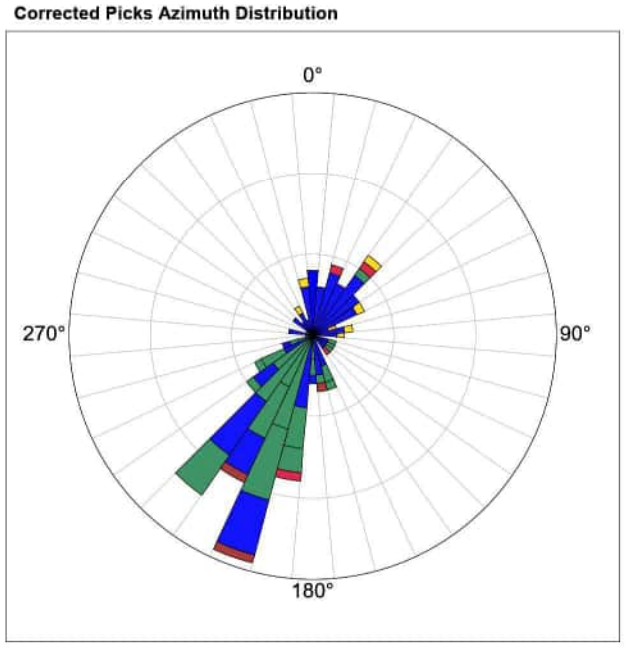
Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
HQ	0	30	PQ	0	7.5		
						Wireline Length:	Depth Factor:

Remarks:
Poor borehole conditions impacting structural interpretation confidence.

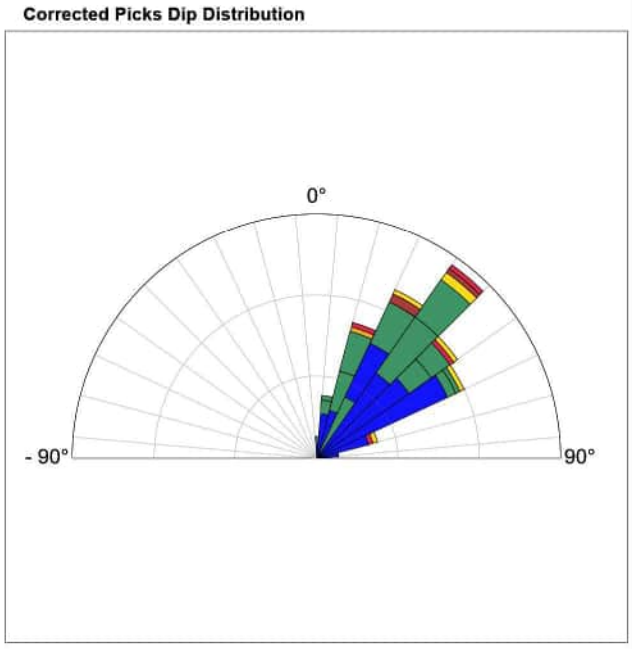
Corrected Picks Polar Projection



Corrected Picks Azimuth Distribution



Corrected Picks Dip Distribution



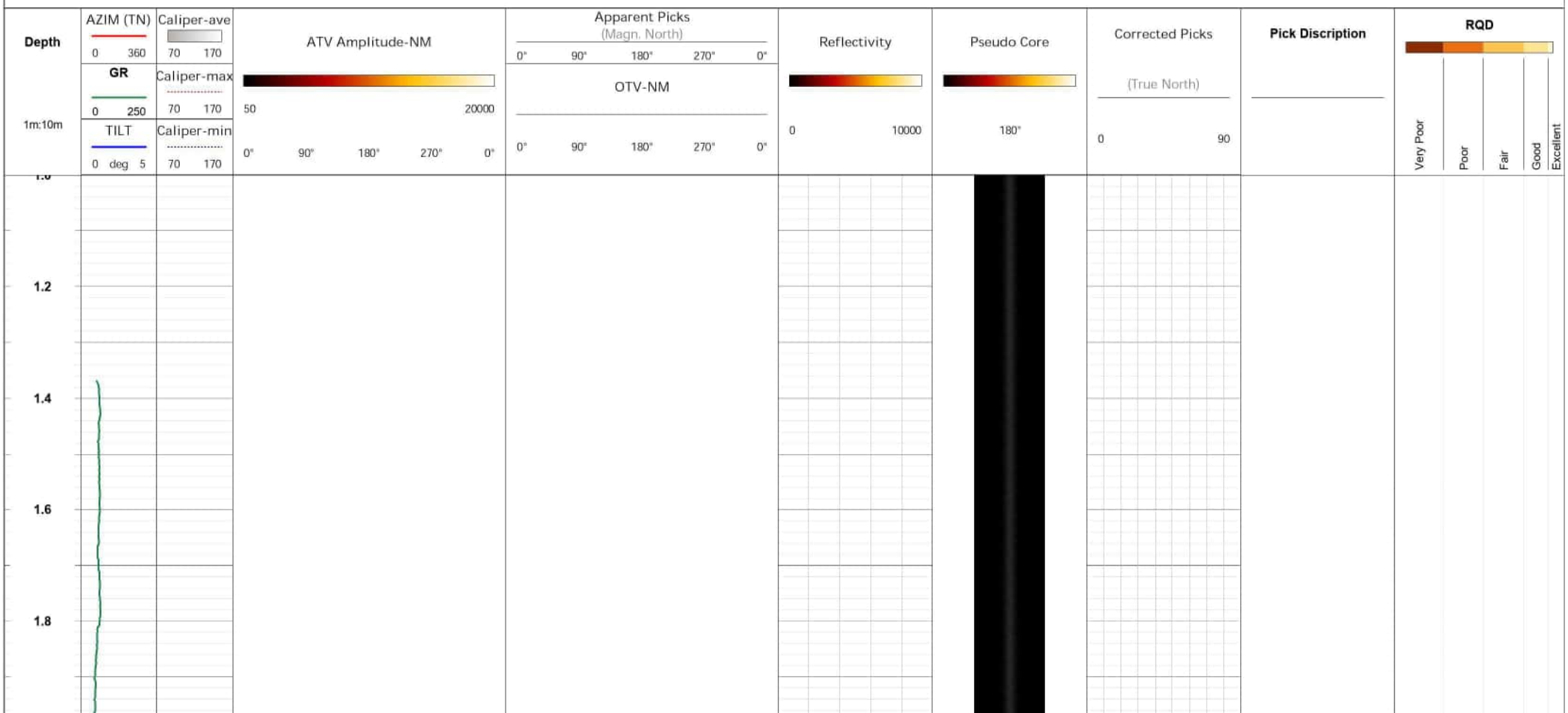
Legend:

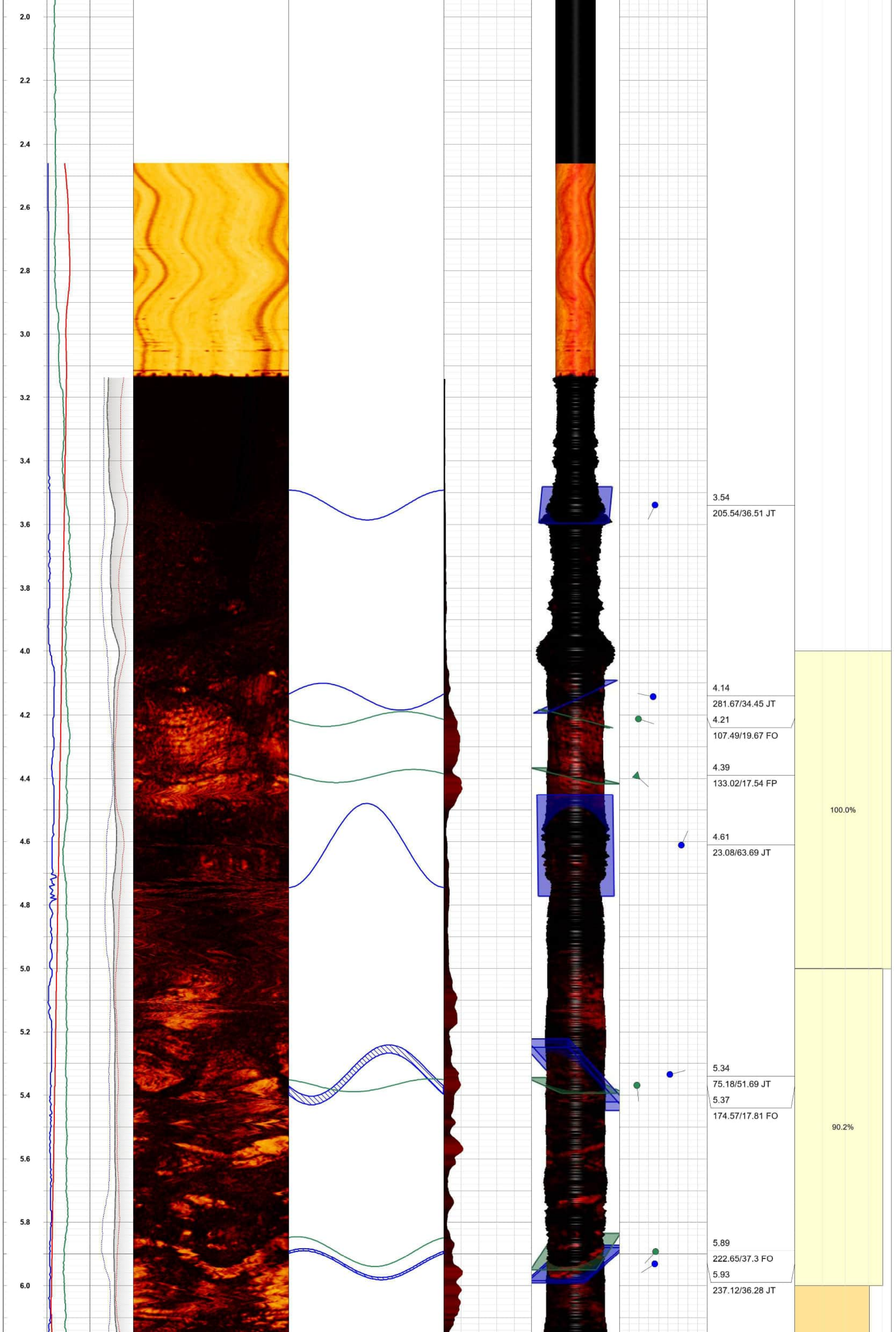
FO - Foliation | FP - Foliation Parting | JT - Joint | FZ - Fractured Zone | SH - Shear | CZ - Crushed Zone | V - Vein

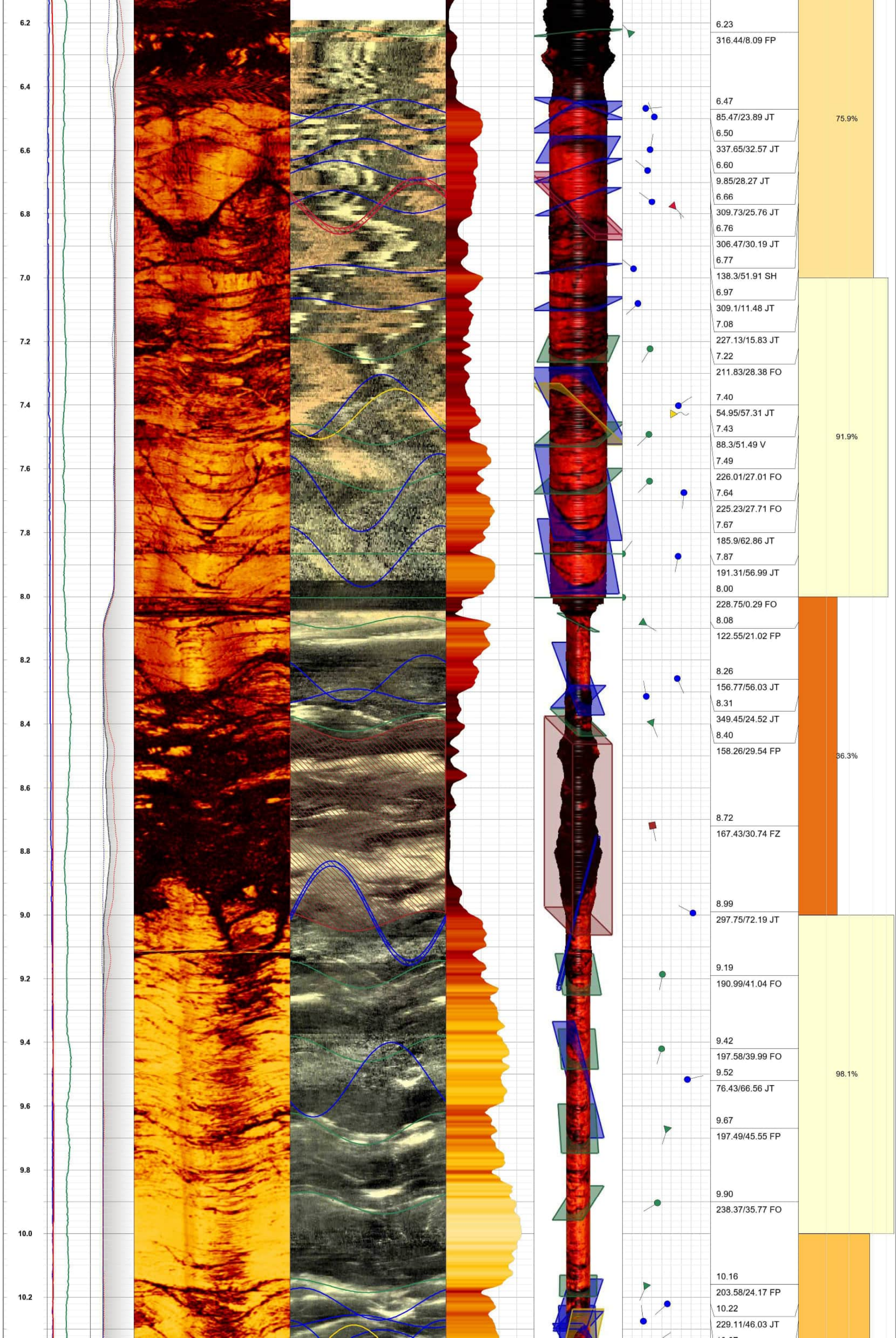
Curve Description:

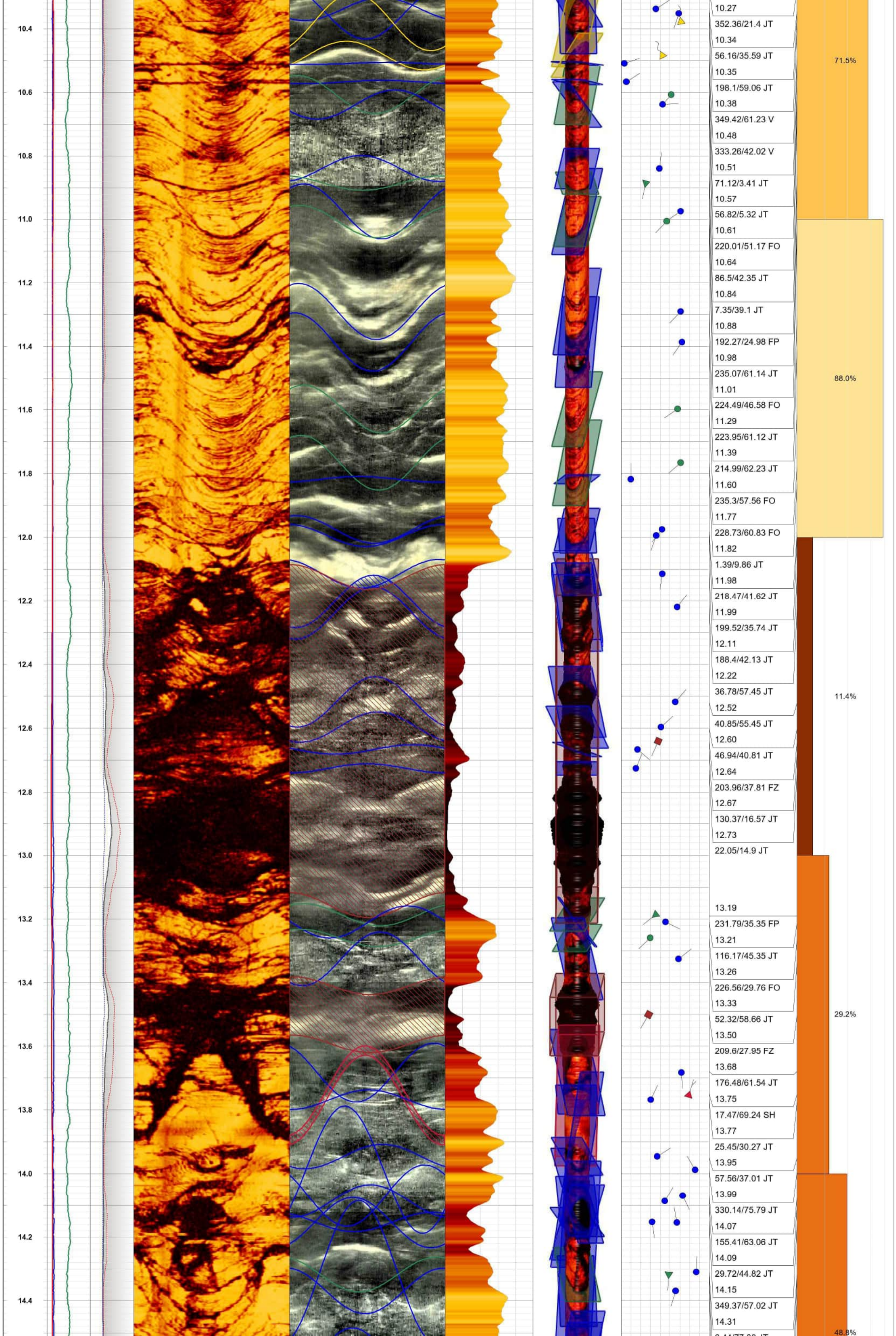
Title	Description	Top [m]	Base [m]	Tool s/n	Run / Date
Depth	Measured depth	1.4	30.4		
TVD	True vertical depth	1.4	30.4		
Tilt	Deviation from the vertical	1.4	30.4		
AZIM (TN)	Deviation from True North	1.4	30.4		
GR	Natural gamma ray	1.4	30.4	ABI/GR 220402	Run 2, 3, 6, 10/12/2024
Caliper	Borehole diameter from ATV traveltime, average, minimum, and maximum	1.4	30.4		
Apparent Picks	Uncorrected structure picks from ATV and OTV images	1.4	30.4		
ATV	ATV amplitude image (MN)	1.4	30.4	ABI/GR 220402	Run 2, 3, 6, 10/12/2024
OTV	OTV image (MN)	6.2	30	OBI 22204	Run 2, 3, 6, 10/12/2024
Reflectivity	Acoustic reflectivity of the rock	1.4	30.4		
Corrected Picks	Structure picks correxcted for borehole deviation (TN)	1.4	30.4		
Pick Discription	Structural pick discription, woth Azimuth, Dip Magnitude, and Type (TN)	1.4	30.4		
Pseudo Core	3D poresentation of ATV amp;litude, borehole radius and apparent picks	1.4	30.4		
RQD	Rock Quality Designation	4	30		

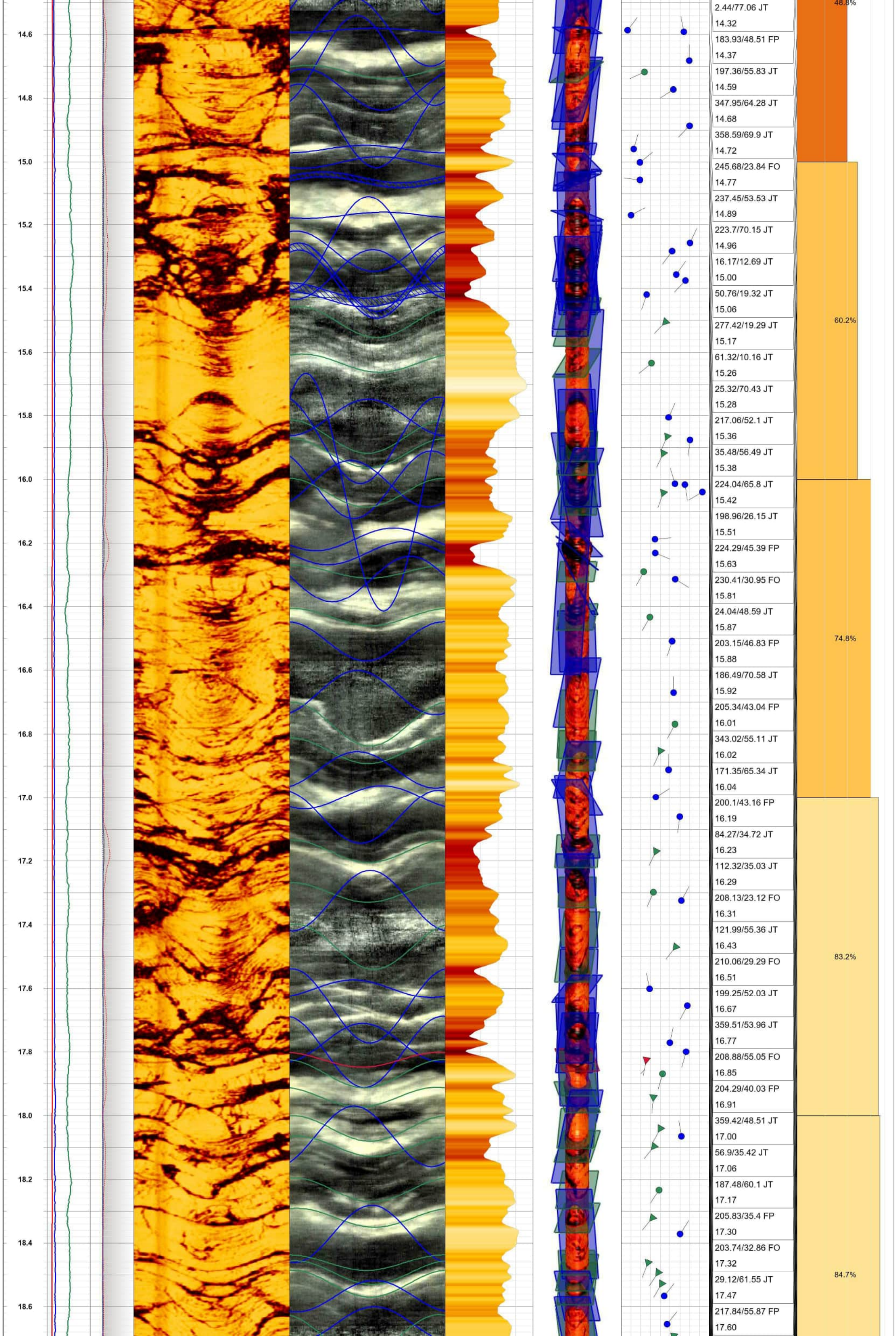
Disclaimer:

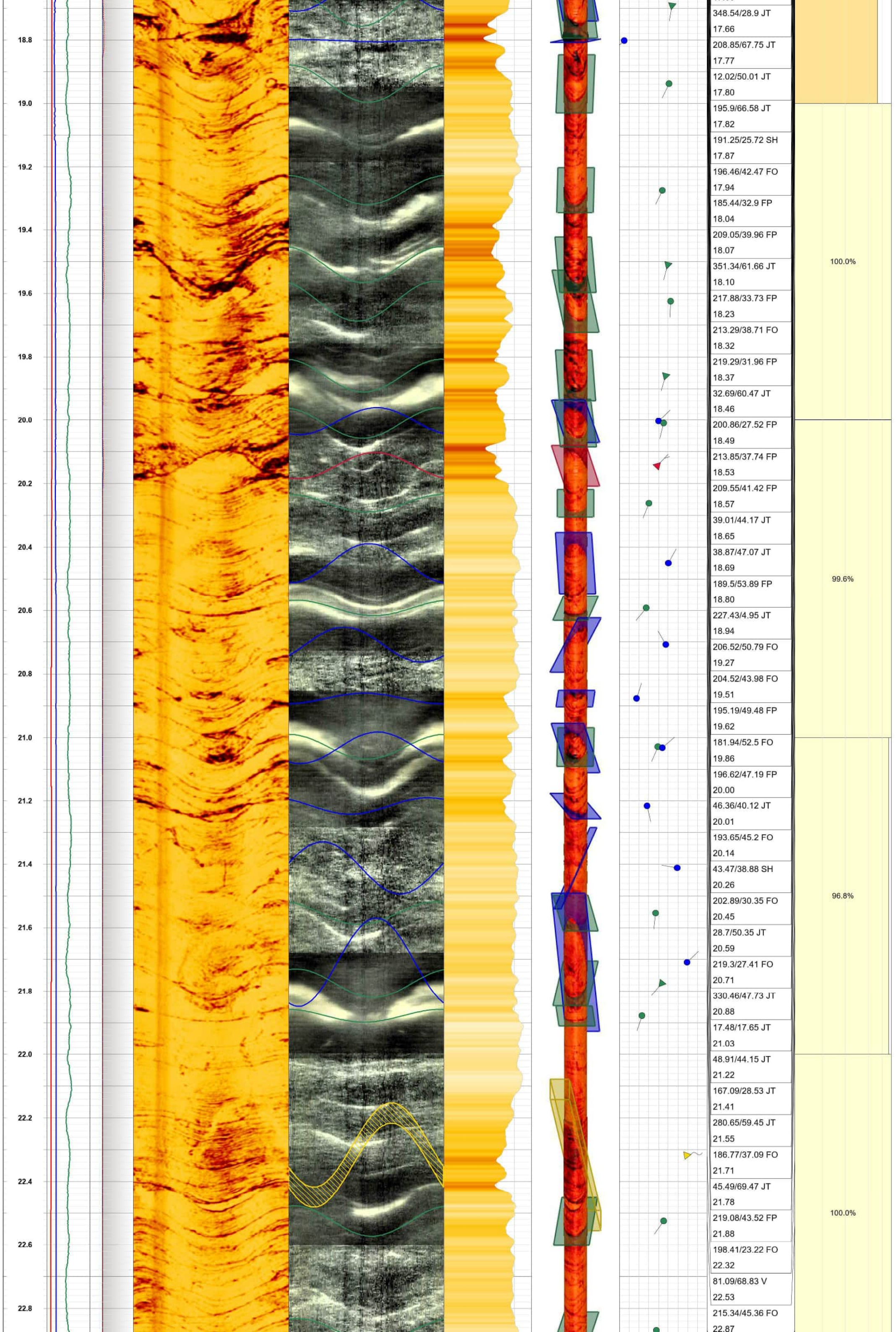



2.0
2.2
2.4
2.6
2.8
3.0
3.2
3.4
3.6
3.8
4.0
4.2
4.4
4.6
4.8
5.0
5.2
5.4
5.6
5.8
6.0
3.54
205.54/36.51 JT
4.14
281.67/34.45 JT
4.21
107.49/19.67 FO
4.39
133.02/17.54 FP
4.61
23.08/63.69 JT
5.34
75.18/51.69 JT
5.37
174.57/17.81 FO
5.89
222.65/37.3 FO
5.93
237.12/36.28 JT
100.0%
90.2%


6.2
6.4
6.6
6.8
7.0
7.2
7.4
7.6
7.8
8.0
8.2
8.4
8.6
8.8
9.0
9.2
9.4
9.6
9.8
10.0
10.2
6.23
316.44/8.09 FP
6.47
85.47/23.89 JT
6.50
337.65/32.57 JT
6.60
9.85/28.27 JT
6.66
309.73/25.76 JT
6.76
306.47/30.19 JT
6.77
138.3/51.91 SH
6.97
309.1/11.48 JT
7.08
227.13/15.83 JT
7.22
211.83/28.38 FO
7.40
54.95/57.31 JT
7.43
88.3/51.49 V
7.49
226.01/27.01 FO
7.64
225.23/27.71 FO
7.67
185.9/62.86 JT
7.87
191.31/56.99 JT
8.00
228.75/0.29 FO
8.08
122.55/21.02 FP
8.26
156.77/56.03 JT
8.31
349.45/24.52 JT
8.40
158.26/29.54 FP
8.72
167.43/30.74 FZ
8.99
297.75/72.19 JT
9.19
190.99/41.04 FO
9.42
197.58/39.99 FO
9.52
76.43/66.56 JT
9.67
197.49/45.55 FP
9.90
238.37/35.77 FO
10.16
203.58/24.17 FP
10.22
229.11/46.03 JT
75.9%
91.9%
36.3%
98.1%


10.4
10.6
10.8
11.0
11.2
11.4
11.6
11.8
12.0
12.2
12.4
12.6
12.8
13.0
13.2
13.4
13.6
13.8
14.0
14.2
14.4
10.27
352.36/21.4 JT
10.34
56.16/35.59 JT
10.35
198.1/59.06 JT
10.38
349.42/61.23 V
10.48
333.26/42.02 V
10.51
71.12/3.41 JT
10.57
56.82/5.32 JT
10.61
220.01/51.17 FO
10.64
86.5/42.35 JT
10.84
7.35/39.1 JT
10.88
192.27/24.98 FP
10.98
235.07/61.14 JT
11.01
224.49/46.58 FO
11.29
223.95/61.12 JT
11.39
214.99/62.23 JT
11.60
235.3/57.56 FO
11.77
228.73/60.83 FO
11.82
1.39/9.86 JT
11.98
218.47/41.62 JT
11.99
199.52/35.74 JT
12.11
188.4/42.13 JT
12.22
36.78/57.45 JT
12.52
40.85/55.45 JT
12.60
46.94/40.81 JT
12.64
203.96/37.81 FZ
12.67
130.37/16.57 JT
12.73
22.05/14.9 JT
13.19
231.79/35.35 FP
13.21
116.17/45.35 JT
13.26
226.56/29.76 FO
13.33
52.32/58.66 JT
13.50
209.6/27.95 FZ
13.68
176.48/61.54 JT
13.75
17.47/69.24 SH
13.77
25.45/30.27 JT
13.95
57.56/37.01 JT
13.99
330.14/75.79 JT
14.07
155.41/63.06 JT
14.09
29.72/44.82 JT
14.15
349.37/57.02 JT
14.31
71.5%
88.0%
11.4%
29.2%
48.8%

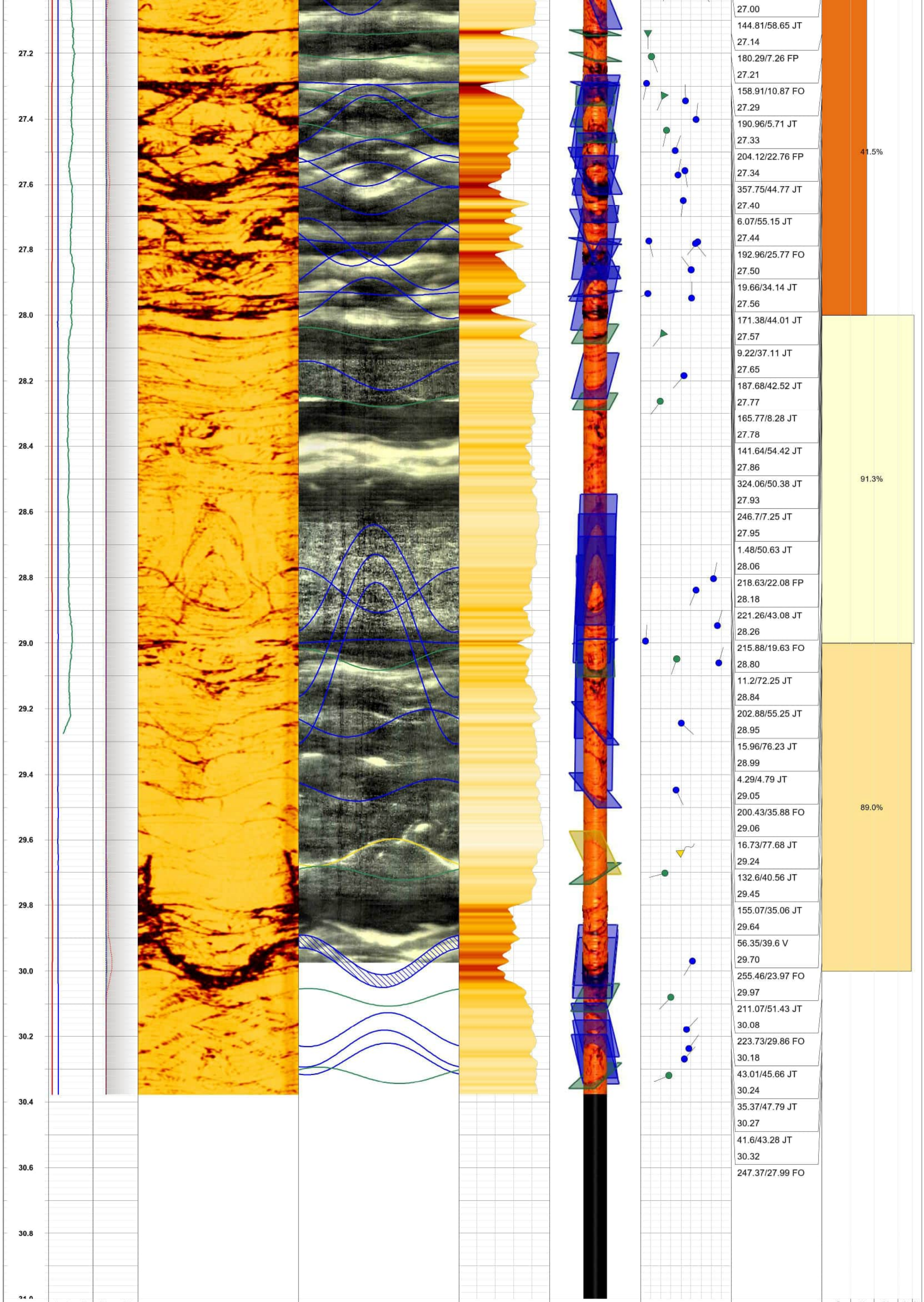

14.6
14.8
15.0
15.2
15.4
15.6
15.8
16.0
16.2
16.4
16.6
16.8
17.0
17.2
17.4
17.6
17.8
18.0
18.2
18.4
18.6
2.44/77.06 JT
14.32
183.93/48.51 FP
14.37
197.36/55.83 JT
14.59
347.95/64.28 JT
14.68
358.59/69.9 JT
14.72
245.68/23.84 FO
14.77
237.45/53.53 JT
14.89
223.7/70.15 JT
14.96
16.17/12.69 JT
15.00
50.76/19.32 JT
15.06
277.42/19.29 JT
15.17
61.32/10.16 JT
15.26
25.32/70.43 JT
15.28
217.06/52.1 JT
15.36
35.48/56.49 JT
15.38
224.04/65.8 JT
15.42
198.96/26.15 JT
15.51
224.29/45.39 FP
15.63
230.41/30.95 FO
15.81
24.04/48.59 JT
15.87
203.15/46.83 FP
15.88
186.49/70.58 JT
15.92
205.34/43.04 FP
16.01
343.02/55.11 JT
16.02
171.35/65.34 JT
16.04
200.1/43.16 FP
16.19
84.27/34.72 JT
16.23
112.32/35.03 JT
16.29
208.13/23.12 FO
16.31
121.99/55.36 JT
16.43
210.06/29.29 FO
16.51
199.25/52.03 JT
16.67
359.51/53.96 JT
16.77
208.88/55.05 FO
16.85
204.29/40.03 FP
16.91
359.42/48.51 JT
17.00
56.9/35.42 JT
17.06
187.48/60.1 JT
17.17
205.83/35.4 FP
17.30
203.74/32.86 FO
17.32
29.12/61.55 JT
17.47
217.84/55.87 FP
17.60
48.8%
60.2%
74.8%
83.2%
84.7%


18.8
19.0
19.2
19.4
19.6
19.8
20.0
20.2
20.4
20.6
20.8
21.0
21.2
21.4
21.6
21.8
22.0
22.2
22.4
22.6
22.8
348.54/28.9 JT
17.66
208.85/67.75 JT
17.77
12.02/50.01 JT
17.80
195.9/66.58 JT
17.82
191.25/25.72 SH
17.87
196.46/42.47 FO
17.94
185.44/32.9 FP
18.04
209.05/39.96 FP
18.07
351.34/61.66 JT
18.10
217.88/33.73 FP
18.23
213.29/38.71 FO
18.32
219.29/31.96 FP
18.37
32.69/60.47 JT
18.46
200.86/27.52 FP
18.49
213.85/37.74 FP
18.53
209.55/41.42 FP
18.57
39.01/44.17 JT
18.65
38.87/47.07 JT
18.69
189.5/53.89 FP
18.80
227.43/4.95 JT
18.94
206.52/50.79 FO
19.27
204.52/43.98 FO
19.51
195.19/49.48 FP
19.62
181.94/52.5 FO
19.86
196.62/47.19 FP
20.00
46.36/40.12 JT
20.01
193.65/45.2 FO
20.14
43.47/38.88 SH
20.26
202.89/30.35 FO
20.45
28.7/50.35 JT
20.59
219.3/27.41 FO
20.71
330.46/47.73 JT
20.88
17.48/17.65 JT
21.03
48.91/44.15 JT
21.22
167.09/28.53 JT
21.41
280.65/59.45 JT
21.55
186.77/37.09 FO
21.71
45.49/69.47 JT
21.78
219.08/43.52 FP
21.88
198.41/23.22 FO
22.32
81.09/68.83 V
22.53
215.34/45.36 FO
22.87
100.0%
99.6%
96.8%
100.0%

23.0
23.2
23.4
23.6
23.8
24.0
24.2
24.4
24.6
24.8
25.0
25.2
25.4
25.6
25.8
26.0
26.2
26.4
26.6
26.8
27.0

22.87
221.98/37.92 FO
23.19
59.11/37.65 JT
23.23
214.47/37.9 FO
23.43
224.3/45.75 FO
23.55
87.81/28.26 JT
23.69
235.85/36.76 FP
23.84
112.33/33.51 JT
23.91
204.35/34.14 FP
24.05
84.63/15.68 JT
24.16
212.83/38.04 FP
24.23
191.25/36.51 FO
24.29
44.68/33.84 V
24.51
180.37/34.62 FO
24.83
69.45/21.6 CZ
25.14
32.39/21.98 JT
25.16
239.02/25.52 FO
25.19
194.47/41.96 JT
25.26
65.39/12.78 JT
25.45
199.21/31.85 FO
25.51
325.26/68.01 JT
25.75
217.94/74.69 JT
25.76
221.5/26.72 FO
26.22
202.77/27.65 FP
26.30
204.33/34.12 FP
26.35
212.1/47.06 JT
26.51
186.85/61.84 JT
26.61
253.67/21.18 FP
26.77
207.58/17.46 FP
26.84
183.41/8.44 FP
26.99
161.82/17.69 FP

100.0%
53.1%
73.6%
100.0%


27.2
27.4
27.6
27.8
28.0
28.2
28.4
28.6
28.8
29.0
29.2
29.4
29.6
29.8
30.0
30.2
30.4
30.6
30.8
27.00
144.81/58.65 JT
27.14
180.29/7.26 FP
27.21
158.91/10.87 FO
27.29
190.96/5.71 JT
27.33
204.12/22.76 FP
27.34
357.75/44.77 JT
27.40
6.07/55.15 JT
27.44
192.96/25.77 FO
27.50
19.66/34.14 JT
27.56
171.38/44.01 JT
27.57
9.22/37.11 JT
27.65
187.68/42.52 JT
27.77
165.77/8.28 JT
27.78
141.64/54.42 JT
27.86
324.06/50.38 JT
27.93
246.7/7.25 JT
27.95
1.48/50.63 JT
28.06
218.63/22.08 FP
28.18
221.26/43.08 JT
28.26
215.88/19.63 FO
28.80
11.2/72.25 JT
28.84
202.88/55.25 JT
28.95
15.96/76.23 JT
28.99
4.29/4.79 JT
29.05
200.43/35.88 FO
29.06
16.73/77.68 JT
29.24
132.6/40.56 JT
29.45
155.07/35.06 JT
29.64
56.35/39.6 V
29.70
255.46/23.97 FO
29.97
211.07/51.43 JT
30.08
223.73/29.86 FO
30.18
43.01/45.66 JT
30.24
35.37/47.79 JT
30.27
41.6/43.28 JT
30.32
247.37/27.99 FO
41.5%
91.3%
89.0%
Very Poor
Poor
Fair
Good
Excellent
1m:10m
0 deg 5
TILT
0 250
GR
0 360
70 170
Caliper-min
70 170
Caliper-max
70 170
0° 90° 180° 270° 0°
50 20000
0° 90° 180° 270° 0°
OTV-NM
0° 90° 180° 270° 0°
0 10000
180°
0 90
(True North)

Depth	AZIM (TN) 0 360	Caliper-ave 70 170	ATV Amplitude-NM	(Magn. North) Apparent Picks	Reflectivity	Pseudo Core	Corrected Picks	Pick Discription	RQD

Well Name:	MDD399
Surveys:	ATV, GR
Location:	Bendigo
Company:	Santana

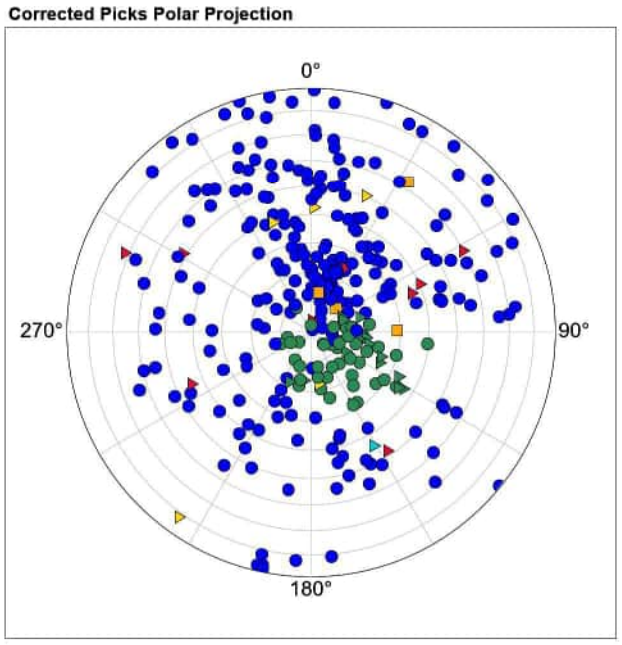
Service Company:	SPEIGHT DRILLING
Operator:	Gareth Speight
Date Logged:	18/01/2025
Drilling Company:	SPEIGHT DRILLING
Date Drilled:	
Field:	
County / Township:	
State / Province:	
Country:	

Log Measured From:	Ground Level		
Drilling Measured From:	Ground Level		
Driller Depth:	70.1	Logger Depth:	70.3
Inclination:	-57°	Heading:	029° (TN)
Easting:		Northing:	
Elevation:		Grid:	True North (22.5°)
Log Top:	1.9	Log Bottom:	70.3
Depth unit:	Meters	Scale ratio:	1 : 20

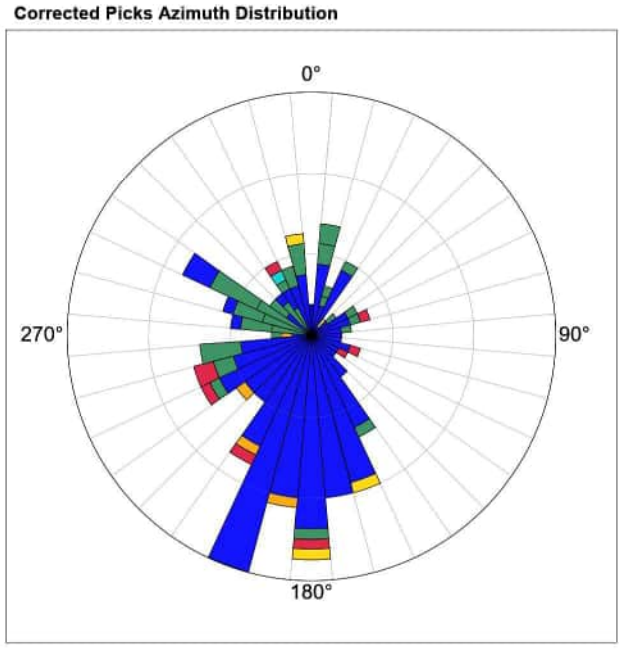
Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	33					
HQ	33	70				Wireline Length:	Depth Factor:

Remarks:
Poor borehole conditions affecting natural feature interpretation.
Corrected picks referencing to True North.

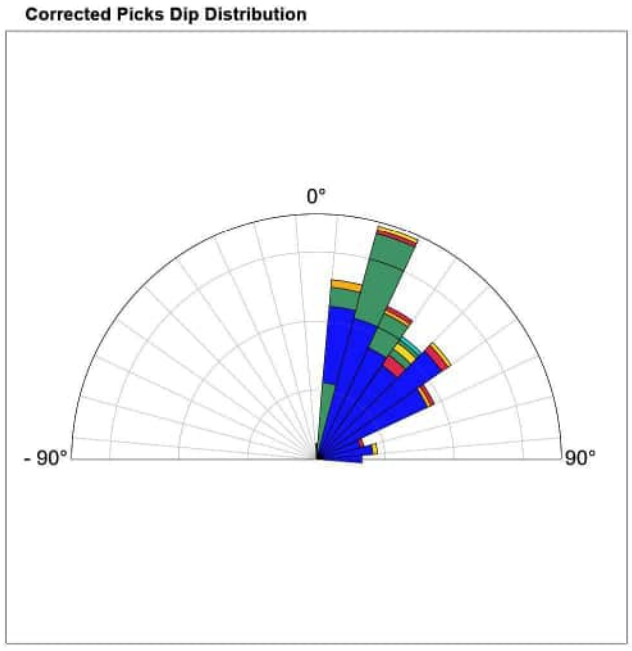
Corrected Picks Polar Projection



Corrected Picks Azimuth Distribution



Corrected Picks Dip Distribution



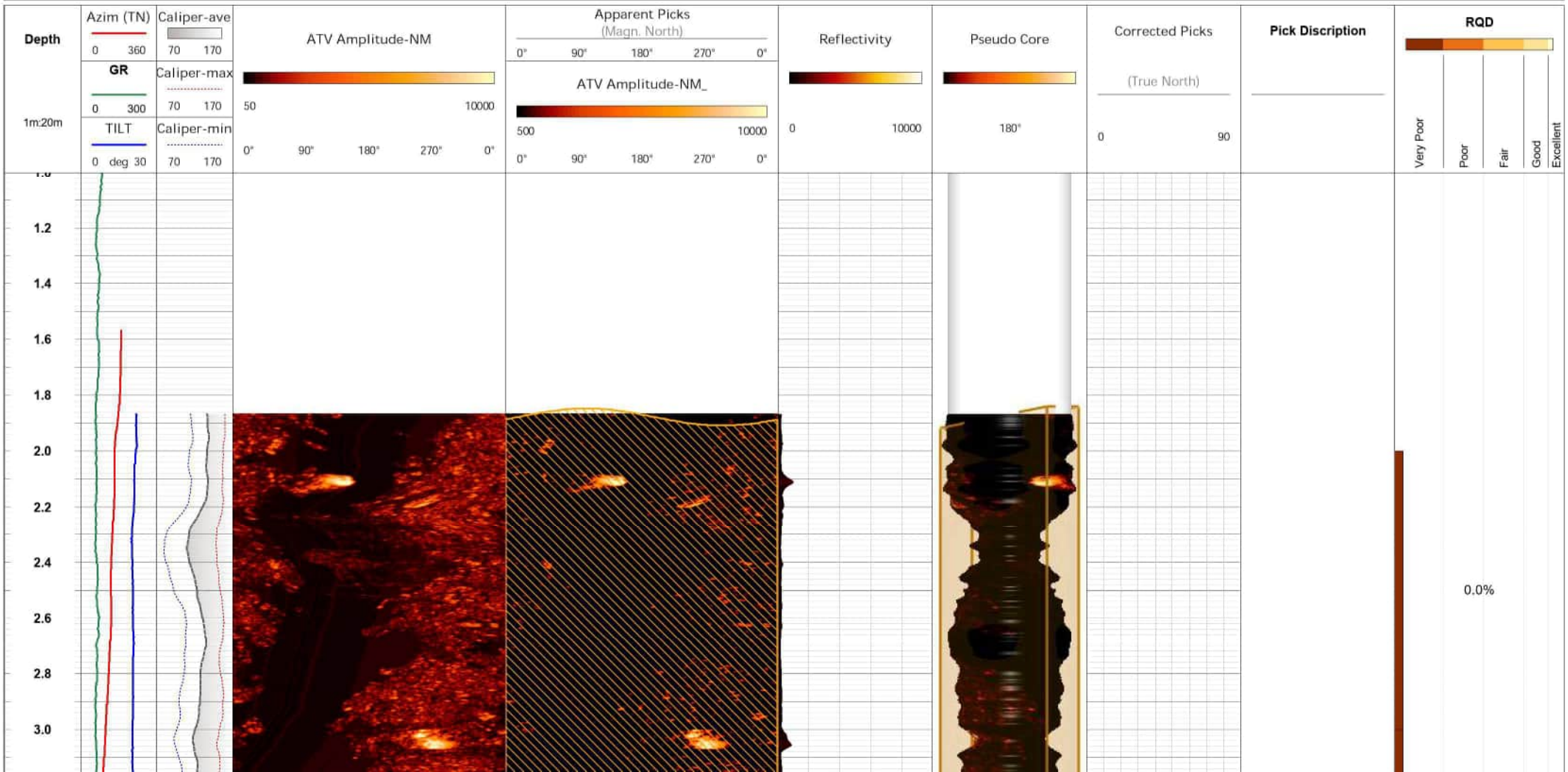
Legend:

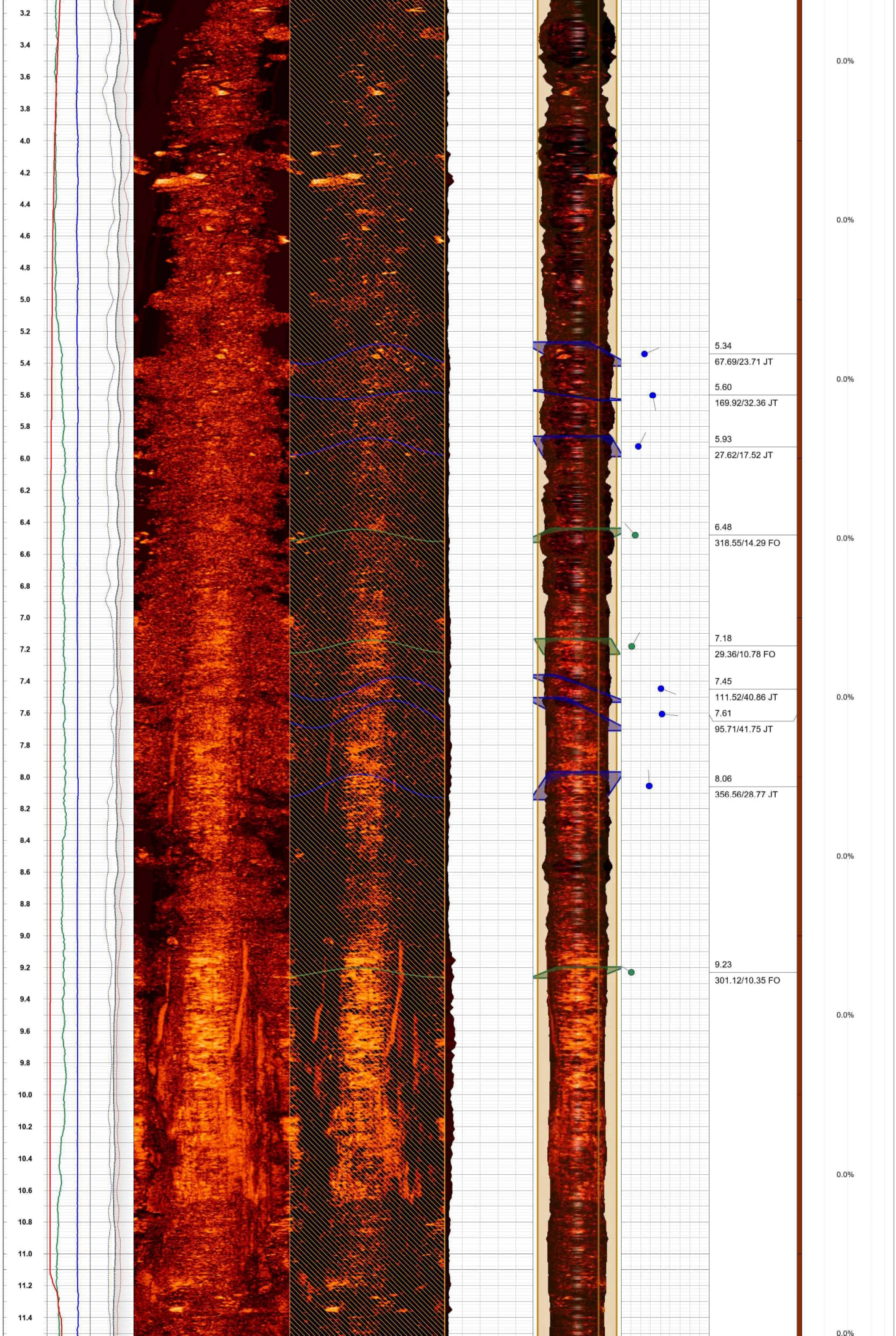
Foliation | Foliation Parting | Joint | Fracture | Shear | Crushed Zone | Vein

Curve Description:

Title	Description	Top [m]	Base [m]	Tool s/n	Run / Date
Depth	Measured depth	0.7	70.3		
TVD	True vertical depth	1.9	70.3		
Tilt	Deviation from the vertical	1.9	70.3		
Azimuth (TN)	Deviation from True North	1.9	70.3		
GR	Natural gamma ray	0.7	69.2	ABI/GR 2204023	18/01/2025
Caliper	Borehole diameter from ATV traveltime	1.9	70.3		
Apparent Picks	Uncorrected structure picks from ATV and OTV images	1.9	70.3		
ATV	ATV amplitude image	1.9	70.3	ABI/GR 220402	18/01/2025
OTV	OTV image	-	-		
Reflectivity	Acoustic reflectivity of the rock	1.9	70.3		
Corr. Picks	Structure picks correxcted for borehole deviation (oriented to True North)	1.9	70.3		
Picks Stats	Stereonet of observed defects, features per 5m interval	1.9	70.3		
Pseudo Core	3D poresentation of ATV amplitude, borehole radius and apparent picks	1.9	70.3		

Disclaimer:




3.2
3.4
3.6
3.8
4.0
4.2
4.4
4.6
4.8
5.0
5.2
5.4
5.6
5.8
6.0
6.2
6.4
6.6
6.8
7.0
7.2
7.4
7.6
7.8
8.0
8.2
8.4
8.6
8.8
9.0
9.2
9.4
9.6
9.8
10.0
10.2
10.4
10.6
10.8
11.0
11.2
11.4
5.34
67.69/23.71 JT
5.60
169.92/32.36 JT
5.93
27.62/17.52 JT
6.48
318.55/14.29 FO
7.18
29.36/10.78 FO
7.45
111.52/40.86 JT
7.61
95.71/41.75 JT
8.06
356.56/28.77 JT
9.23
301.12/10.35 FO
0.0%
0.0%
0.0%
0.0%
0.0%
0.0%
0.0%

11.6
11.8
12.0
12.2
12.4
12.6
12.8
13.0
13.2
13.4
13.6
13.8
14.0
14.2
14.4
14.6
14.8
15.0
15.2
15.4
15.6
15.8
16.0
16.2
16.4
16.6
16.8
17.0
17.2
17.4
17.6
17.8
18.0
18.2
18.4
18.6
18.8
19.0
19.2
19.4
19.6
19.8

11.95
51.47/5.39 FO
12.30
12.69/82.26 JT
12.64
163.84/82.9 JT
12.69
313.8/49.72 JT
13.36
49.04/41.19 JT
14.72
203.54/17.35 JT
15.37
94.8/15.67 JT
17.18
201.27/18.14 JT
17.81
268.78/28.96 CZ
18.88
326.66/28.39 FO

0.0%
0.0%
0.0%
0.0%
0.0%
0.0%
0.0%
0.0%

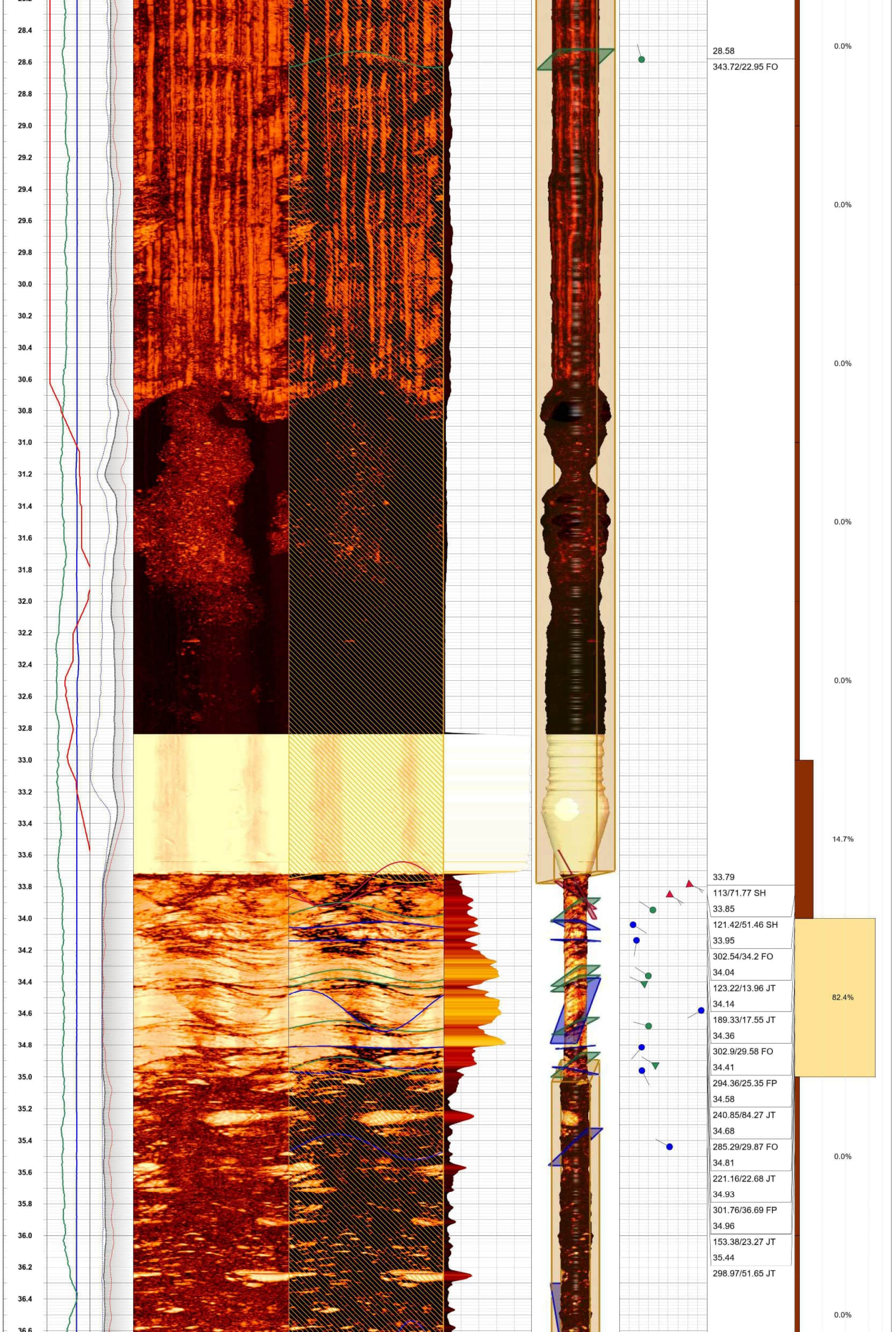
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20.2
20.4
20.6
20.8
21.0
21.2
21.4
21.6
21.8
22.0
22.2
22.4
22.6
22.8
23.0
23.2
23.4
23.6
23.8
24.0
24.2
24.4
24.6
24.8
25.0
25.2
25.4
25.6
25.8
26.0
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26.6
26.8
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27.2
27.4
27.6
27.8
28.0
28.2

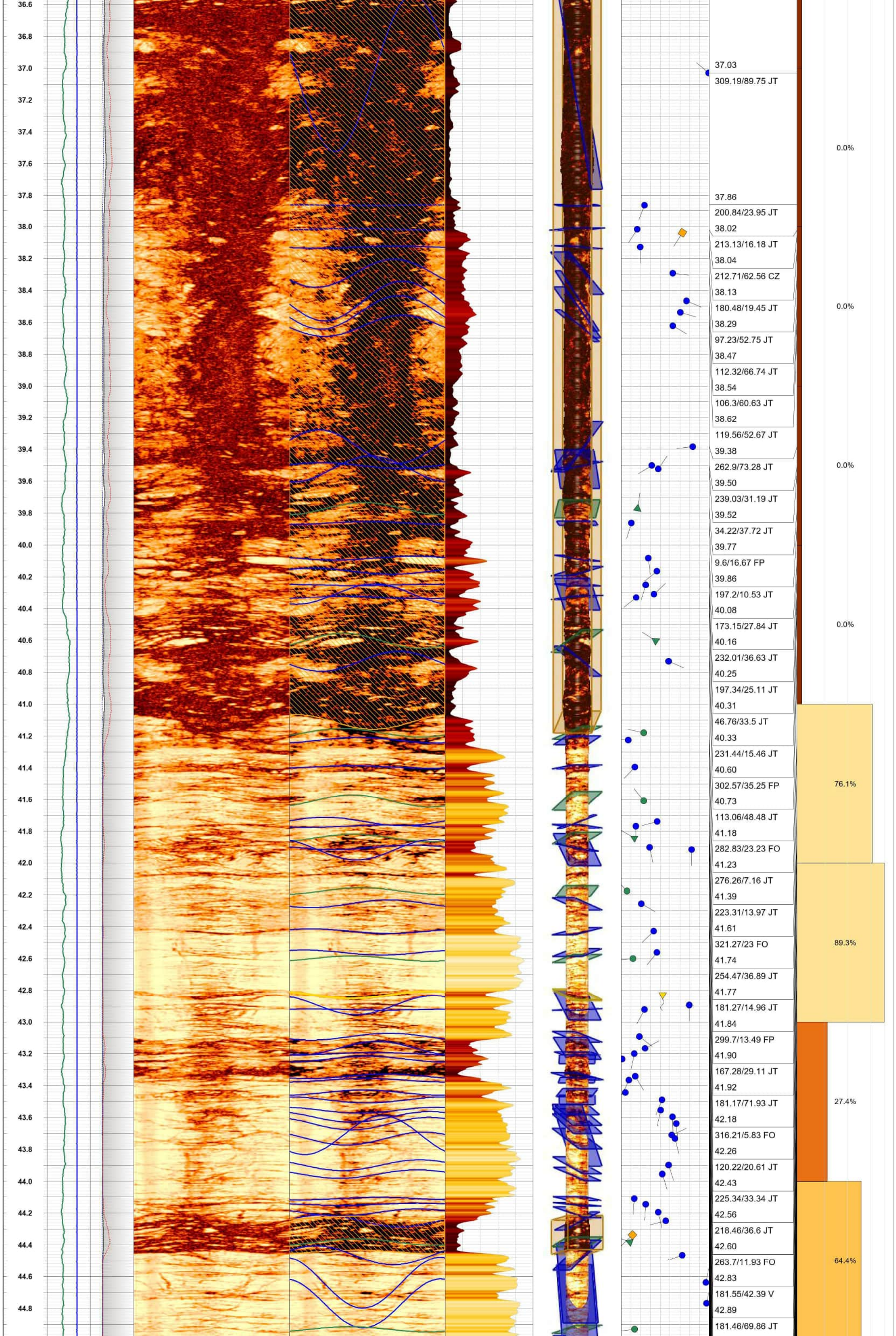
20.25
349.47/19.28 FO

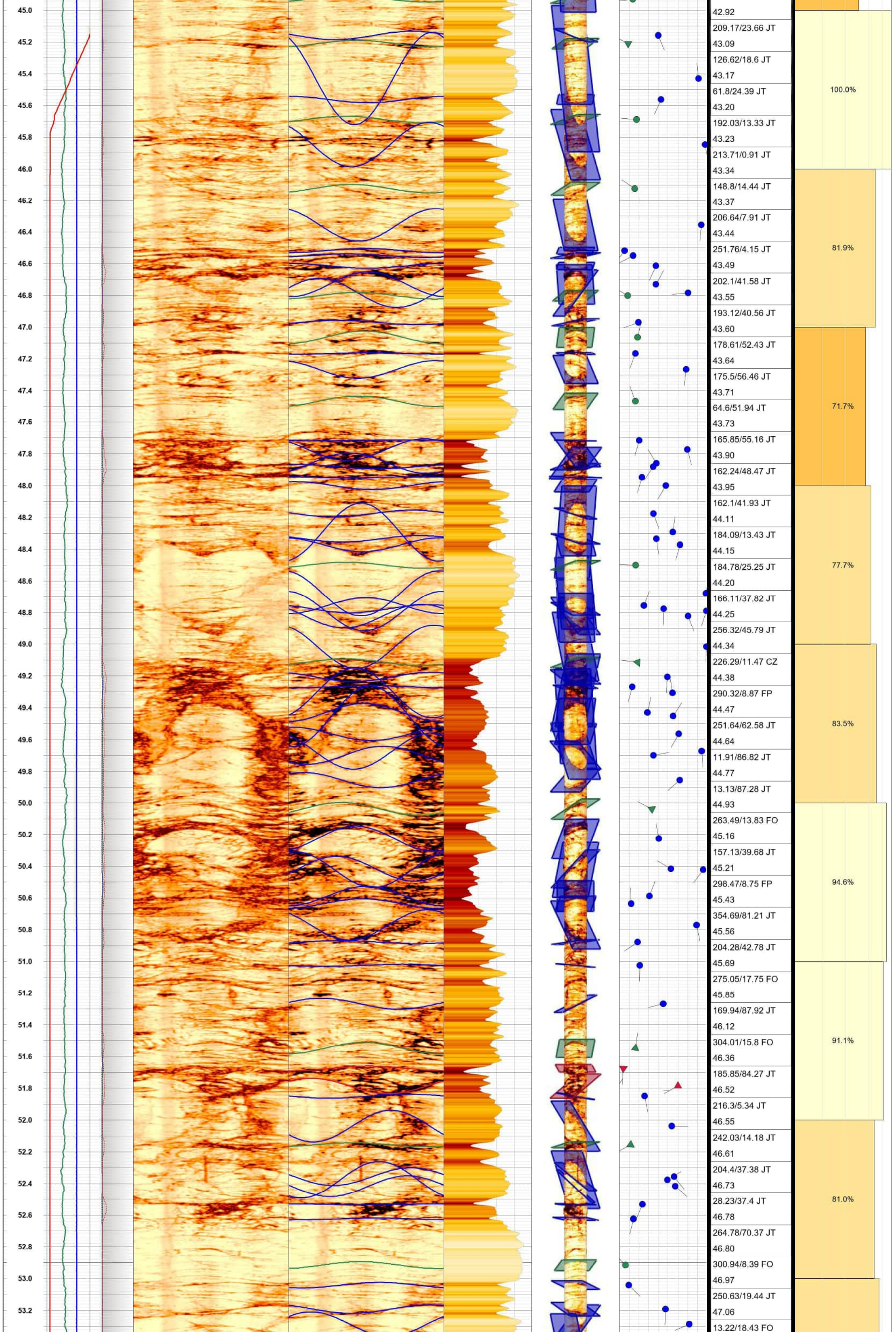
22.92
276.07/39.9 FO
23.10
308.61/27.95 FO
23.37
316.38/19.9 FO
24.54
302.04/19.07 FO

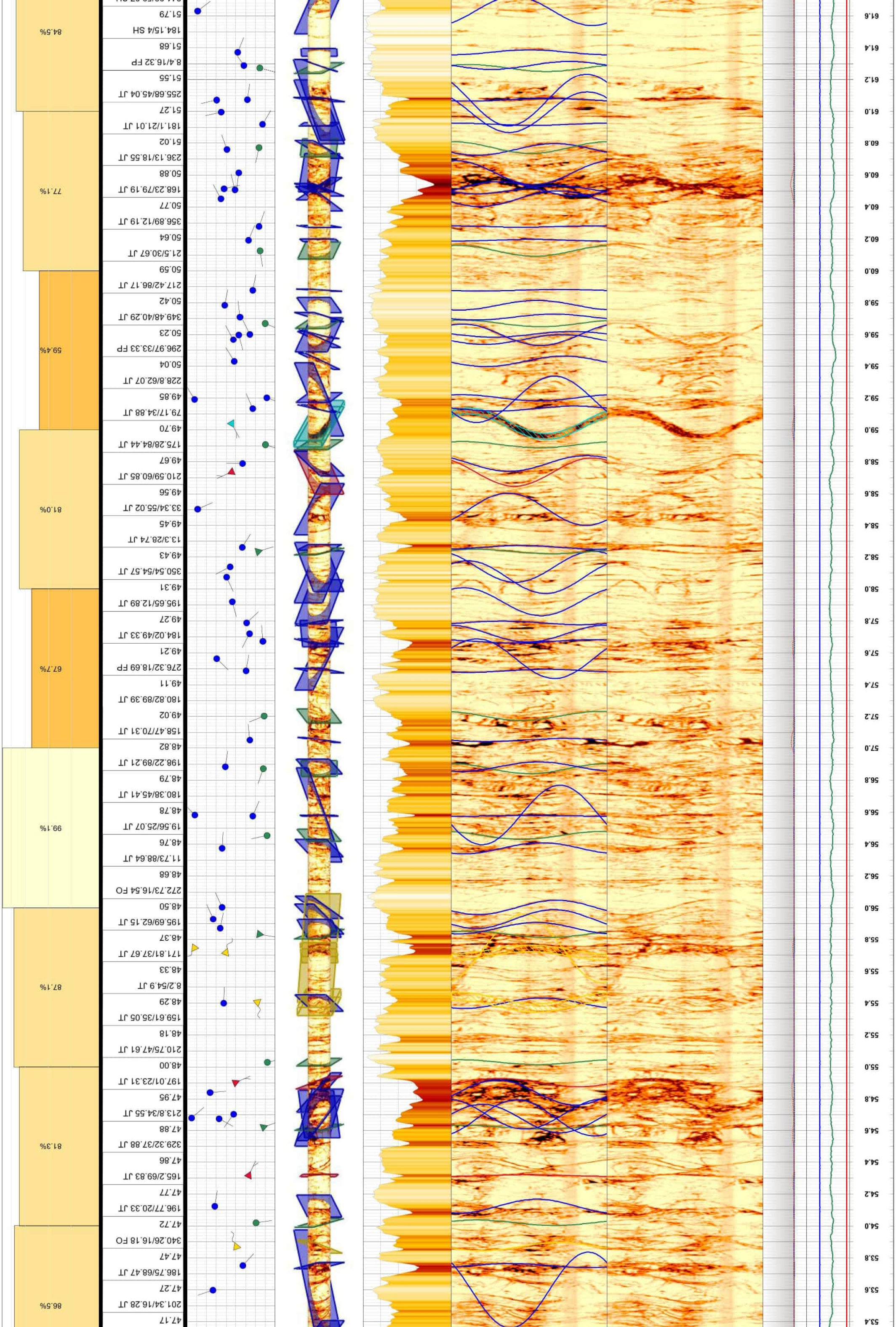
26.73
202.56/16.41 JT

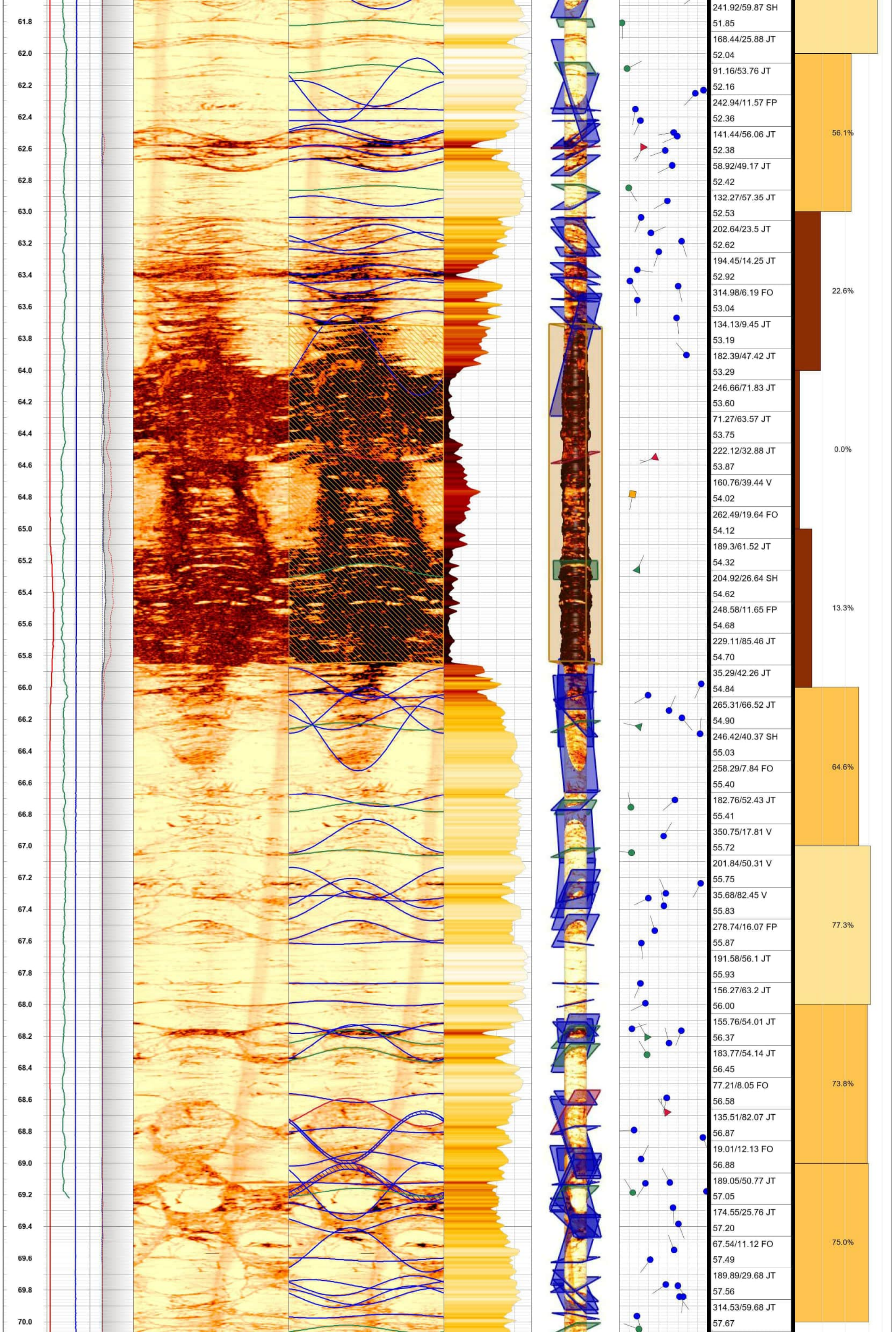
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0.0%

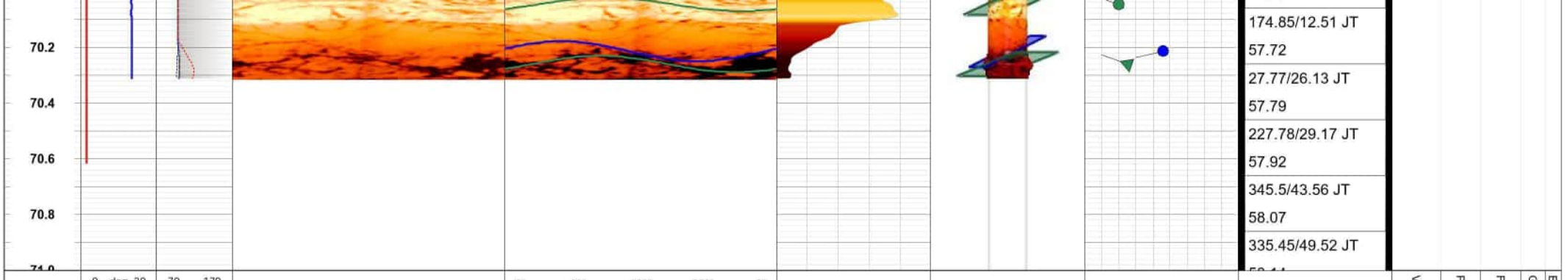

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28.8
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29.2
29.4
29.6
29.8
30.0
30.2
30.4
30.6
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31.0
31.2
31.4
31.6
31.8
32.0
32.2
32.4
32.6
32.8
33.0
33.2
33.4
33.6
33.8
34.0
34.2
34.4
34.6
34.8
35.0
35.2
35.4
35.6
35.8
36.0
36.2
36.4
36.6
28.58
343.72/22.95 FO
33.79
113/71.77 SH
33.85
121.42/51.46 SH
33.95
302.54/34.2 FO
34.04
123.22/13.96 JT
34.14
189.33/17.55 JT
34.36
302.9/29.58 FO
34.41
294.36/25.35 FP
34.58
240.85/84.27 JT
34.68
285.29/29.87 FO
34.81
221.16/22.68 JT
34.93
301.76/36.69 FP
34.96
153.38/23.27 JT
35.44
298.97/51.65 JT
0.0%
0.0%
0.0%
0.0%
14.7%
82.4%
0.0%
0.0%


36.6
36.8
37.0
37.2
37.4
37.6
37.8
38.0
38.2
38.4
38.6
38.8
39.0
39.2
39.4
39.6
39.8
40.0
40.2
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40.6
40.8
41.0
41.2
41.4
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41.8
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42.2
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42.6
42.8
43.0
43.2
43.4
43.6
43.8
44.0
44.2
44.4
44.6
44.8
37.03
309.19/89.75 JT
37.86
200.84/23.95 JT
38.02
213.13/16.18 JT
38.04
212.71/62.56 CZ
38.13
180.48/19.45 JT
38.29
97.23/52.75 JT
38.47
112.32/66.74 JT
38.54
106.3/60.63 JT
38.62
119.56/52.67 JT
39.38
262.9/73.28 JT
39.50
239.03/31.19 JT
39.52
34.22/37.72 JT
39.77
9.6/16.67 FP
39.86
197.2/10.53 JT
40.08
173.15/27.84 JT
40.16
232.01/36.63 JT
40.25
197.34/25.11 JT
40.31
46.76/33.5 JT
40.33
231.44/15.46 JT
40.60
302.57/35.25 FP
40.73
113.06/48.48 JT
41.18
282.83/23.23 FO
41.23
276.26/7.16 JT
41.39
223.31/13.97 JT
41.61
321.27/23 FO
41.74
254.47/36.89 JT
41.77
181.27/14.96 JT
41.84
299.7/13.49 FP
41.90
167.28/29.11 JT
41.92
181.17/71.93 JT
42.18
316.21/5.83 FO
42.26
120.22/20.61 JT
42.43
225.34/33.34 JT
42.56
218.46/36.6 JT
42.60
263.7/11.93 FO
42.83
181.55/42.39 V
42.89
181.46/69.86 JT
0.0%
0.0%
0.0%
0.0%
76.1%
89.3%
27.4%
64.4%


45.0
45.2
45.4
45.6
45.8
46.0
46.2
46.4
46.6
46.8
47.0
47.2
47.4
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48.0
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48.8
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50.8
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51.2
51.4
51.6
51.8
52.0
52.2
52.4
52.6
52.8
53.0
53.2
42.92
209.17/23.66 JT
43.09
126.62/18.6 JT
43.17
61.8/24.39 JT
43.20
192.03/13.33 JT
43.23
213.71/0.91 JT
43.34
148.8/14.44 JT
43.37
206.64/7.91 JT
43.44
251.76/4.15 JT
43.49
202.1/41.58 JT
43.55
193.12/40.56 JT
43.60
178.61/52.43 JT
43.64
175.5/56.46 JT
43.71
64.6/51.94 JT
43.73
165.85/55.16 JT
43.90
162.24/48.47 JT
43.95
162.1/41.93 JT
44.11
184.09/13.43 JT
44.15
184.78/25.25 JT
44.20
166.11/37.82 JT
44.25
256.32/45.79 JT
44.34
226.29/11.47 CZ
44.38
290.32/8.87 FP
44.47
251.64/62.58 JT
44.64
11.91/86.82 JT
44.77
13.13/87.28 JT
44.93
263.49/13.83 FO
45.16
157.13/39.68 JT
45.21
298.47/8.75 FP
45.43
354.69/81.21 JT
45.56
204.28/42.78 JT
45.69
275.05/17.75 FO
45.85
169.94/87.92 JT
46.12
304.01/15.8 FO
46.36
185.85/84.27 JT
46.52
216.3/5.34 JT
46.55
242.03/14.18 JT
46.61
204.4/37.38 JT
46.73
28.23/37.4 JT
46.78
264.78/70.37 JT
46.80
300.94/8.39 FO
46.97
250.63/19.44 JT
47.06
13.22/18.43 FO
100.0%
81.9%
71.7%
77.7%
83.5%
94.6%
91.1%
81.0%


84.5%
77.1%
59.4%
81.0%
67.7%
99.1%
87.1%
81.3%
86.5%
61.6
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61.0
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60.0
59.8
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57.4
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56.2
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55.8
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55.4
55.2
55.0
54.8
54.6
54.4
54.2
54.0
53.8
53.6
53.4
51.79
184.15/4 SH
51.68
8.4/16.32 FP
51.55
255.68/45.04 JT
51.27
181.1/21.01 JT
51.02
236.13/18.55 JT
50.88
168.23/79.19 JT
50.77
356.89/12.19 JT
50.64
21.5/30.67 JT
50.59
217.42/86.17 JT
50.42
349.48/40.29 JT
50.23
296.97/33.33 FP
50.04
228.8/62.07 JT
49.85
79.17/34.88 JT
49.70
175.28/84.44 JT
49.67
210.59/60.85 JT
49.56
33.34/55.02 JT
49.45
13.3/28.74 JT
49.43
350.54/54.57 JT
49.31
195.65/12.89 JT
49.27
184.02/49.33 JT
49.21
276.32/18.69 FP
49.11
180.82/89.39 JT
49.02
158.47/70.31 JT
48.82
198.22/89.21 JT
48.79
180.38/45.41 JT
48.78
19.56/25.07 JT
48.76
11.73/88.64 JT
48.68
272.73/16.54 FO
48.50
195.69/62.15 JT
48.37
171.81/37.67 JT
48.33
8.2/54.9 JT
48.29
159.61/35.05 JT
48.18
210.75/47.61 JT
48.00
197.01/23.31 JT
47.95
213.8/34.55 JT
47.88
329.32/37.88 JT
47.86
165.2/69.83 JT
47.77
196.77/20.33 JT
47.72
340.26/16.18 FO
47.47
186.75/68.47 JT
47.27
201.34/16.28 JT
47.17
13.22/18.43 FO


61.8
62.0
62.2
62.4
62.6
62.8
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66.8
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67.2
67.4
67.6
67.8
68.0
68.2
68.4
68.6
68.8
69.0
69.2
69.4
69.6
69.8
70.0
241.92/59.87 SH
51.85
168.44/25.88 JT
52.04
91.16/53.76 JT
52.16
242.94/11.57 FP
52.36
141.44/56.06 JT
52.38
58.92/49.17 JT
52.42
132.27/57.35 JT
52.53
202.64/23.5 JT
52.62
194.45/14.25 JT
52.92
314.98/6.19 FO
53.04
134.13/9.45 JT
53.19
182.39/47.42 JT
53.29
246.66/71.83 JT
53.60
71.27/63.57 JT
53.75
222.12/32.88 JT
53.87
160.76/39.44 V
54.02
262.49/19.64 FO
54.12
189.3/61.52 JT
54.32
204.92/26.64 SH
54.62
248.58/11.65 FP
54.68
229.11/85.46 JT
54.70
35.29/42.26 JT
54.84
265.31/66.52 JT
54.90
246.42/40.37 SH
55.03
258.29/7.84 FO
55.40
182.76/52.43 JT
55.41
350.75/17.81 V
55.72
201.84/50.31 V
55.75
35.68/82.45 V
55.83
278.74/16.07 FP
55.87
191.58/56.1 JT
55.93
156.27/63.2 JT
56.00
155.76/54.01 JT
56.37
183.77/54.14 JT
56.45
77.21/8.05 FO
56.58
135.51/82.07 JT
56.87
19.01/12.13 FO
56.88
189.05/50.77 JT
57.05
174.55/25.76 JT
57.20
67.54/11.12 FO
57.49
189.89/29.68 JT
57.56
314.53/59.68 JT
57.67
56.1%
22.6%
0.0%
13.3%
64.6%
77.3%
73.8%
75.0%



Depth	1m:20m	0 deg 30 TILT	0 300 GR	0 360 Azim (TN)	70 170 Caliper-min	70 170 Caliper-max	70 170 Caliper-ave	0° 90° 180° 270° 0° 50 10000 ATV Amplitude-NM	0° 90° 180° 270° 0° 500 10000 ATV Amplitude-NM_ 0° 90° 180° 270° 0° (Magn. North) Apparent Picks	0 10000 Reflectivity	180° Pseudo Core	0 90 (True North) Corrected Picks	Pick Discription	Very Poor Poor Fair Good Excellent RQD

Well Name:	MDD491
Surveys:	ATV, OPTV, GR
Location:	Bendigo
Company:	Santana

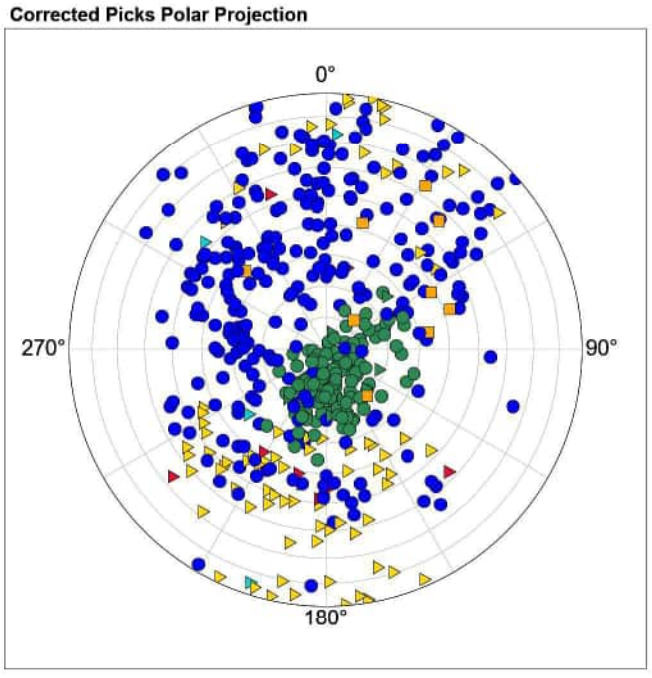
Service Company:	SPEIGHT DRILLING
Operator:	Gareth Speight
Date Logged:	1/04/2025
Drilling Company:	SPEIGHT DRILLING
Date Drilled:	
Field:	
County / Township:	
State / Province:	
Country:	

Log Measured From:	Ground Level		
Drilling Measured From:	Ground Level		
Driller Depth:	100	**Logger Depth:**	99
Inclination:	-71°	**Heading:**	360° (TN)
Easting:		**Northing:**	
Elevation:		**Grid:**	True North (22.5°)
Log Top:	4	**Log Bottom:**	99
Depth unit:	Meters	**Scale ratio:**	1 : 20

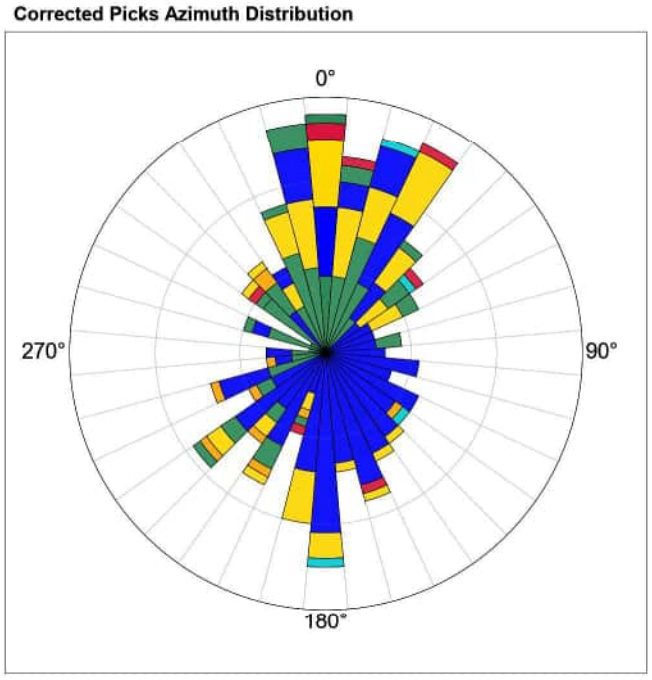
Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	60					
HQ	60	100				Wireline Length:	Depth Factor:

Remarks:
Corrected Picks referencing to True North.

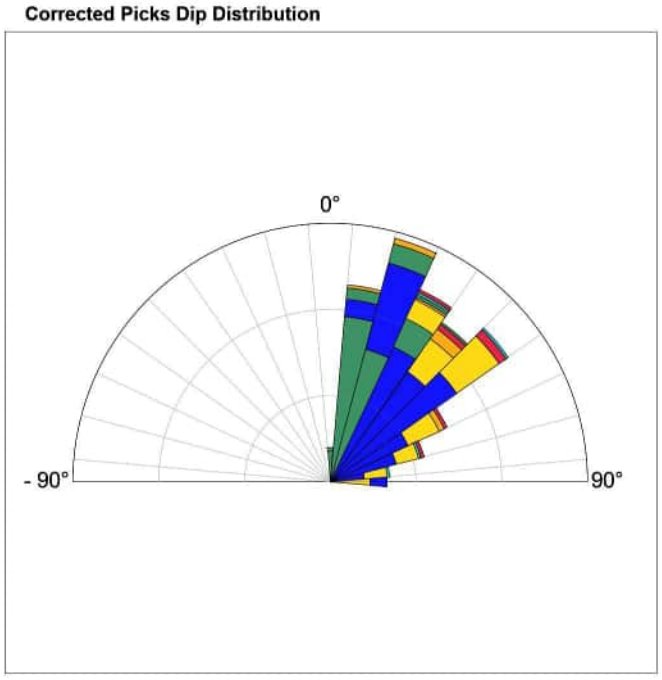
Corrected Picks Polar Projection



Corrected Picks Azimuth Distribution



Corrected Picks Dip Distribution

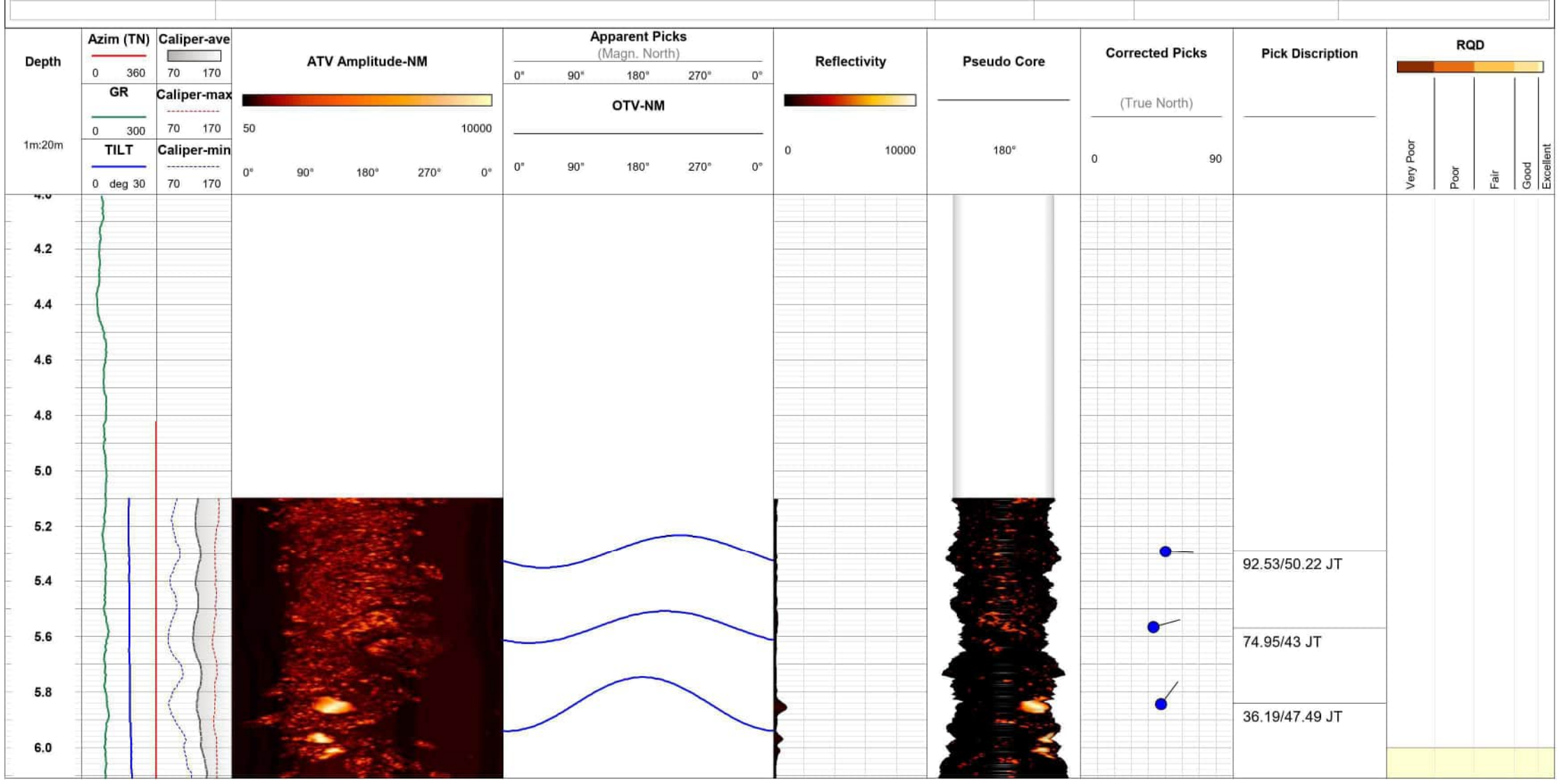


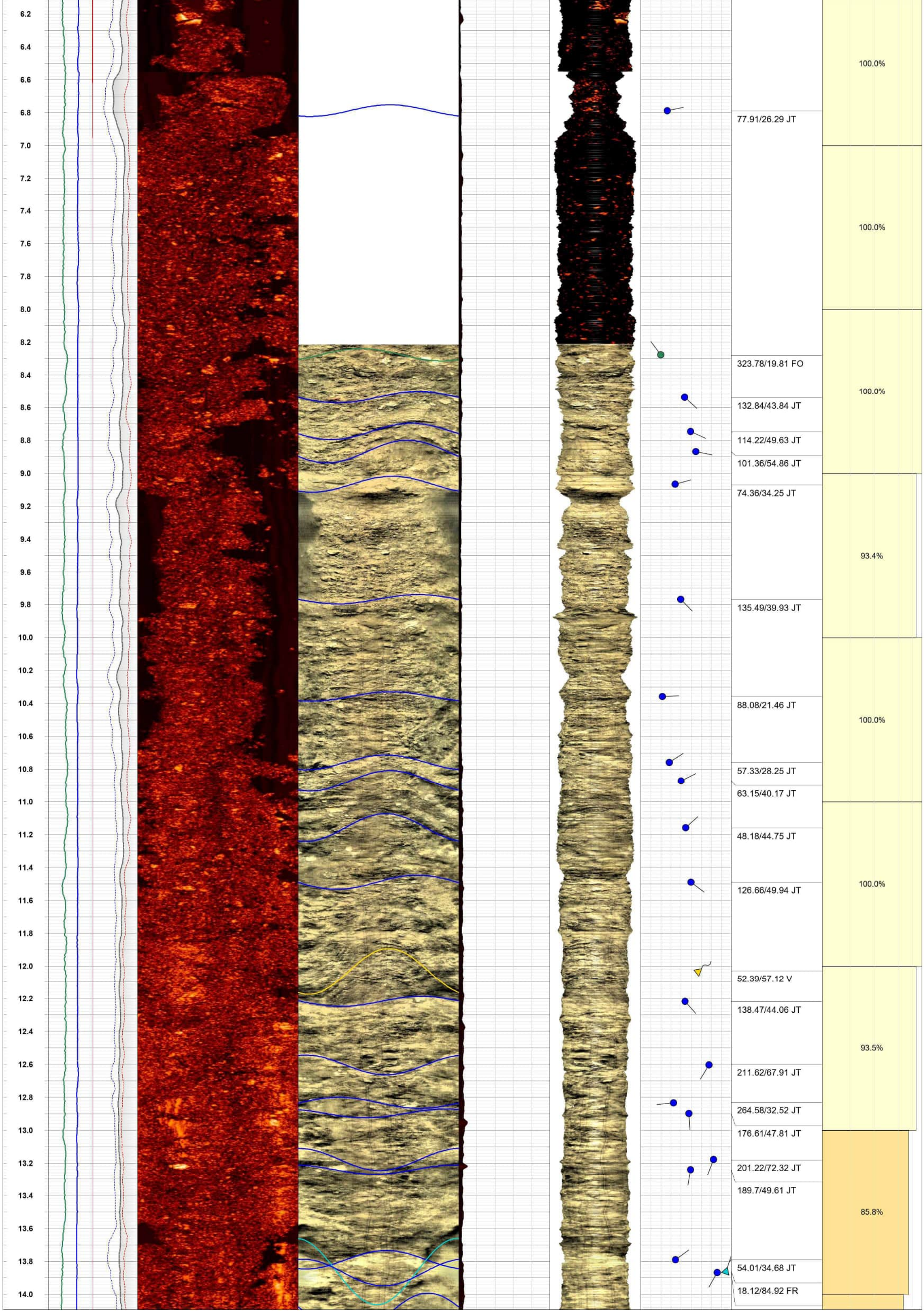
Legend:

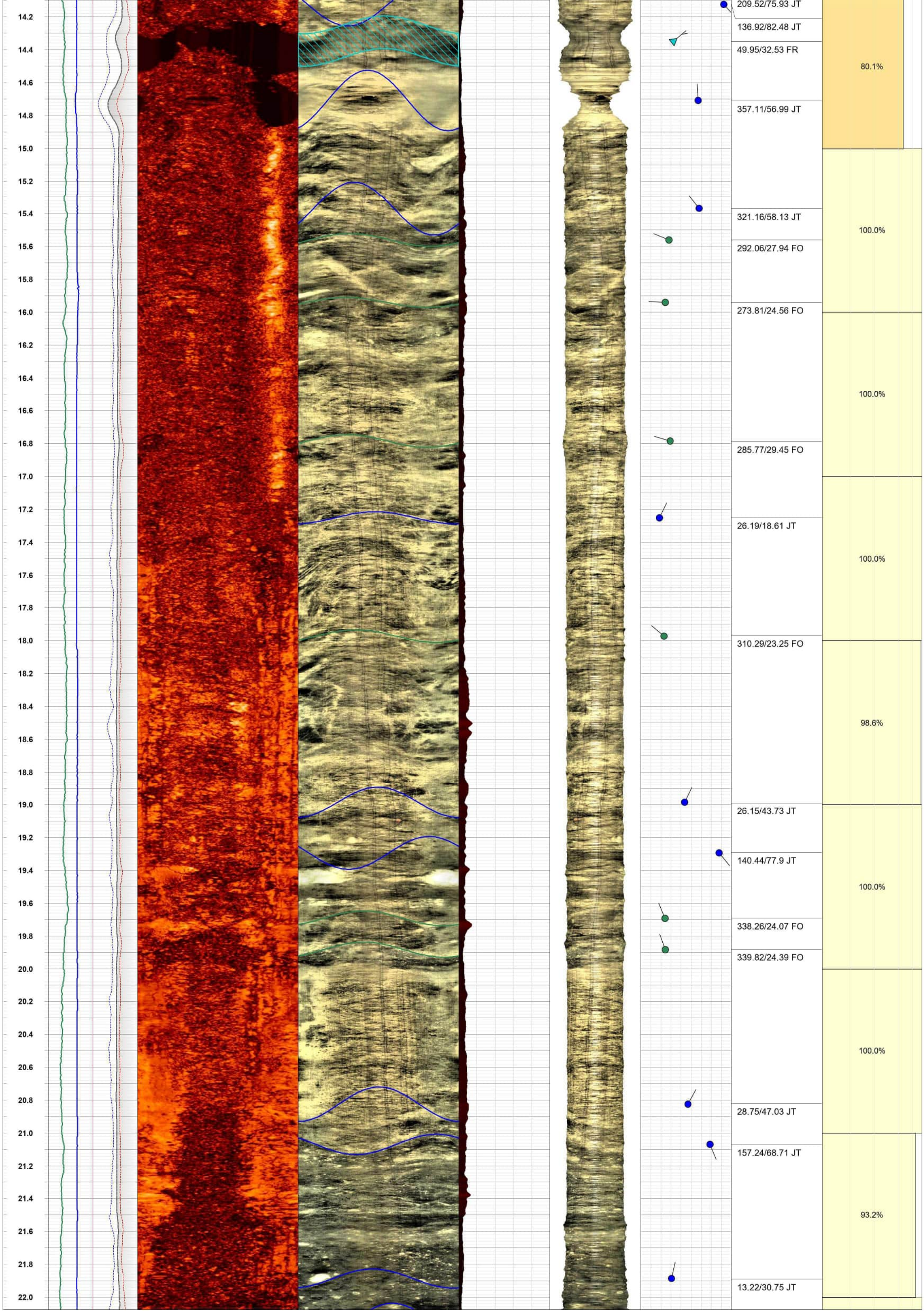


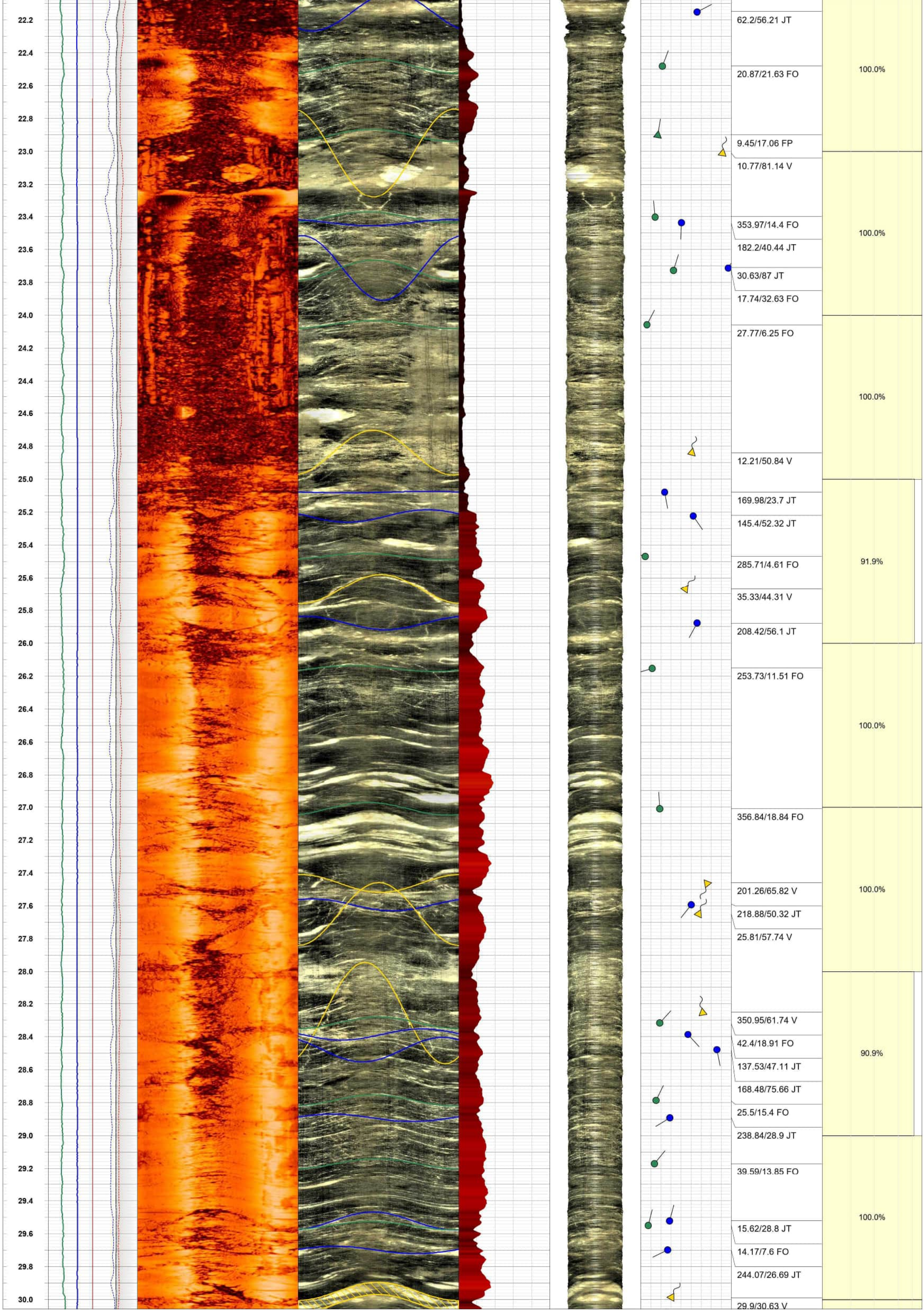
Curve Description:

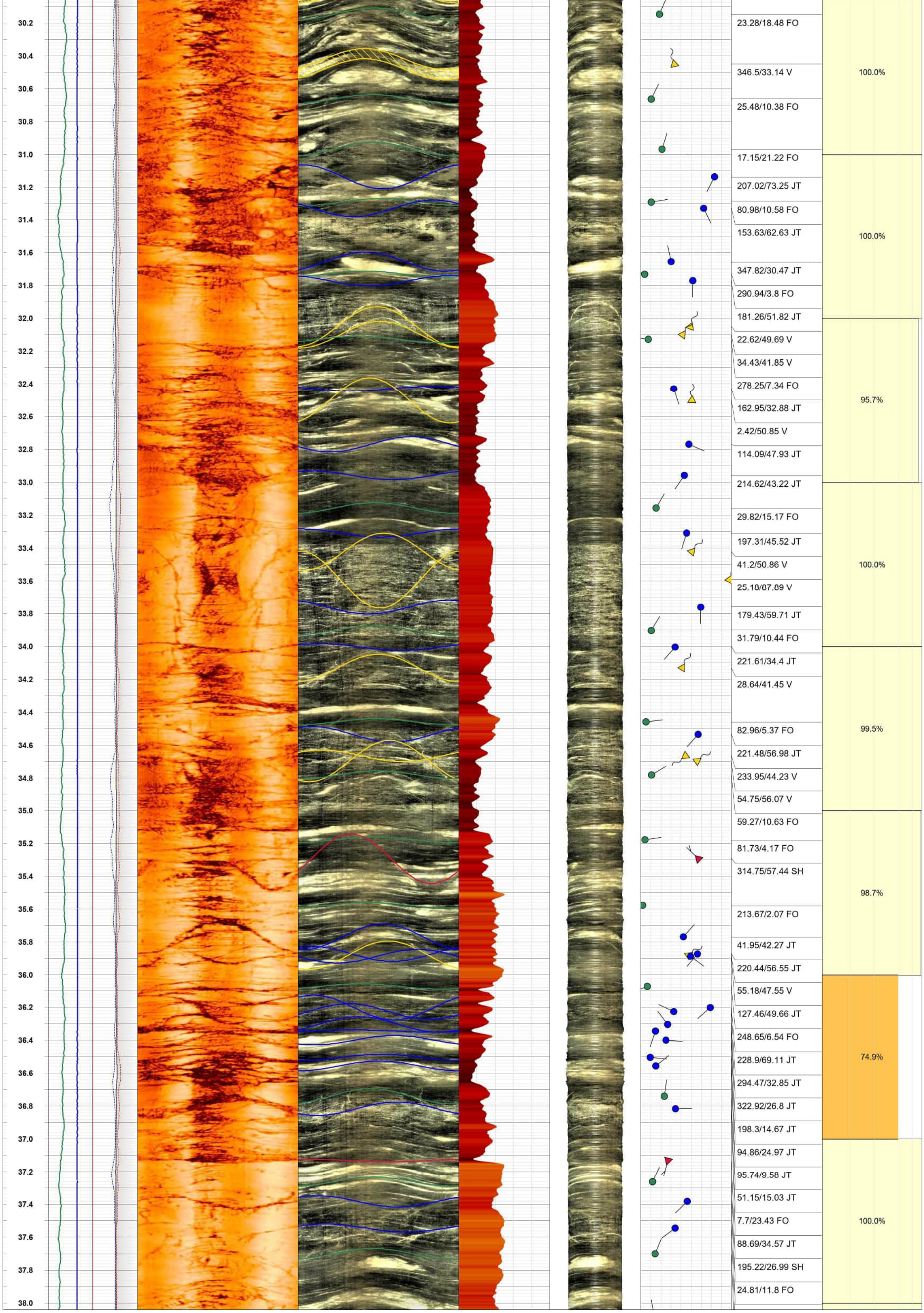
Title	Description	Top [m]	Base [m]	Tool s/n	Run / Date
Depth	Measured depth	5.1	99		
TVD	True vertical depth	5.1	99		
Tilt	Deviation from the vertical	5.1	99		
Azimuth (TN)	Deviation from True North	5.1	99		
GR	Natural gamma ray	5.1	98	ABI/GR 2204023	1/04/2025
Caliper	Borehole diameter from ATV traveltime	5.1	99		
Apparent Picks	Uncorrected structure picks from ATV and OTV images	5.1	99		
ATV	ATV amplitude image	5.1	99	ABI/GR 220402	1/04/2025
OTV	OTV image	8.2	98.7	OBI 222204	1/04/2025
Reflectivity	Acoustic reflectivity of the rock	5.1	99		
Corr. Picks	Structure picks correxcted for borehole deviation (oriented to True North)	5.1	99		
RQD	Rock Quality Designation	6	99		
Pseudo Core	3D poresentation of ATV amplitude, borehole radius and apparent picks	5.1	99		

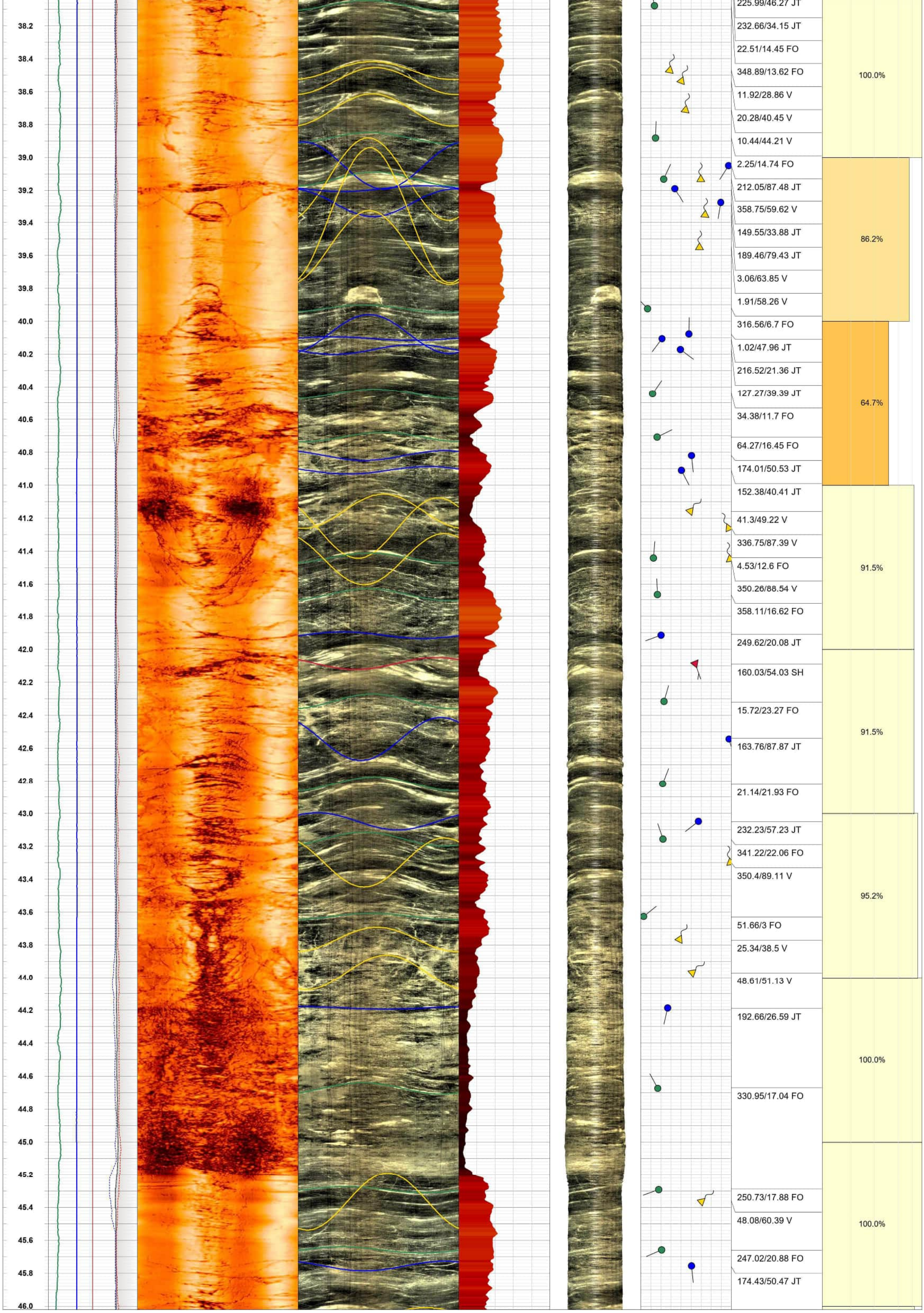


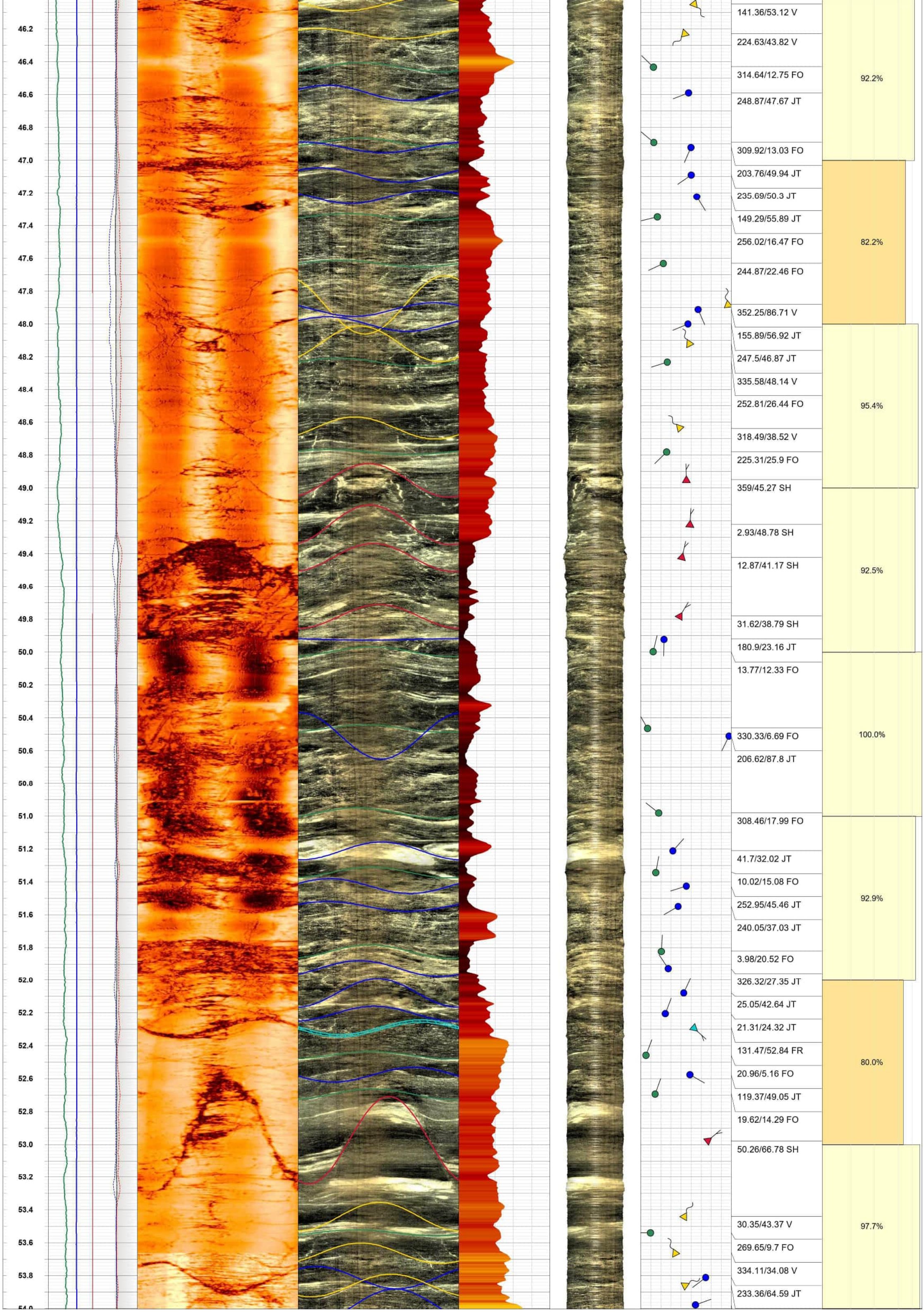

6.2
6.4
6.6
6.8
7.0
7.2
7.4
7.6
7.8
8.0
8.2
8.4
8.6
8.8
9.0
9.2
9.4
9.6
9.8
10.0
10.2
10.4
10.6
10.8
11.0
11.2
11.4
11.6
11.8
12.0
12.2
12.4
12.6
12.8
13.0
13.2
13.4
13.6
13.8
14.0
77.91/26.29 JT
323.78/19.81 FO
132.84/43.84 JT
114.22/49.63 JT
101.36/54.86 JT
74.36/34.25 JT
135.49/39.93 JT
88.08/21.46 JT
57.33/28.25 JT
63.15/40.17 JT
48.18/44.75 JT
126.66/49.94 JT
52.39/57.12 V
138.47/44.06 JT
211.62/67.91 JT
264.58/32.52 JT
176.61/47.81 JT
201.22/72.32 JT
189.7/49.61 JT
54.01/34.68 JT
18.12/84.92 FR
100.0%
100.0%
100.0%
93.4%
100.0%
100.0%
93.5%
85.8%

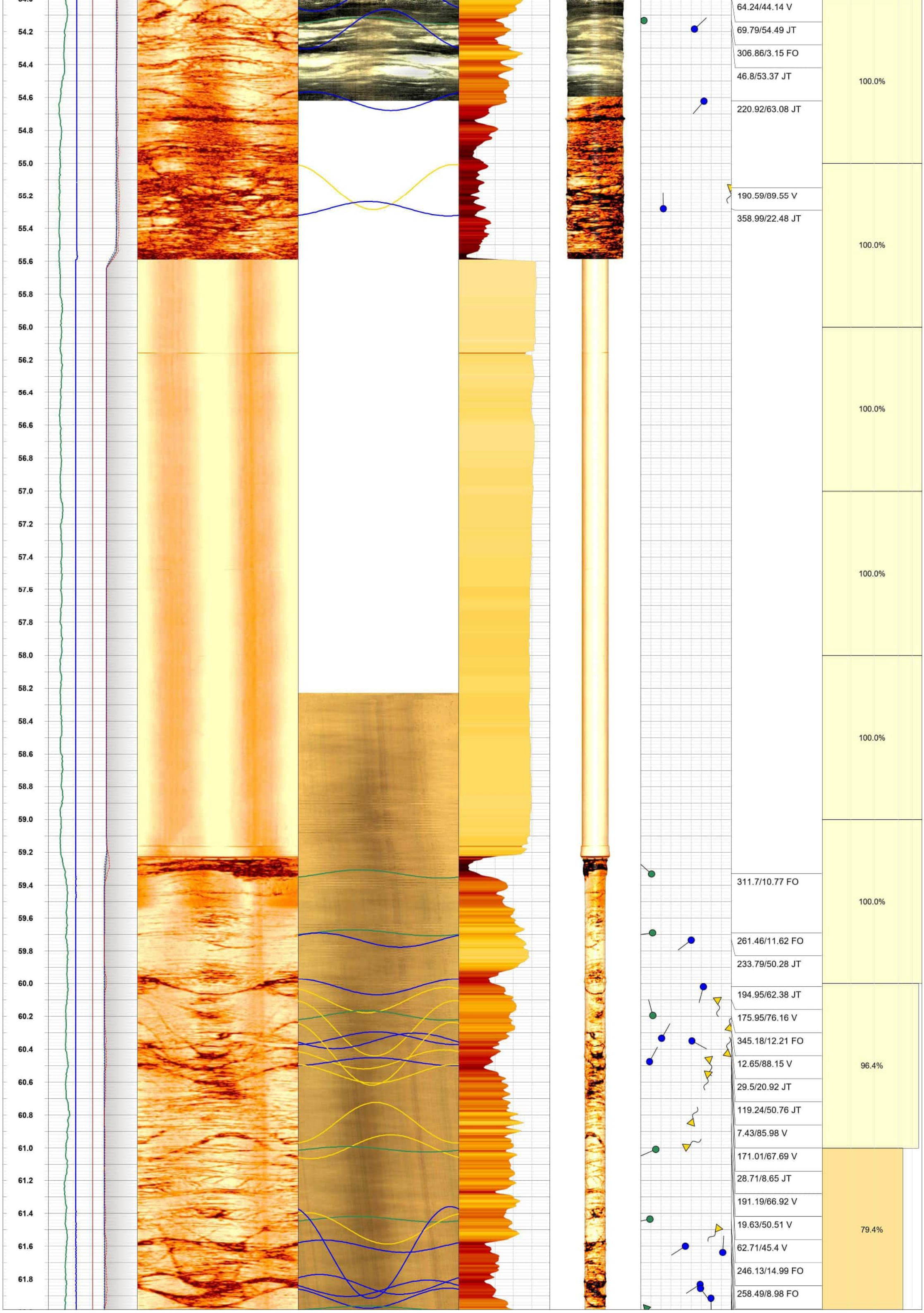

14.2
14.4
14.6
14.8
15.0
15.2
15.4
15.6
15.8
16.0
16.2
16.4
16.6
16.8
17.0
17.2
17.4
17.6
17.8
18.0
18.2
18.4
18.6
18.8
19.0
19.2
19.4
19.6
19.8
20.0
20.2
20.4
20.6
20.8
21.0
21.2
21.4
21.6
21.8
22.0
209.52/75.93 JT
136.92/82.48 JT
49.95/32.53 FR
357.11/56.99 JT
321.16/58.13 JT
292.06/27.94 FO
273.81/24.56 FO
285.77/29.45 FO
26.19/18.61 JT
310.29/23.25 FO
26.15/43.73 JT
140.44/77.9 JT
338.26/24.07 FO
339.82/24.39 FO
28.75/47.03 JT
157.24/68.71 JT
13.22/30.75 JT
80.1%
100.0%
100.0%
100.0%
98.6%
100.0%
93.2%

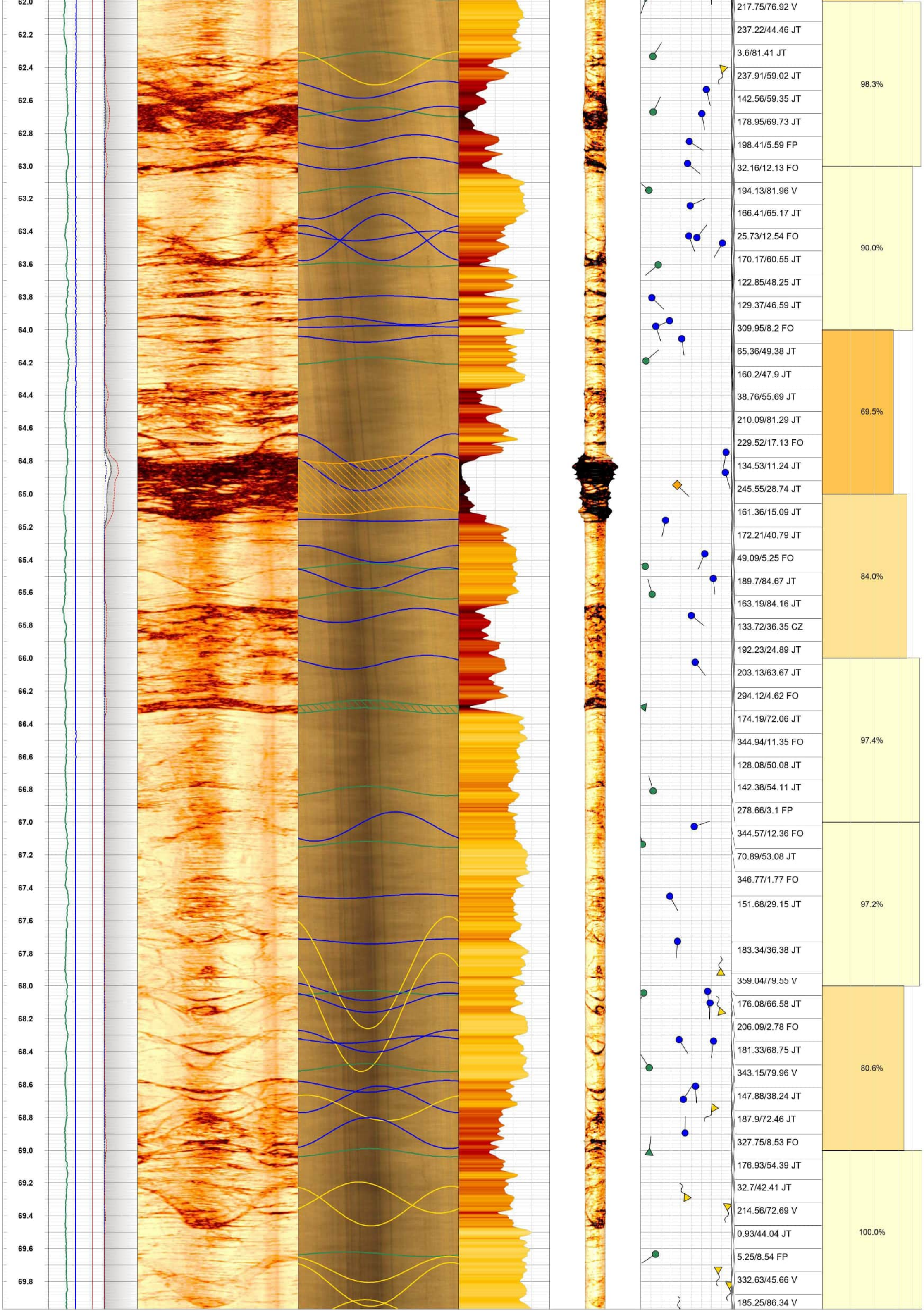

22.2
22.4
22.6
22.8
23.0
23.2
23.4
23.6
23.8
24.0
24.2
24.4
24.6
24.8
25.0
25.2
25.4
25.6
25.8
26.0
26.2
26.4
26.6
26.8
27.0
27.2
27.4
27.6
27.8
28.0
28.2
28.4
28.6
28.8
29.0
29.2
29.4
29.6
29.8
30.0
62.2/56.21 JT
20.87/21.63 FO
9.45/17.06 FP
10.77/81.14 V
353.97/14.4 FO
182.2/40.44 JT
30.63/87 JT
17.74/32.63 FO
27.77/6.25 FO
12.21/50.84 V
169.98/23.7 JT
145.4/52.32 JT
285.71/4.61 FO
35.33/44.31 V
208.42/56.1 JT
253.73/11.51 FO
356.84/18.84 FO
201.26/65.82 V
218.88/50.32 JT
25.81/57.74 V
350.95/61.74 V
42.4/18.91 FO
137.53/47.11 JT
168.48/75.66 JT
25.5/15.4 FO
238.84/28.9 JT
39.59/13.85 FO
15.62/28.8 JT
14.17/7.6 FO
244.07/26.69 JT
29.9/30.63 V
100.0%
100.0%
91.9%
100.0%
100.0%
90.9%
100.0%

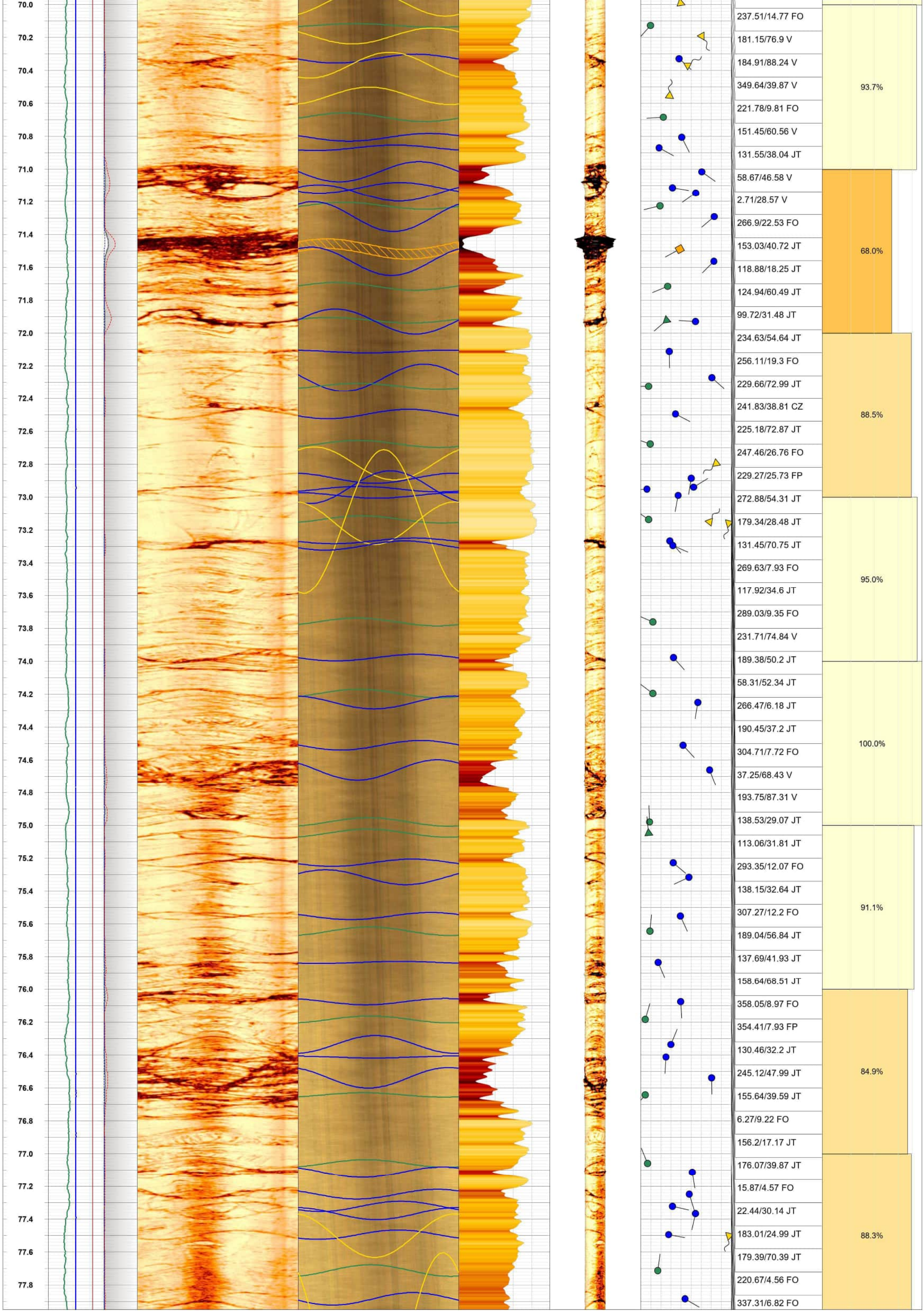

30.2
30.4
30.6
30.8
31.0
31.2
31.4
31.6
31.8
32.0
32.2
32.4
32.6
32.8
33.0
33.2
33.4
33.6
33.8
34.0
34.2
34.4
34.6
34.8
35.0
35.2
35.4
35.6
35.8
36.0
36.2
36.4
36.6
36.8
37.0
37.2
37.4
37.6
37.8
38.0
23.28/18.48 FO
346.5/33.14 V
25.48/10.38 FO
17.15/21.22 FO
207.02/73.25 JT
80.98/10.58 FO
153.63/62.63 JT
347.82/30.47 JT
290.94/3.8 FO
181.26/51.82 JT
22.62/49.69 V
34.43/41.85 V
278.25/7.34 FO
162.95/32.88 JT
2.42/50.85 V
114.09/47.93 JT
214.62/43.22 JT
29.82/15.17 FO
197.31/45.52 JT
41.2/50.86 V
25.18/87.89 V
179.43/59.71 JT
31.79/10.44 FO
221.61/34.4 JT
28.64/41.45 V
82.96/5.37 FO
221.48/56.98 JT
233.95/44.23 V
54.75/56.07 V
59.27/10.63 FO
81.73/4.17 FO
314.75/57.44 SH
213.67/2.07 FO
41.95/42.27 JT
220.44/56.55 JT
55.18/47.55 V
127.46/49.66 JT
248.65/6.54 FO
228.9/69.11 JT
294.47/32.85 JT
322.92/26.8 JT
198.3/14.67 JT
94.86/24.97 JT
95.74/9.58 JT
51.15/15.03 JT
7.7/23.43 FO
88.69/34.57 JT
195.22/26.99 SH
24.81/11.8 FO
100.0%
100.0%
95.7%
100.0%
99.5%
98.7%
74.9%
100.0%

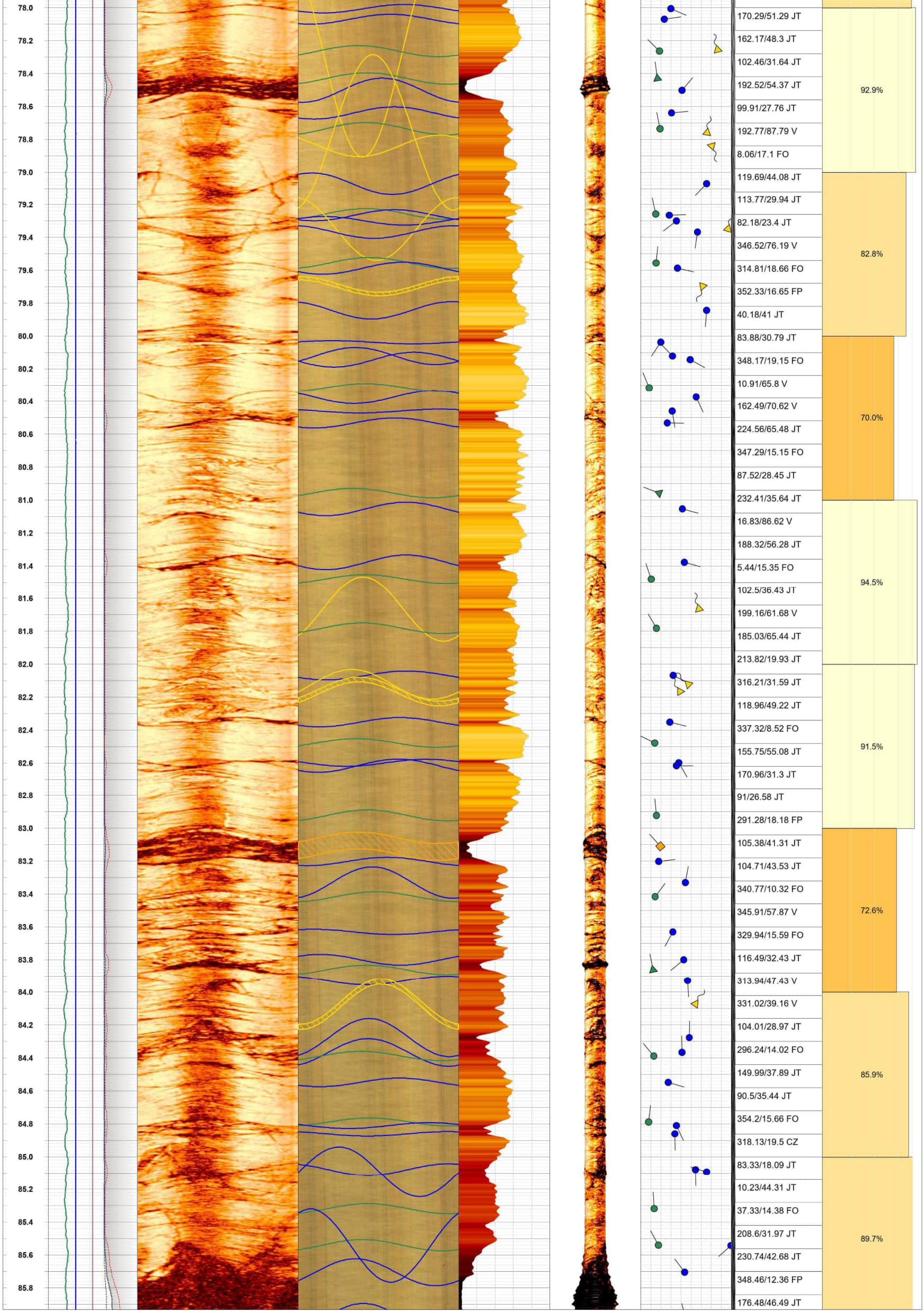

38.2
38.4
38.6
38.8
39.0
39.2
39.4
39.6
39.8
40.0
40.2
40.4
40.6
40.8
41.0
41.2
41.4
41.6
41.8
42.0
42.2
42.4
42.6
42.8
43.0
43.2
43.4
43.6
43.8
44.0
44.2
44.4
44.6
44.8
45.0
45.2
45.4
45.6
45.8
46.0
225.99/46.27 JT
232.66/34.15 JT
22.51/14.45 FO
348.89/13.62 FO
11.92/28.86 V
20.28/40.45 V
10.44/44.21 V
100.0%
2.25/14.74 FO
212.05/87.48 JT
358.75/59.62 V
149.55/33.88 JT
189.46/79.43 JT
3.06/63.85 V
1.91/58.26 V
86.2%
316.56/6.7 FO
1.02/47.96 JT
216.52/21.36 JT
127.27/39.39 JT
34.38/11.7 FO
64.27/16.45 FO
174.01/50.53 JT
64.7%
152.38/40.41 JT
41.3/49.22 V
336.75/87.39 V
4.53/12.6 FO
350.26/88.54 V
358.11/16.62 FO
249.62/20.08 JT
91.5%
160.03/54.03 SH
15.72/23.27 FO
163.76/87.87 JT
21.14/21.93 FO
232.23/57.23 JT
341.22/22.06 FO
350.4/89.11 V
91.5%
51.66/3 FO
25.34/38.5 V
95.2%
48.61/51.13 V
192.66/26.59 JT
330.95/17.04 FO
100.0%
250.73/17.88 FO
48.08/60.39 V
247.02/20.88 FO
174.43/50.47 JT
100.0%

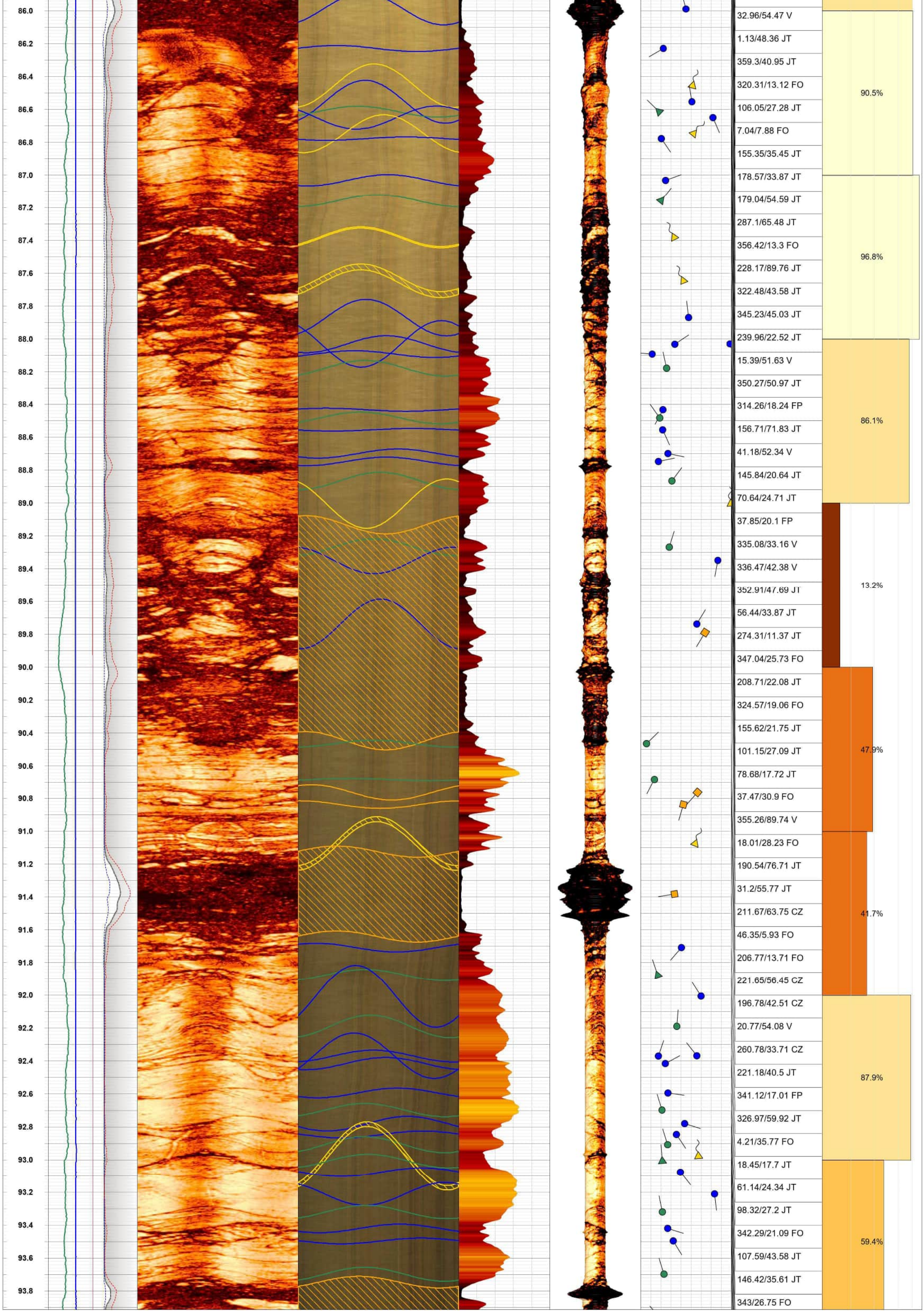

46.2
46.4
46.6
46.8
47.0
47.2
47.4
47.6
47.8
48.0
48.2
48.4
48.6
48.8
49.0
49.2
49.4
49.6
49.8
50.0
50.2
50.4
50.6
50.8
51.0
51.2
51.4
51.6
51.8
52.0
52.2
52.4
52.6
52.8
53.0
53.2
53.4
53.6
53.8
54.0
141.36/53.12 V
224.63/43.82 V
314.64/12.75 FO
248.87/47.67 JT
92.2%
309.92/13.03 FO
203.76/49.94 JT
235.69/50.3 JT
149.29/55.89 JT
256.02/16.47 FO
244.87/22.46 FO
82.2%
352.25/86.71 V
155.89/56.92 JT
247.5/46.87 JT
335.58/48.14 V
252.81/26.44 FO
95.4%
318.49/38.52 V
225.31/25.9 FO
359/45.27 SH
2.93/48.78 SH
12.87/41.17 SH
92.5%
31.62/38.79 SH
180.9/23.16 JT
13.77/12.33 FO
330.33/6.69 FO
206.62/87.8 JT
100.0%
308.46/17.99 FO
41.7/32.02 JT
10.02/15.08 FO
252.95/45.46 JT
240.05/37.03 JT
92.9%
3.98/20.52 FO
326.32/27.35 JT
25.05/42.64 JT
21.31/24.32 JT
131.47/52.84 FR
20.96/5.16 FO
119.37/49.05 JT
19.62/14.29 FO
80.0%
50.26/66.78 SH
30.35/43.37 V
269.65/9.7 FO
334.11/34.08 V
233.36/64.59 JT
97.7%


54.2
54.4
54.6
54.8
55.0
55.2
55.4
55.6
55.8
56.0
56.2
56.4
56.6
56.8
57.0
57.2
57.4
57.6
57.8
58.0
58.2
58.4
58.6
58.8
59.0
59.2
59.4
59.6
59.8
60.0
60.2
60.4
60.6
60.8
61.0
61.2
61.4
61.6
61.8
64.24/44.14 V
69.79/54.49 JT
306.86/3.15 FO
46.8/53.37 JT
220.92/63.08 JT
190.59/89.55 V
358.99/22.48 JT
311.7/10.77 FO
261.46/11.62 FO
233.79/50.28 JT
194.95/62.38 JT
175.95/76.16 V
345.18/12.21 FO
12.65/88.15 V
29.5/20.92 JT
119.24/50.76 JT
7.43/85.98 V
171.01/67.69 V
28.71/8.65 JT
191.19/66.92 V
19.63/50.51 V
62.71/45.4 V
246.13/14.99 FO
258.49/8.98 FO
100.0%
100.0%
100.0%
100.0%
100.0%
96.4%
79.4%


62.0
62.2
62.4
62.6
62.8
63.0
63.2
63.4
63.6
63.8
64.0
64.2
64.4
64.6
64.8
65.0
65.2
65.4
65.6
65.8
66.0
66.2
66.4
66.6
66.8
67.0
67.2
67.4
67.6
67.8
68.0
68.2
68.4
68.6
68.8
69.0
69.2
69.4
69.6
69.8
217.75/76.92 V
237.22/44.46 JT
3.6/81.41 JT
237.91/59.02 JT
142.56/59.35 JT
178.95/69.73 JT
198.41/5.59 FP
32.16/12.13 FO
194.13/81.96 V
166.41/65.17 JT
25.73/12.54 FO
170.17/60.55 JT
122.85/48.25 JT
129.37/46.59 JT
309.95/8.2 FO
65.36/49.38 JT
160.2/47.9 JT
38.76/55.69 JT
210.09/81.29 JT
229.52/17.13 FO
134.53/11.24 JT
245.55/28.74 JT
161.36/15.09 JT
172.21/40.79 JT
49.09/5.25 FO
189.7/84.67 JT
163.19/84.16 JT
133.72/36.35 CZ
192.23/24.89 JT
203.13/63.67 JT
294.12/4.62 FO
174.19/72.06 JT
344.94/11.35 FO
128.08/50.08 JT
142.38/54.11 JT
278.66/3.1 FP
344.57/12.36 FO
70.89/53.08 JT
346.77/1.77 FO
151.68/29.15 JT
183.34/36.38 JT
359.04/79.55 V
176.08/66.58 JT
206.09/2.78 FO
181.33/68.75 JT
343.15/79.96 V
147.88/38.24 JT
187.9/72.46 JT
327.75/8.53 FO
176.93/54.39 JT
32.7/42.41 JT
214.56/72.69 V
0.93/44.04 JT
5.25/8.54 FP
332.63/45.66 V
185.25/86.34 V
98.3%
90.0%
69.5%
84.0%
97.4%
97.2%
80.6%
100.0%


70.0
70.2
70.4
70.6
70.8
71.0
71.2
71.4
71.6
71.8
72.0
72.2
72.4
72.6
72.8
73.0
73.2
73.4
73.6
73.8
74.0
74.2
74.4
74.6
74.8
75.0
75.2
75.4
75.6
75.8
76.0
76.2
76.4
76.6
76.8
77.0
77.2
77.4
77.6
77.8
237.51/14.77 FO
181.15/76.9 V
184.91/88.24 V
349.64/39.87 V
221.78/9.81 FO
151.45/60.56 V
131.55/38.04 JT
93.7%
58.67/46.58 V
2.71/28.57 V
266.9/22.53 FO
153.03/40.72 JT
118.88/18.25 JT
124.94/60.49 JT
99.72/31.48 JT
68.0%
234.63/54.64 JT
256.11/19.3 FO
229.66/72.99 JT
241.83/38.81 CZ
225.18/72.87 JT
247.46/26.76 FO
229.27/25.73 FP
88.5%
272.88/54.31 JT
179.34/28.48 JT
131.45/70.75 JT
269.63/7.93 FO
117.92/34.6 JT
289.03/9.35 FO
231.71/74.84 V
95.0%
189.38/50.2 JT
58.31/52.34 JT
266.47/6.18 JT
190.45/37.2 JT
304.71/7.72 FO
37.25/68.43 V
193.75/87.31 V
100.0%
138.53/29.07 JT
113.06/31.81 JT
293.35/12.07 FO
138.15/32.64 JT
307.27/12.2 FO
189.04/56.84 JT
137.69/41.93 JT
158.64/68.51 JT
91.1%
358.05/8.97 FO
354.41/7.93 FP
130.46/32.2 JT
245.12/47.99 JT
155.64/39.59 JT
6.27/9.22 FO
156.2/17.17 JT
84.9%
176.07/39.87 JT
15.87/4.57 FO
22.44/30.14 JT
183.01/24.99 JT
179.39/70.39 JT
220.67/4.56 FO
337.31/6.82 FO
88.3%


78.0
78.2
78.4
78.6
78.8
79.0
79.2
79.4
79.6
79.8
80.0
80.2
80.4
80.6
80.8
81.0
81.2
81.4
81.6
81.8
82.0
82.2
82.4
82.6
82.8
83.0
83.2
83.4
83.6
83.8
84.0
84.2
84.4
84.6
84.8
85.0
85.2
85.4
85.6
85.8
170.29/51.29 JT
162.17/48.3 JT
102.46/31.64 JT
192.52/54.37 JT
99.91/27.76 JT
192.77/87.79 V
8.06/17.1 FO
92.9%
119.69/44.08 JT
113.77/29.94 JT
82.18/23.4 JT
346.52/76.19 V
314.81/18.66 FO
352.33/16.65 FP
40.18/41 JT
82.8%
83.88/30.79 JT
348.17/19.15 FO
10.91/65.8 V
162.49/70.62 V
224.56/65.48 JT
347.29/15.15 FO
87.52/28.45 JT
70.0%
232.41/35.64 JT
16.83/86.62 V
188.32/56.28 JT
5.44/15.35 FO
102.5/36.43 JT
199.16/61.68 V
185.03/65.44 JT
213.82/19.93 JT
94.5%
316.21/31.59 JT
118.96/49.22 JT
337.32/8.52 FO
155.75/55.08 JT
170.96/31.3 JT
91/26.58 JT
291.28/18.18 FP
91.5%
105.38/41.31 JT
104.71/43.53 JT
340.77/10.32 FO
345.91/57.87 V
329.94/15.59 FO
116.49/32.43 JT
313.94/47.43 V
72.6%
331.02/39.16 V
104.01/28.97 JT
296.24/14.02 FO
149.99/37.89 JT
90.5/35.44 JT
354.2/15.66 FO
318.13/19.5 CZ
85.9%
83.33/18.09 JT
10.23/44.31 JT
37.33/14.38 FO
208.6/31.97 JT
230.74/42.68 JT
348.46/12.36 FP
176.48/46.49 JT
89.7%


86.0
86.2
86.4
86.6
86.8
87.0
87.2
87.4
87.6
87.8
88.0
88.2
88.4
88.6
88.8
89.0
89.2
89.4
89.6
89.8
90.0
90.2
90.4
90.6
90.8
91.0
91.2
91.4
91.6
91.8
92.0
92.2
92.4
92.6
92.8
93.0
93.2
93.4
93.6
93.8
32.96/54.47 V
1.13/48.36 JT
359.3/40.95 JT
320.31/13.12 FO
106.05/27.28 JT
7.04/7.88 FO
155.35/35.45 JT
178.57/33.87 JT
179.04/54.59 JT
287.1/65.48 JT
356.42/13.3 FO
228.17/89.76 JT
322.48/43.58 JT
345.23/45.03 JT
239.96/22.52 JT
15.39/51.63 V
350.27/50.97 JT
314.26/18.24 FP
156.71/71.83 JT
41.18/52.34 V
145.84/20.64 JT
70.64/24.71 JT
37.85/20.1 FP
335.08/33.16 V
336.47/42.38 V
352.91/47.69 JT
56.44/33.87 JT
274.31/11.37 JT
347.04/25.73 FO
208.71/22.08 JT
324.57/19.06 FO
155.62/21.75 JT
101.15/27.09 JT
78.68/17.72 JT
37.47/30.9 FO
355.26/89.74 V
18.01/28.23 FO
190.54/76.71 JT
31.2/55.77 JT
211.67/63.75 CZ
46.35/5.93 FO
206.77/13.71 FO
221.65/56.45 CZ
196.78/42.51 CZ
20.77/54.08 V
260.78/33.71 CZ
221.18/40.5 JT
341.12/17.01 FP
326.97/59.92 JT
4.21/35.77 FO
18.45/17.7 JT
61.14/24.34 JT
98.32/27.2 JT
342.29/21.09 FO
107.59/43.58 JT
146.42/35.61 JT
343/26.75 FO
90.5%
96.8%
86.1%
13.2%
47.9%
41.7%
87.9%
59.4%

Depth	Pick Discription	Corrected Picks
94.0	355.45/57.3 V	
94.2	355.64/21.4 FP	
94.4	140.96/39.55 JT	
94.6	173.08/73.24 JT	
94.8	349.04/21.37 FO	
95.0	106.91/26.59 JT	
95.2	148.02/32.13 JT	
95.4	342.52/23 FO	
95.6	318.78/19.99 CZ	
95.8	225.37/13.06 CZ	
96.0	260.14/30.62 JT	
96.2	19.62/23.06 FO	
96.4	175.19/25.93 JT	
96.6	53.77/27.67 JT	
96.8	23.73/16.38 JT	
97.0	7.52/27.61 FO	
97.2	226.24/82.38 JT	
97.4	139.48/57.26 JT	
97.6	39.23/18.09 FO	
97.8	172.39/47.95 JT	
98.0	356.05/43.31 JT	
98.2	122.73/38.09 JT	
98.4	182.82/73.15 FR	
98.6	149.17/20.82 JT	
98.8	14.15/43.73 JT	
99.0	1.32/15.25 FO	
99.2	176.08/68.98 JT	
99.4	327.38/22.68 FO	
99.6	252.24/42.19 CZ	
99.8	323.27/64.49 JT	
100.0	346.07/22.58 FO	
	182.57/83.62 JT	
	208.69/22.16 JT	
	9.82/32.63 V	
	19.23/11.74 FO	
	173.54/55.92 JT	
	345.13/49.45 JT	
	350.11/55.28 JT	
	76.59/15.9 JT	
	122.88/72.45 JT	
	120.27/36.64 JT	
	338.4/18.31 FO	
	95.92/29.75 JT	

50.8%

90.7%

75.0%

81.1%

1m:20m

Depth

0 deg 30
TILT
0 300
GR
0 360
Azim (TN)

70 170
Caliper-min
70 170
Caliper-max
70 170
Caliper-ave

0° 90° 180° 270° 0°
50 10000
ATV Amplitude-NM

0° 90° 180° 270° 0°
OTV-NM
0° 90° 180° 270° 0°
(Magn. North)
Apparent Picks

0 10000
Reflectivity

180°
Pseudo Core

0 90
(True North)
Corrected Picks

Pick Discription

Very Poor
Poor
Fair
Good
Excellent
RQD

Well Name:	MDD493
Surveys:	ATV, OPTV, GR
Location:	Bendigo
Company:	Santana

Service Company:	SPEIGHT DRILLING
Operator:	Gareth Speight
Date Logged:	16/01/2026
Drilling Company:	SPEIGHT DRILLING
Date Drilled:	
Field:	
County / Township:	
State / Province:	
Country:	

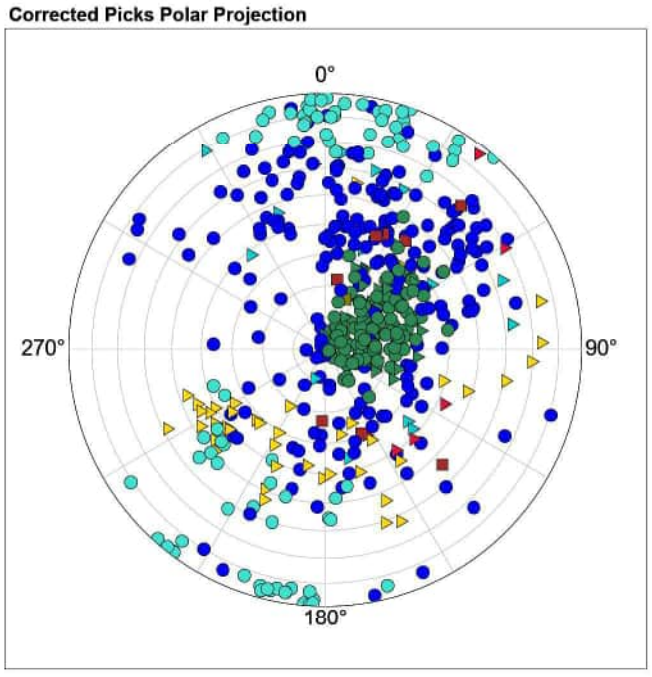
Log Measured From:	Ground Level		
Drilling Measured From:	Ground Level		
Driller Depth:	100	**Logger Depth:**	99
Inclination:	-69°	**Heading:**	024° (TN)
Easting:		**Northing:**	
Elevation:		**Grid:**	True North (22.5°)
Log Top:	1.6	**Log Bottom:**	99.7
Depth unit:	Meters	**Scale ratio:**	1 : 20

Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	60					
HQ	60	100				Wireline Length:	Depth Factor:

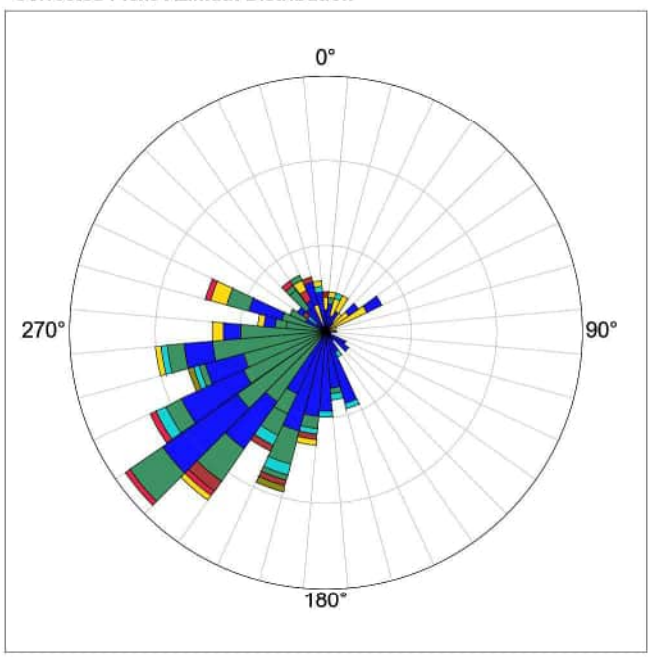
Remarks:

Corrected Picks referencing True North.

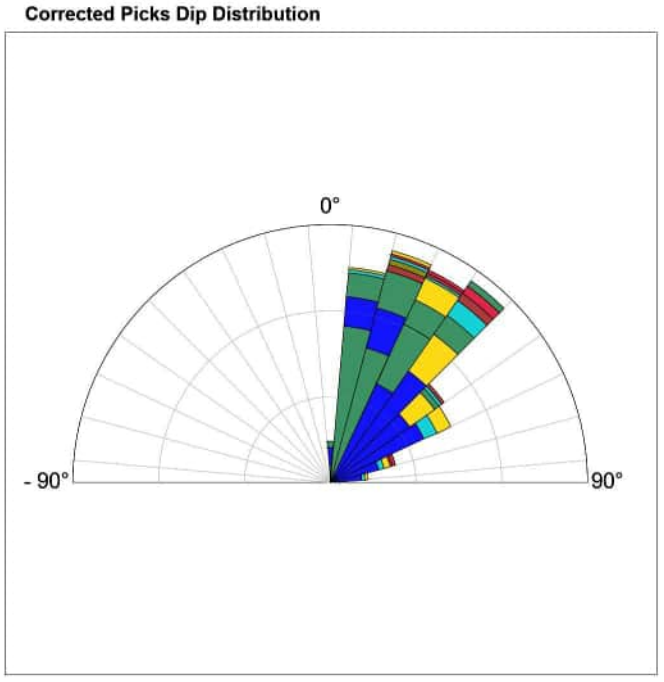
Corrected Picks Polar Projection



Corrected Picks Azimuth Distribution



Corrected Picks Dip Distribution

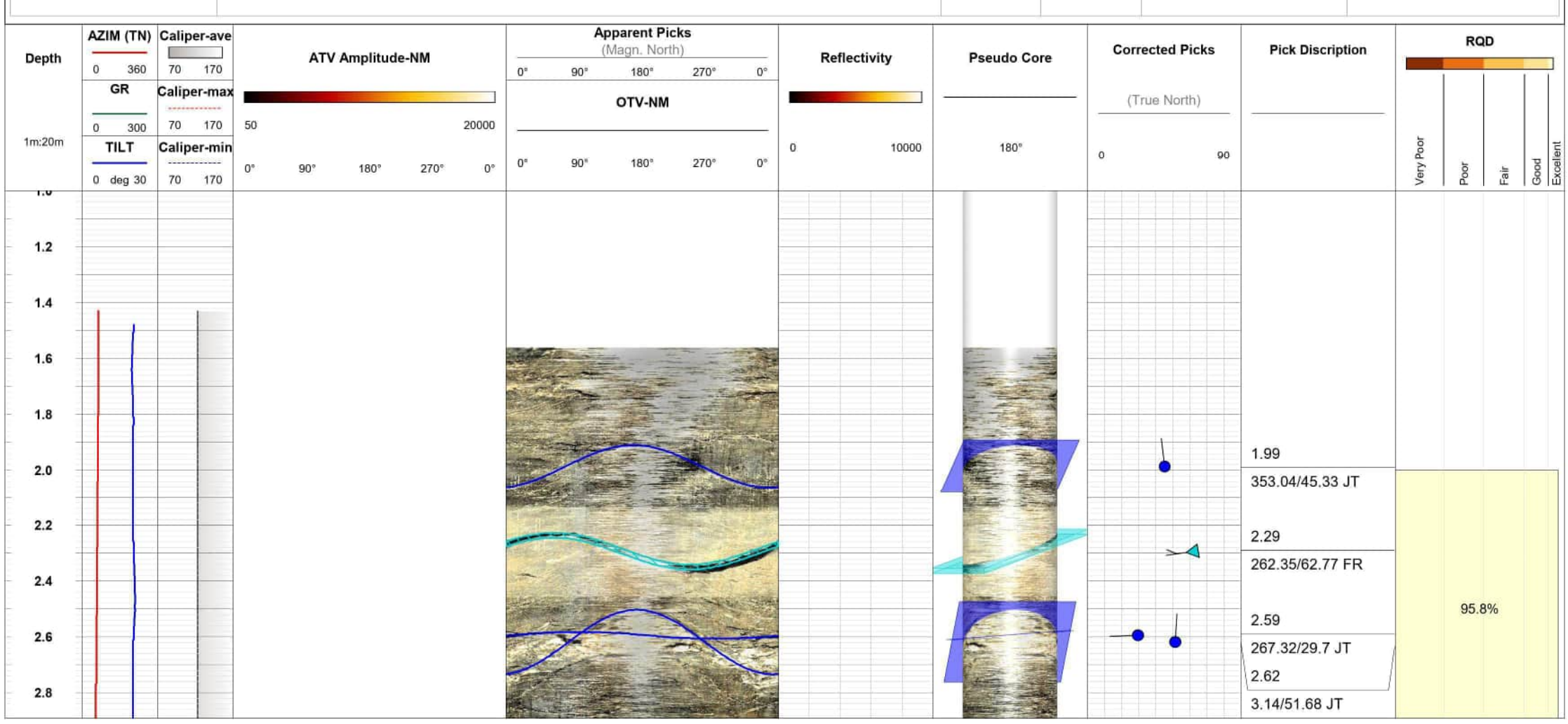


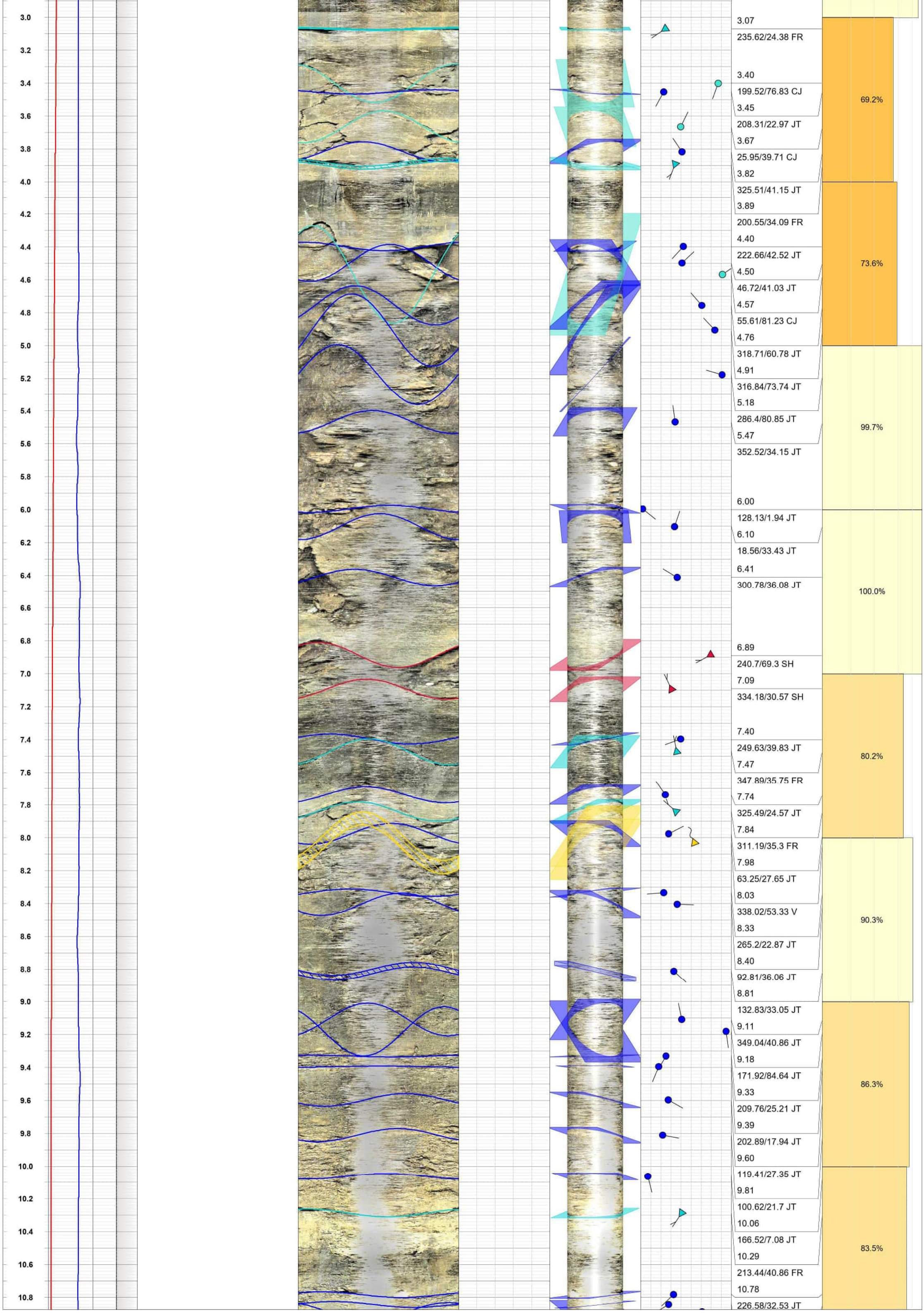
Legend:

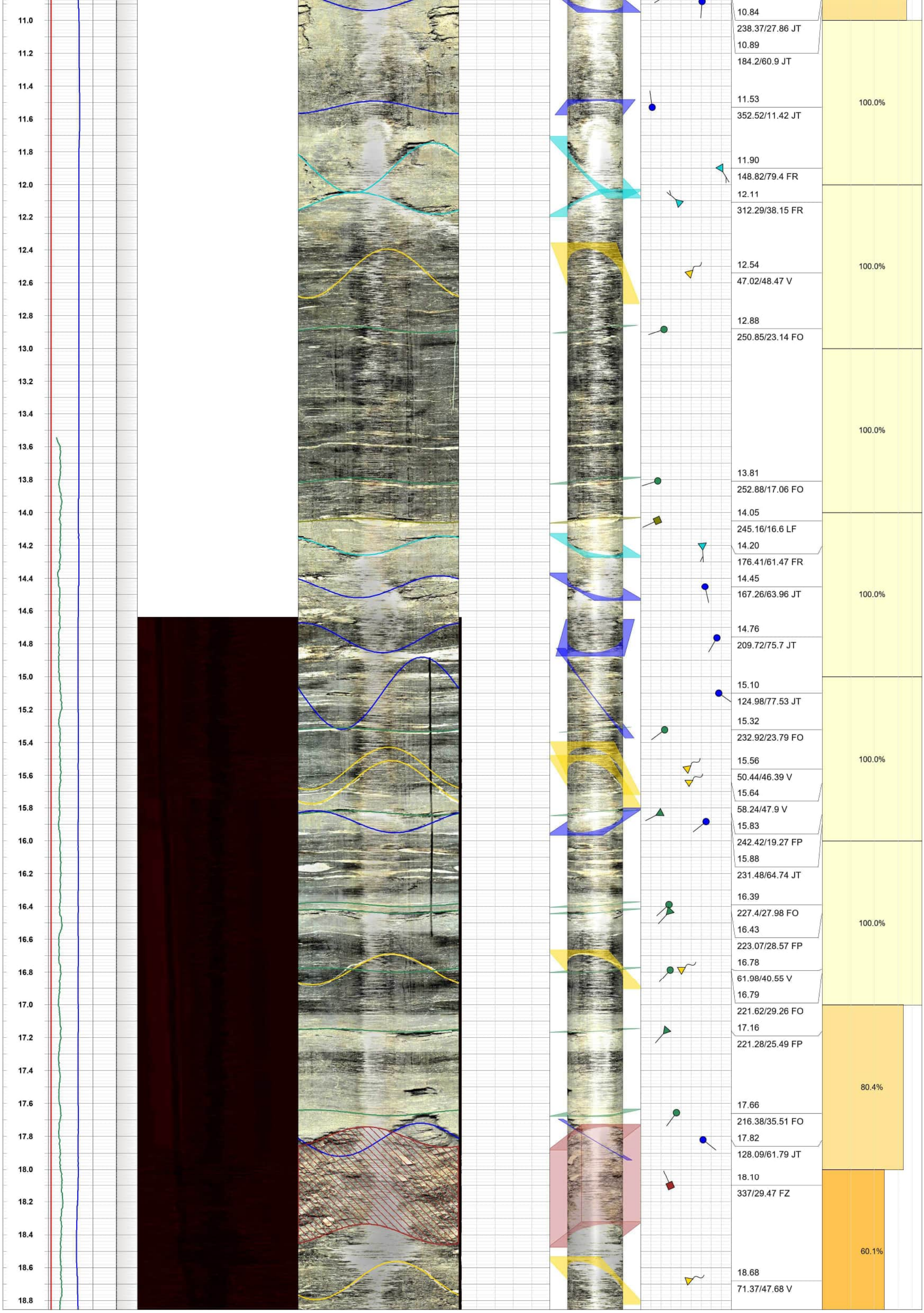


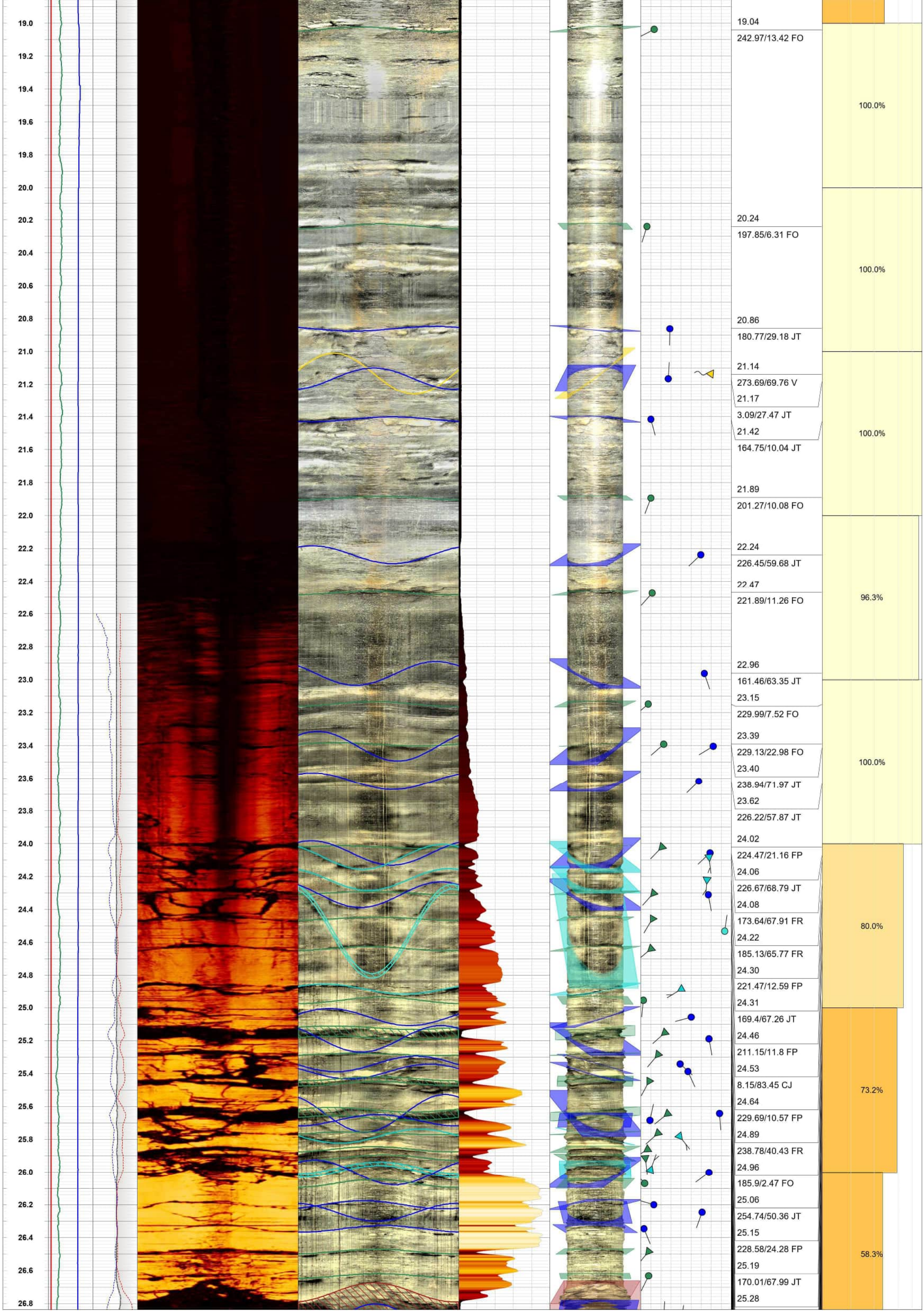
Curve Description:

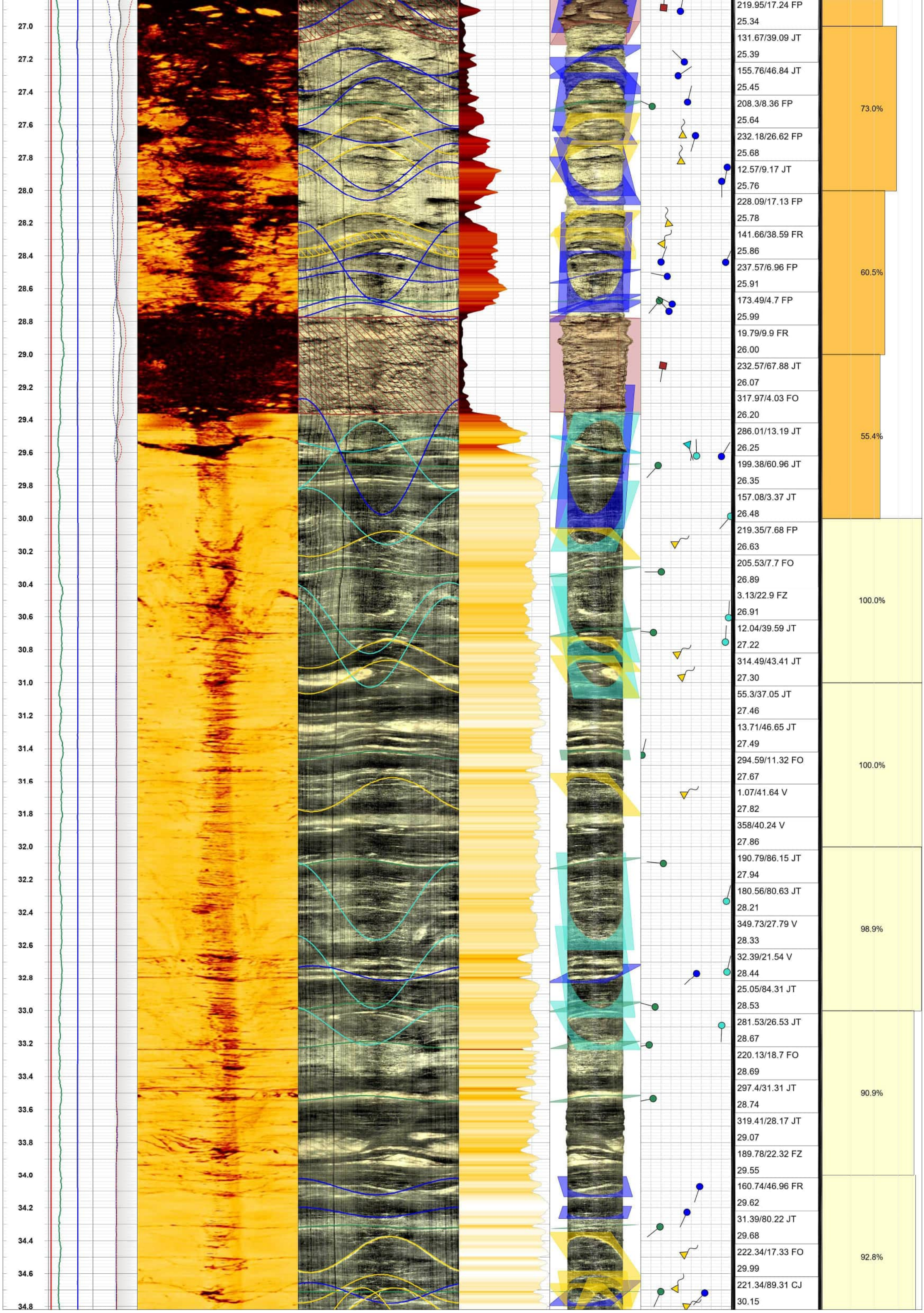
Title	Description	Top [m]	Base [m]	Tool s/n	Run / Date
Depth	Measured depth	1.6	99.7		
TVD	True vertical depth	1.6	99.7		
Tilt	Deviation from the vertical	1.6	99.7		
Azimuth (TN)	Deviation from True North	1.6	99.7		
GR	Natural gamma ray	1.6	99.7	ABI/GR 2204023	16/01/2026
Caliper	Borehole diameter from ATV traveltime	1.6	99.7		
Apparent Picks	Uncorrected structure picks from ATV and OTV images	1.6	99.7		
ATV	ATV amplitude image	14.6	99.7	ABI/GR 220402	16/01/2026
OTV	OTV image	1.6	99.7	OBI 222204	16/01/2026
Reflectivity	Acoustic reflectivity of the rock	14.6	99.7		
Corr. Picks	Structure picks correxcted for borehole deviation (oriented to True North)	1.6	99.7		
Picks Stats	Stereonet of observed defects, features per 5m interval	1.6	99.7		
Pseudo Core	3D poresentation of ATV amp;litude, borehole radius and apparent picks	1.6	99.7		

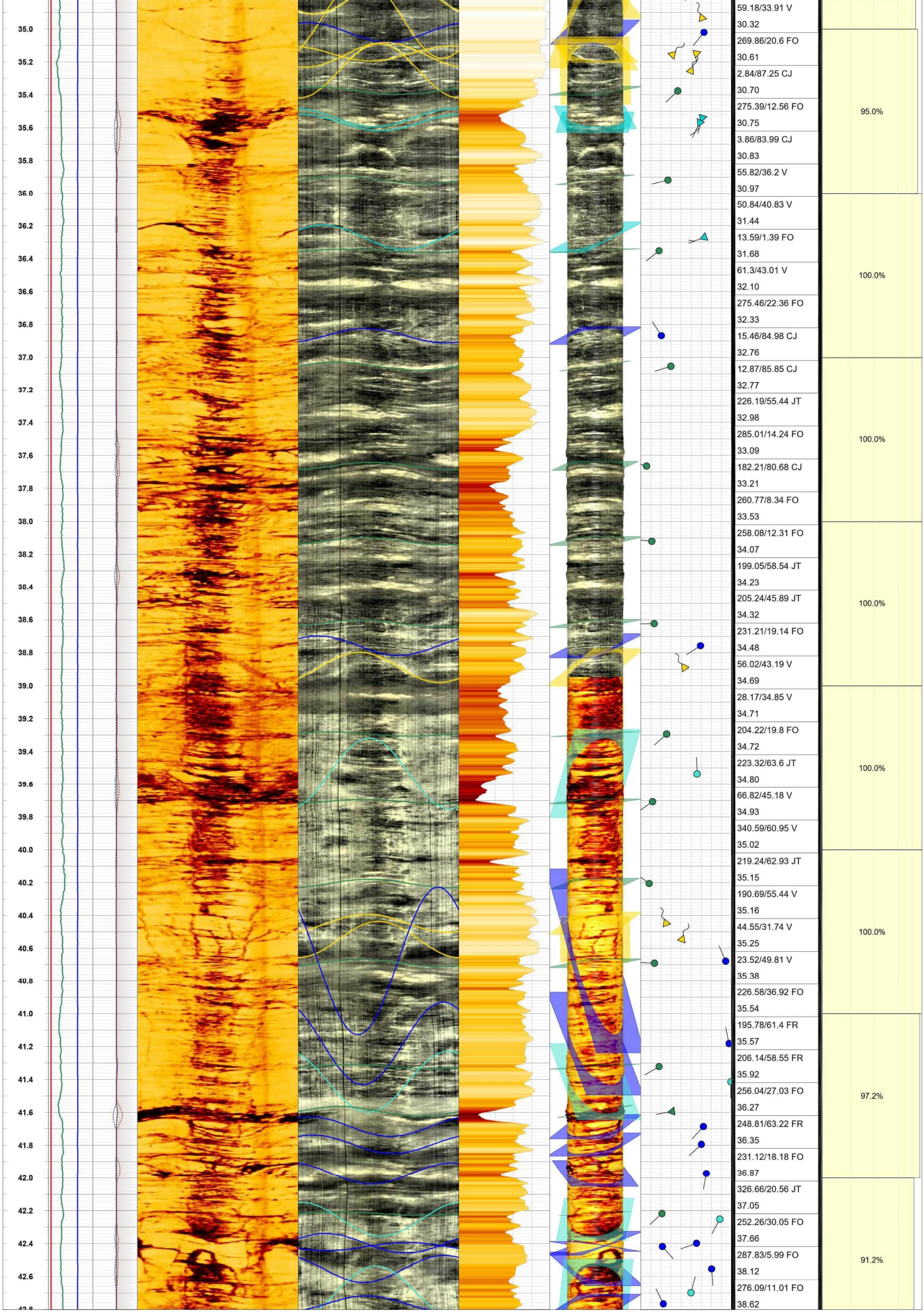


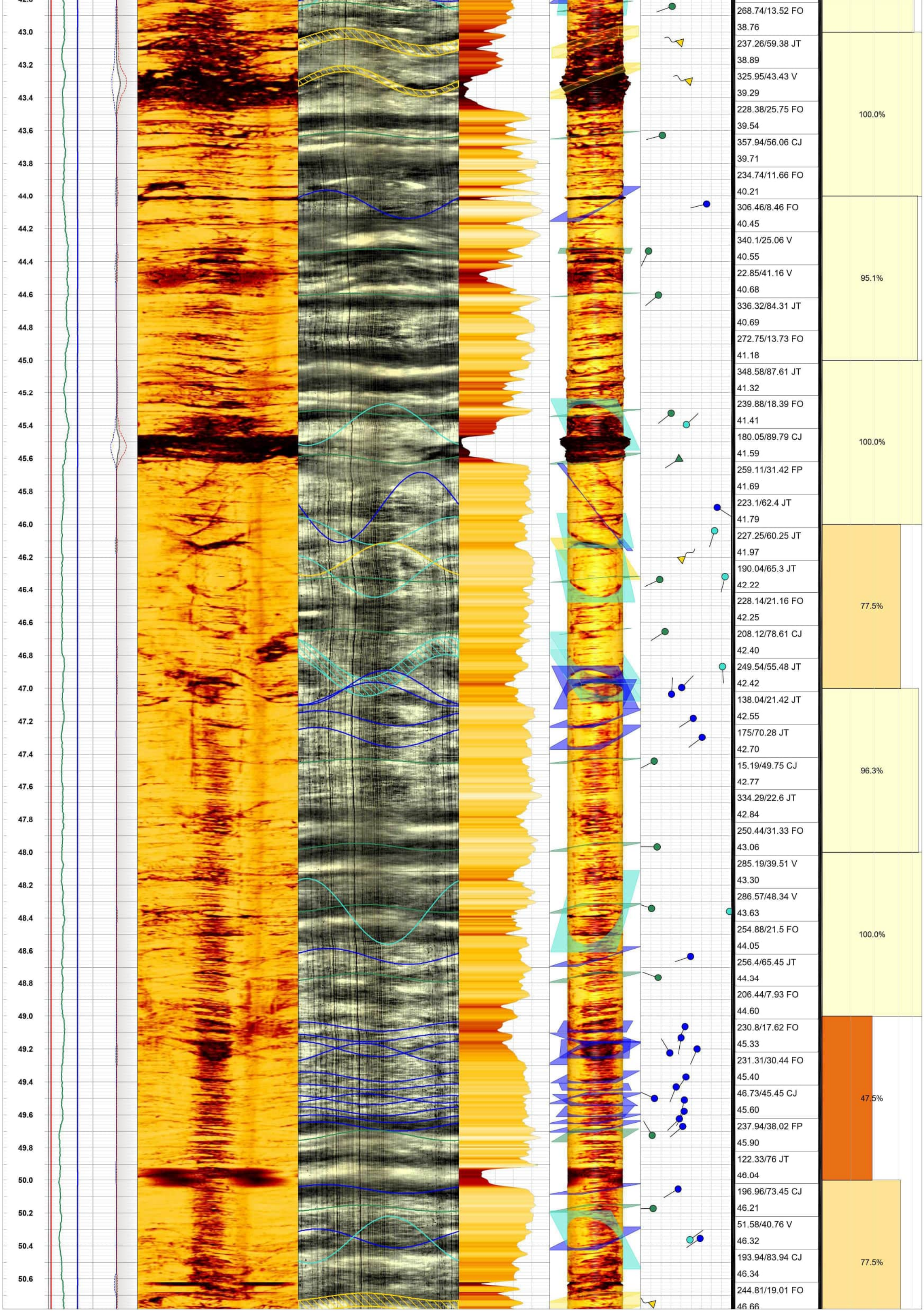

3.0
3.2
3.4
3.6
3.8
4.0
4.2
4.4
4.6
4.8
5.0
5.2
5.4
5.6
5.8
6.0
6.2
6.4
6.6
6.8
7.0
7.2
7.4
7.6
7.8
8.0
8.2
8.4
8.6
8.8
9.0
9.2
9.4
9.6
9.8
10.0
10.2
10.4
10.6
10.8
3.07
235.62/24.38 FR
3.40
199.52/76.83 CJ
3.45
208.31/22.97 JT
3.67
25.95/39.71 CJ
3.82
325.51/41.15 JT
3.89
200.55/34.09 FR
4.40
222.66/42.52 JT
4.50
46.72/41.03 JT
4.57
55.61/81.23 CJ
4.76
318.71/60.78 JT
4.91
316.84/73.74 JT
5.18
286.4/80.85 JT
5.47
352.52/34.15 JT
6.00
128.13/1.94 JT
6.10
18.56/33.43 JT
6.41
300.78/36.08 JT
6.89
240.7/69.3 SH
7.09
334.18/30.57 SH
7.40
249.63/39.83 JT
7.47
347.89/35.75 FR
7.74
325.49/24.57 JT
7.84
311.19/35.3 FR
7.98
63.25/27.65 JT
8.03
338.02/53.33 V
8.33
265.2/22.87 JT
8.40
92.81/36.06 JT
8.81
132.83/33.05 JT
9.11
349.04/40.86 JT
9.18
171.92/84.64 JT
9.33
209.76/25.21 JT
9.39
202.89/17.94 JT
9.60
119.41/27.35 JT
9.81
100.62/21.7 JT
10.06
166.52/7.08 JT
10.29
213.44/40.86 FR
10.78
226.58/32.53 JT
69.2%
73.6%
99.7%
100.0%
80.2%
90.3%
86.3%
83.5%

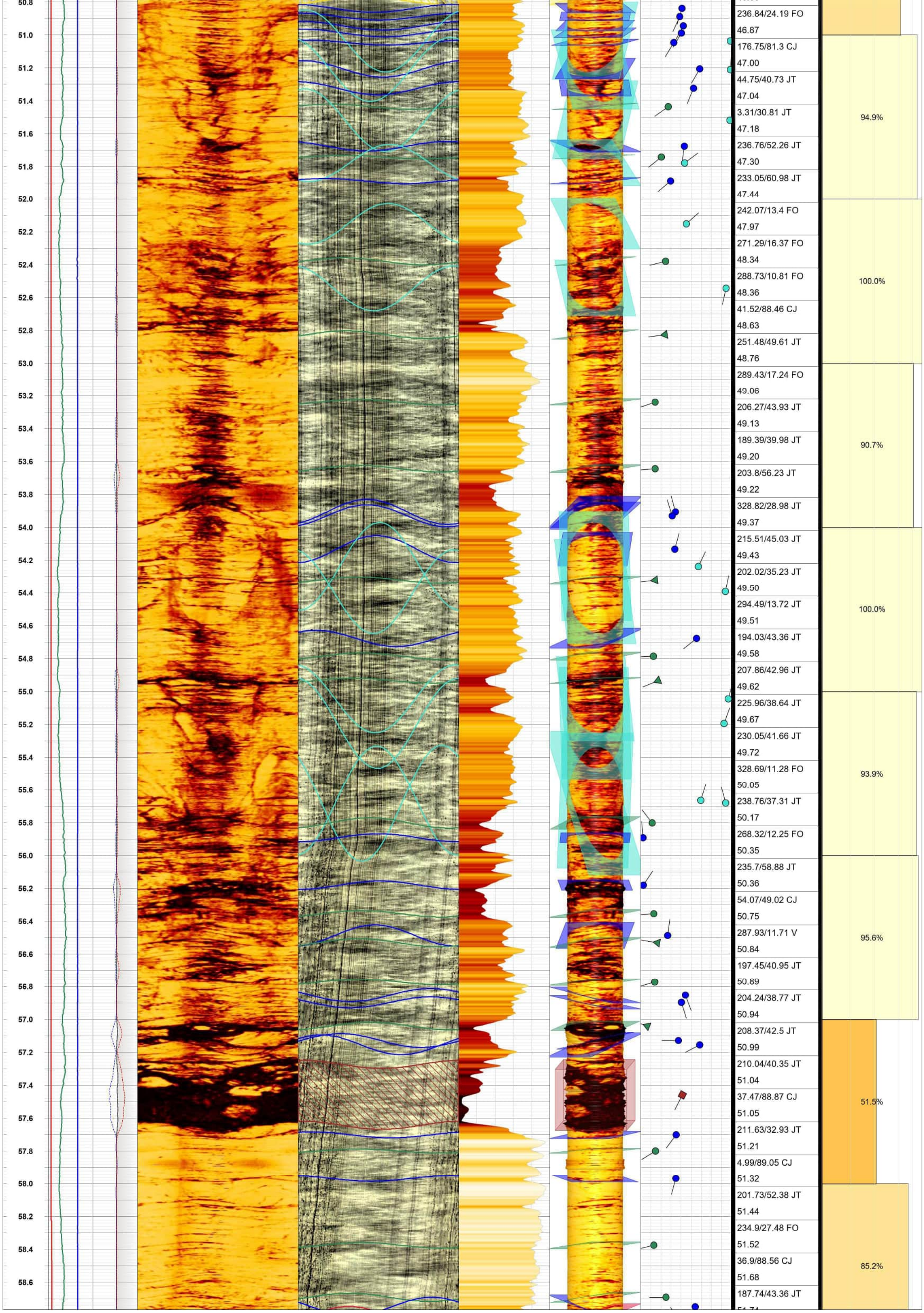

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11.2
11.4
11.6
11.8
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12.4
12.6
12.8
13.0
13.2
13.4
13.6
13.8
14.0
14.2
14.4
14.6
14.8
15.0
15.2
15.4
15.6
15.8
16.0
16.2
16.4
16.6
16.8
17.0
17.2
17.4
17.6
17.8
18.0
18.2
18.4
18.6
18.8
10.84
238.37/27.86 JT
10.89
184.2/60.9 JT
11.53
352.52/11.42 JT
11.90
148.82/79.4 FR
12.11
312.29/38.15 FR
12.54
47.02/48.47 V
12.88
250.85/23.14 FO
13.81
252.88/17.06 FO
14.05
245.16/16.6 LF
14.20
176.41/61.47 FR
14.45
167.26/63.96 JT
14.76
209.72/75.7 JT
15.10
124.98/77.53 JT
15.32
232.92/23.79 FO
15.56
50.44/46.39 V
15.64
58.24/47.9 V
15.83
242.42/19.27 FP
15.88
231.48/64.74 JT
16.39
227.4/27.98 FO
16.43
223.07/28.57 FP
16.78
61.98/40.55 V
16.79
221.62/29.26 FO
17.16
221.28/25.49 FP
17.66
216.38/35.51 FO
17.82
128.09/61.79 JT
18.10
337/29.47 FZ
18.68
71.37/47.68 V
100.0%
100.0%
100.0%
100.0%
80.4%
60.1%

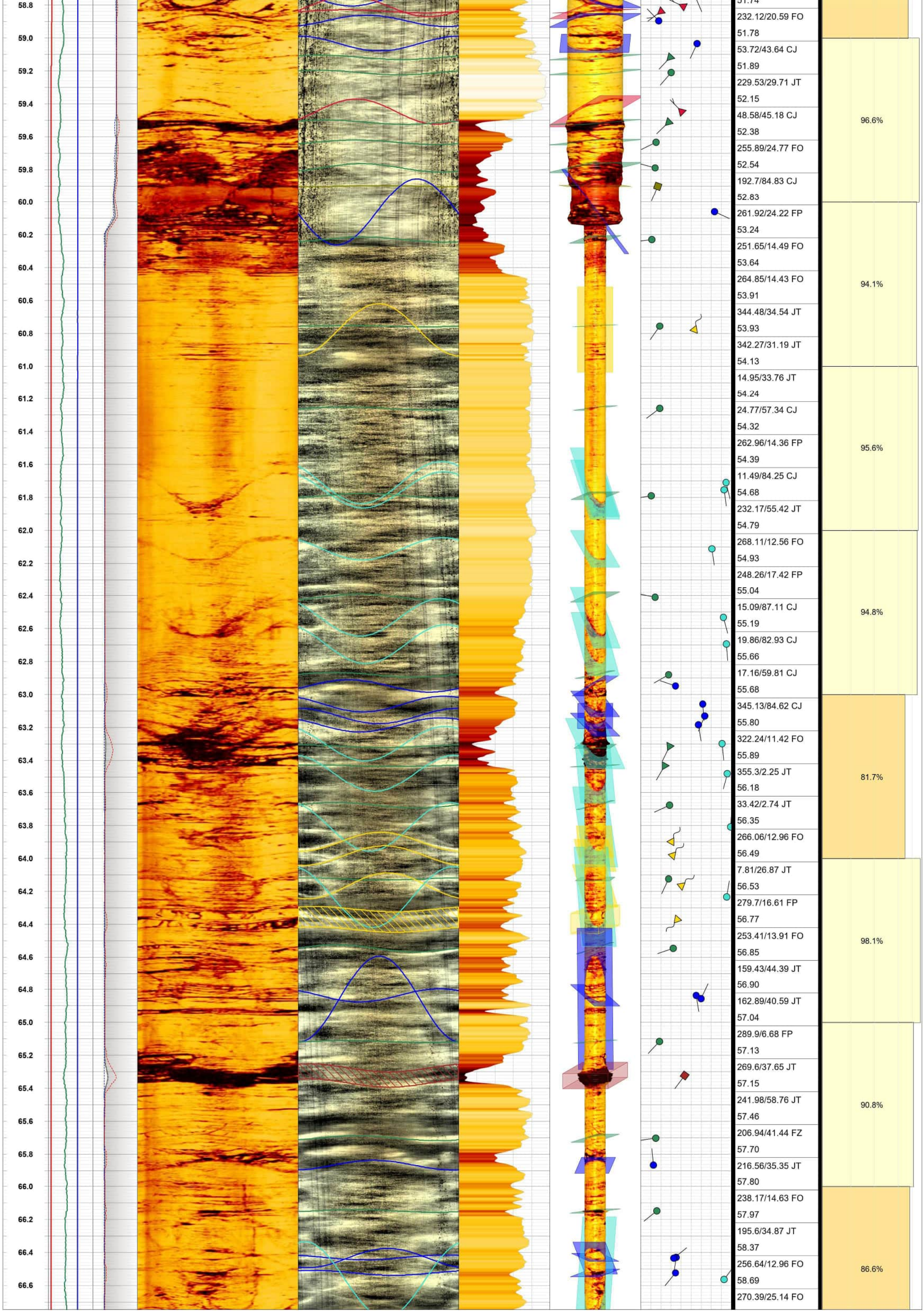

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20.6
20.8
21.0
21.2
21.4
21.6
21.8
22.0
22.2
22.4
22.6
22.8
23.0
23.2
23.4
23.6
23.8
24.0
24.2
24.4
24.6
24.8
25.0
25.2
25.4
25.6
25.8
26.0
26.2
26.4
26.6
26.8
19.04
242.97/13.42 FO
100.0%
20.24
197.85/6.31 FO
100.0%
20.86
180.77/29.18 JT
21.14
273.69/69.76 V
21.17
3.09/27.47 JT
21.42
164.75/10.04 JT
100.0%
21.89
201.27/10.08 FO
22.24
226.45/59.68 JT
22.47
221.89/11.26 FO
96.3%
22.96
161.46/63.35 JT
23.15
229.99/7.52 FO
23.39
229.13/22.98 FO
23.40
238.94/71.97 JT
23.62
226.22/57.87 JT
24.02
100.0%
224.47/21.16 FP
24.06
226.67/68.79 JT
24.08
173.64/67.91 FR
24.22
185.13/65.77 FR
24.30
221.47/12.59 FP
24.31
80.0%
169.4/67.26 JT
24.46
211.15/11.8 FP
24.53
8.15/83.45 CJ
24.64
229.69/10.57 FP
24.89
238.78/40.43 FR
24.96
73.2%
185.9/2.47 FO
25.06
254.74/50.36 JT
25.15
228.58/24.28 FP
25.19
170.01/67.99 JT
25.28
58.3%

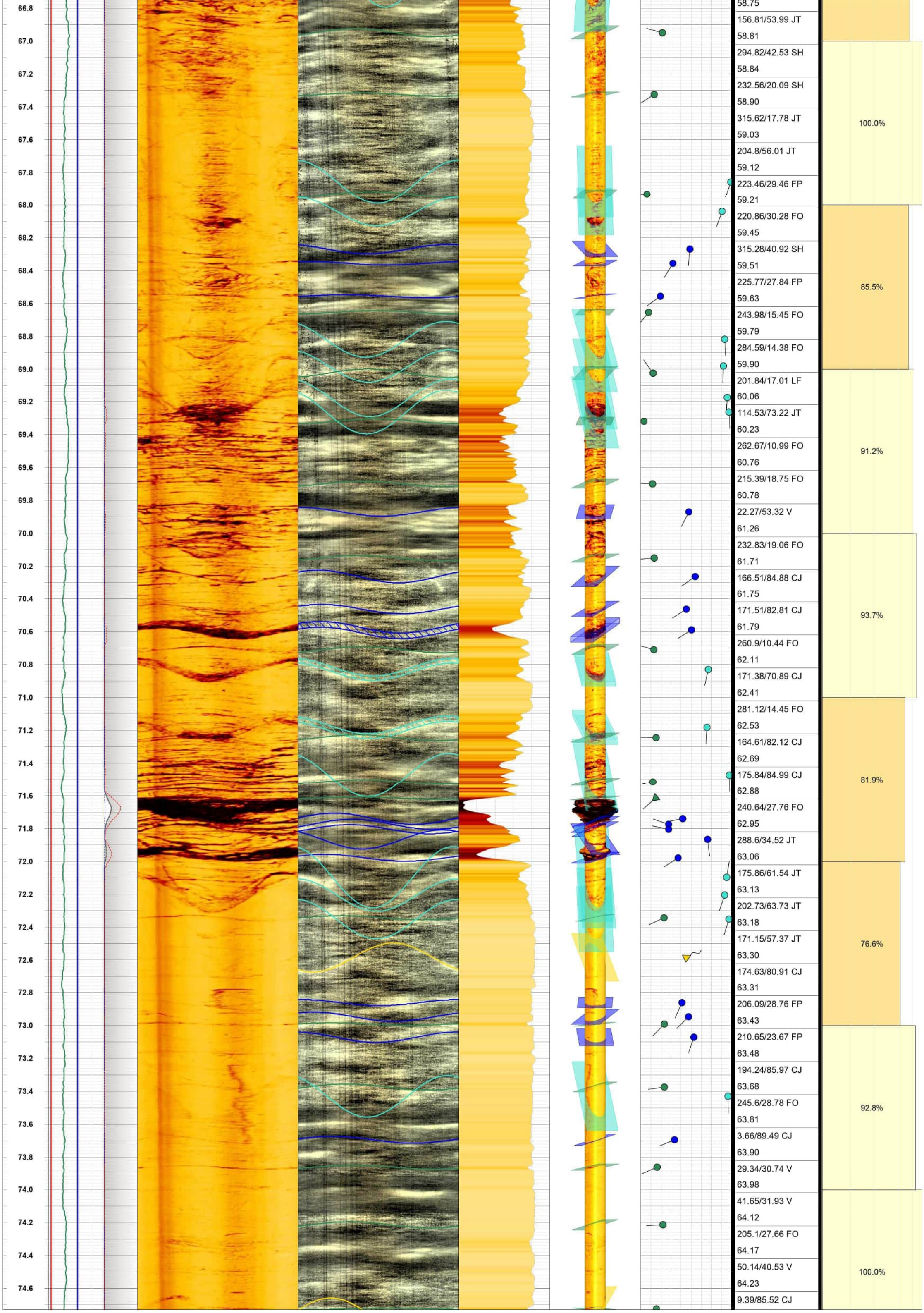

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33.0
33.2
33.4
33.6
33.8
34.0
34.2
34.4
34.6
34.8
219.95/17.24 FP
25.34
131.67/39.09 JT
25.39
155.76/46.84 JT
25.45
208.3/8.36 FP
25.64
232.18/26.62 FP
25.68
12.57/9.17 JT
25.76
228.09/17.13 FP
25.78
141.66/38.59 FR
25.86
237.57/6.96 FP
25.91
173.49/4.7 FP
25.99
19.79/9.9 FR
26.00
232.57/67.88 JT
26.07
317.97/4.03 FO
26.20
286.01/13.19 JT
26.25
199.38/60.96 JT
26.35
157.08/3.37 JT
26.48
219.35/7.68 FP
26.63
205.53/7.7 FO
26.89
3.13/22.9 FZ
26.91
12.04/39.59 JT
27.22
314.49/43.41 JT
27.30
55.3/37.05 JT
27.46
13.71/46.65 JT
27.49
294.59/11.32 FO
27.67
1.07/41.64 V
27.82
358/40.24 V
27.86
190.79/86.15 JT
27.94
180.56/80.63 JT
28.21
349.73/27.79 V
28.33
32.39/21.54 V
28.44
25.05/84.31 JT
28.53
281.53/26.53 JT
28.67
220.13/18.7 FO
28.69
297.4/31.31 JT
28.74
319.41/28.17 JT
29.07
189.78/22.32 FZ
29.55
160.74/46.96 FR
29.62
31.39/80.22 JT
29.68
222.34/17.33 FO
29.99
221.34/89.31 CJ
30.15
73.0%
60.5%
55.4%
100.0%
100.0%
98.9%
90.9%
92.8%

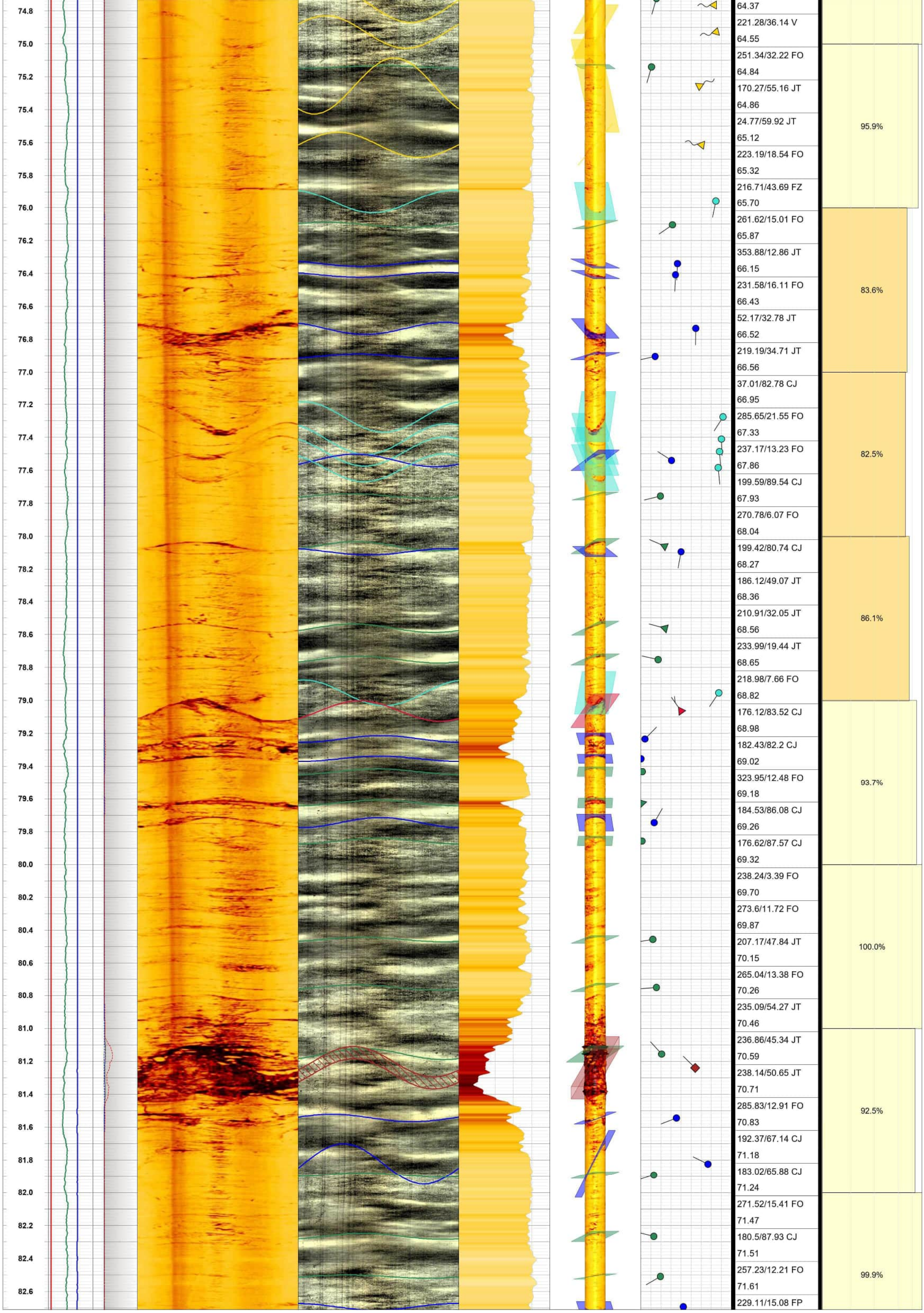

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37.6
37.8
38.0
38.2
38.4
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38.8
39.0
39.2
39.4
39.6
39.8
40.0
40.2
40.4
40.6
40.8
41.0
41.2
41.4
41.6
41.8
42.0
42.2
42.4
42.6
59.18/33.91 V
30.32
269.86/20.6 FO
30.61
2.84/87.25 CJ
30.70
275.39/12.56 FO
30.75
3.86/83.99 CJ
30.83
55.82/36.2 V
30.97
50.84/40.83 V
31.44
13.59/1.39 FO
31.68
61.3/43.01 V
32.10
275.46/22.36 FO
32.33
15.46/84.98 CJ
32.76
12.87/85.85 CJ
32.77
226.19/55.44 JT
32.98
285.01/14.24 FO
33.09
182.21/80.68 CJ
33.21
260.77/8.34 FO
33.53
258.08/12.31 FO
34.07
199.05/58.54 JT
34.23
205.24/45.89 JT
34.32
231.21/19.14 FO
34.48
56.02/43.19 V
34.69
28.17/34.85 V
34.71
204.22/19.8 FO
34.72
223.32/63.6 JT
34.80
66.82/45.18 V
34.93
340.59/60.95 V
35.02
219.24/62.93 JT
35.15
190.69/55.44 V
35.16
44.55/31.74 V
35.25
23.52/49.81 V
35.38
226.58/36.92 FO
35.54
195.78/61.4 FR
35.57
206.14/58.55 FR
35.92
256.04/27.03 FO
36.27
248.81/63.22 FR
36.35
231.12/18.18 FO
36.87
326.66/20.56 JT
37.05
252.26/30.05 FO
37.66
287.83/5.99 FO
38.12
276.09/11.01 FO
38.62
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100.0%
100.0%
100.0%
100.0%
97.2%
91.2%

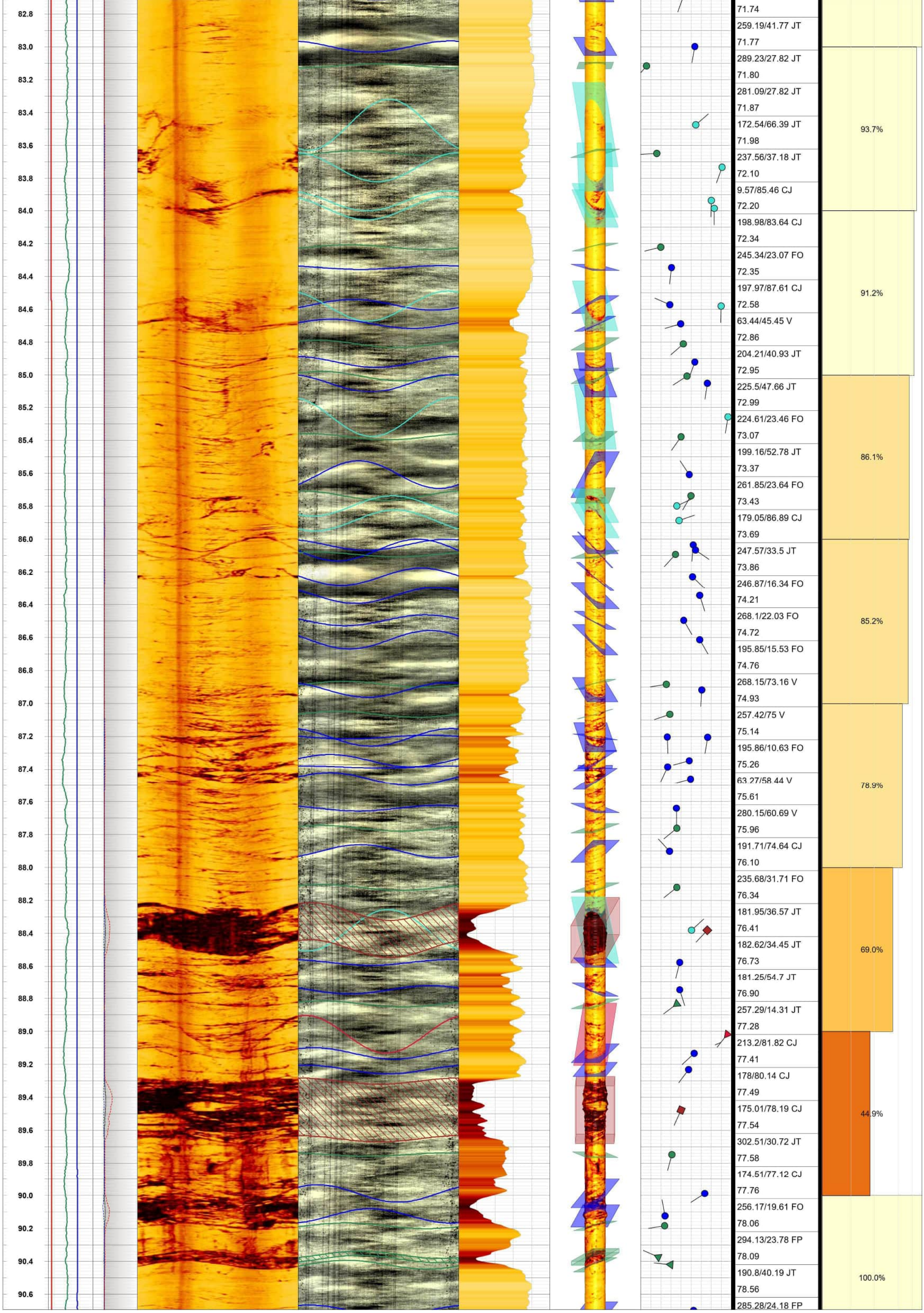

42.8
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45.2
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45.8
46.0
46.2
46.4
46.6
46.8
47.0
47.2
47.4
47.6
47.8
48.0
48.2
48.4
48.6
48.8
49.0
49.2
49.4
49.6
49.8
50.0
50.2
50.4
50.6
268.74/13.52 FO
38.76
237.26/59.38 JT
38.89
325.95/43.43 V
39.29
228.38/25.75 FO
39.54
357.94/56.06 CJ
39.71
234.74/11.66 FO
40.21
306.46/8.46 FO
40.45
340.1/25.06 V
40.55
22.85/41.16 V
40.68
336.32/84.31 JT
40.69
272.75/13.73 FO
41.18
348.58/87.61 JT
41.32
239.88/18.39 FO
41.41
180.05/89.79 CJ
41.59
259.11/31.42 FP
41.69
223.1/62.4 JT
41.79
227.25/60.25 JT
41.97
190.04/65.3 JT
42.22
228.14/21.16 FO
42.25
208.12/78.61 CJ
42.40
249.54/55.48 JT
42.42
138.04/21.42 JT
42.55
175/70.28 JT
42.70
15.19/49.75 CJ
42.77
334.29/22.6 JT
42.84
250.44/31.33 FO
43.06
285.19/39.51 V
43.30
286.57/48.34 V
43.63
254.88/21.5 FO
44.05
256.4/65.45 JT
44.34
206.44/7.93 FO
44.60
230.8/17.62 FO
45.33
231.31/30.44 FO
45.40
46.73/45.45 CJ
45.60
237.94/38.02 FP
45.90
122.33/76 JT
46.04
196.96/73.45 CJ
46.21
51.58/40.76 V
46.32
193.94/83.94 CJ
46.34
244.81/19.01 FO
46.66
100.0%
95.1%
100.0%
77.5%
96.3%
100.0%
47.5%
77.5%

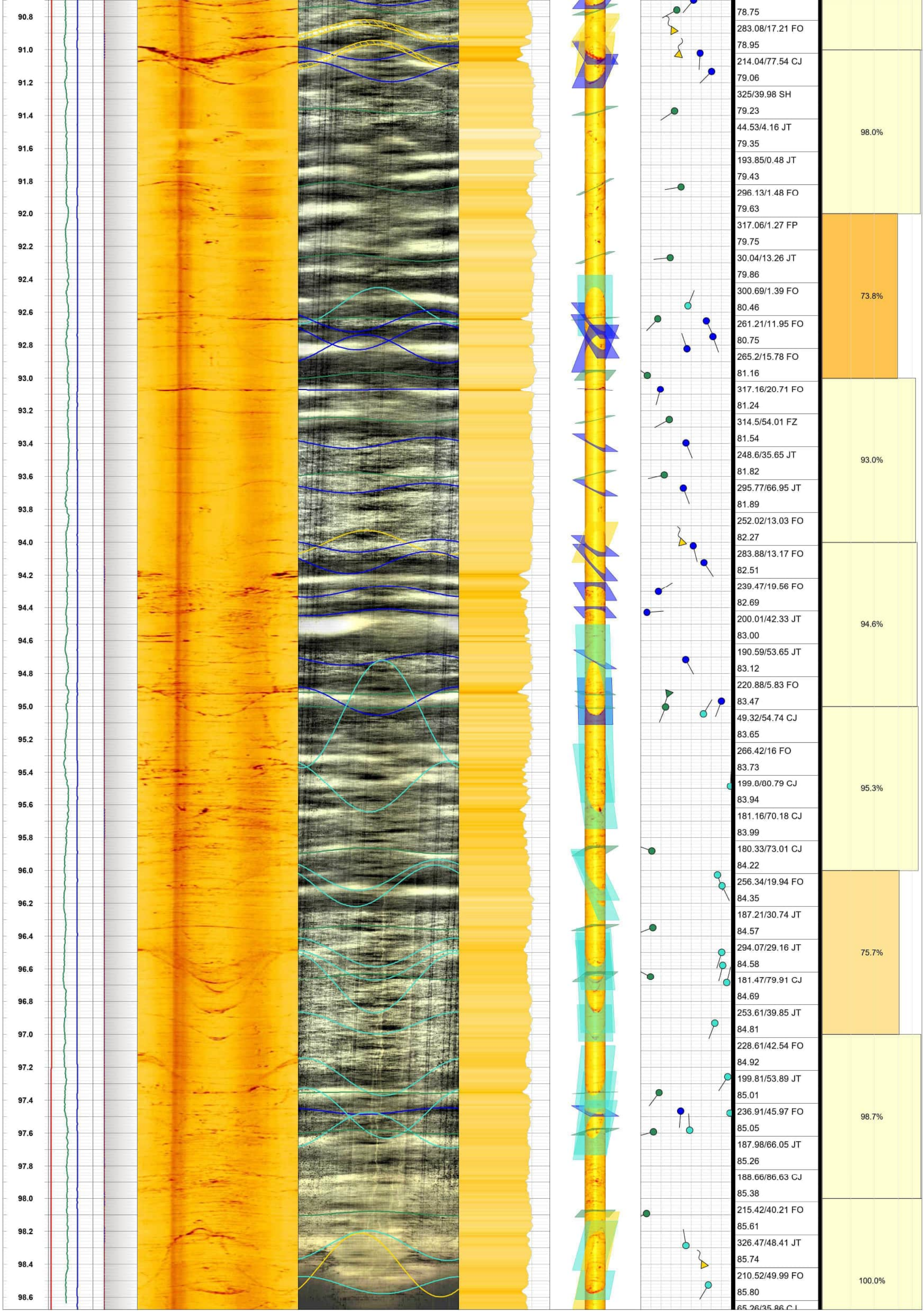

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51.4
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53.2
53.4
53.6
53.8
54.0
54.2
54.4
54.6
54.8
55.0
55.2
55.4
55.6
55.8
56.0
56.2
56.4
56.6
56.8
57.0
57.2
57.4
57.6
57.8
58.0
58.2
58.4
58.6
236.84/24.19 FO
46.87
176.75/81.3 CJ
47.00
44.75/40.73 JT
47.04
3.31/30.81 JT
47.18
94.9%
236.76/52.26 JT
47.30
233.05/60.98 JT
47.44
242.07/13.4 FO
47.97
271.29/16.37 FO
48.34
288.73/10.81 FO
48.36
100.0%
41.52/88.46 CJ
48.63
251.48/49.61 JT
48.76
289.43/17.24 FO
49.06
206.27/43.93 JT
49.13
189.39/39.98 JT
49.20
90.7%
203.8/56.23 JT
49.22
328.82/28.98 JT
49.37
215.51/45.03 JT
49.43
202.02/35.23 JT
49.50
294.49/13.72 JT
49.51
100.0%
194.03/43.36 JT
49.58
207.86/42.96 JT
49.62
225.96/38.64 JT
49.67
230.05/41.66 JT
49.72
328.69/11.28 FO
50.05
238.76/37.31 JT
50.17
268.32/12.25 FO
50.35
93.9%
235.7/58.88 JT
50.36
54.07/49.02 CJ
50.75
287.93/11.71 V
50.84
197.45/40.95 JT
50.89
204.24/38.77 JT
50.94
95.6%
208.37/42.5 JT
50.99
210.04/40.35 JT
51.04
37.47/88.87 CJ
51.05
211.63/32.93 JT
51.21
4.99/89.05 CJ
51.32
51.5%
201.73/52.38 JT
51.44
234.9/27.48 FO
51.52
36.9/88.56 CJ
51.68
187.74/43.36 JT
85.2%

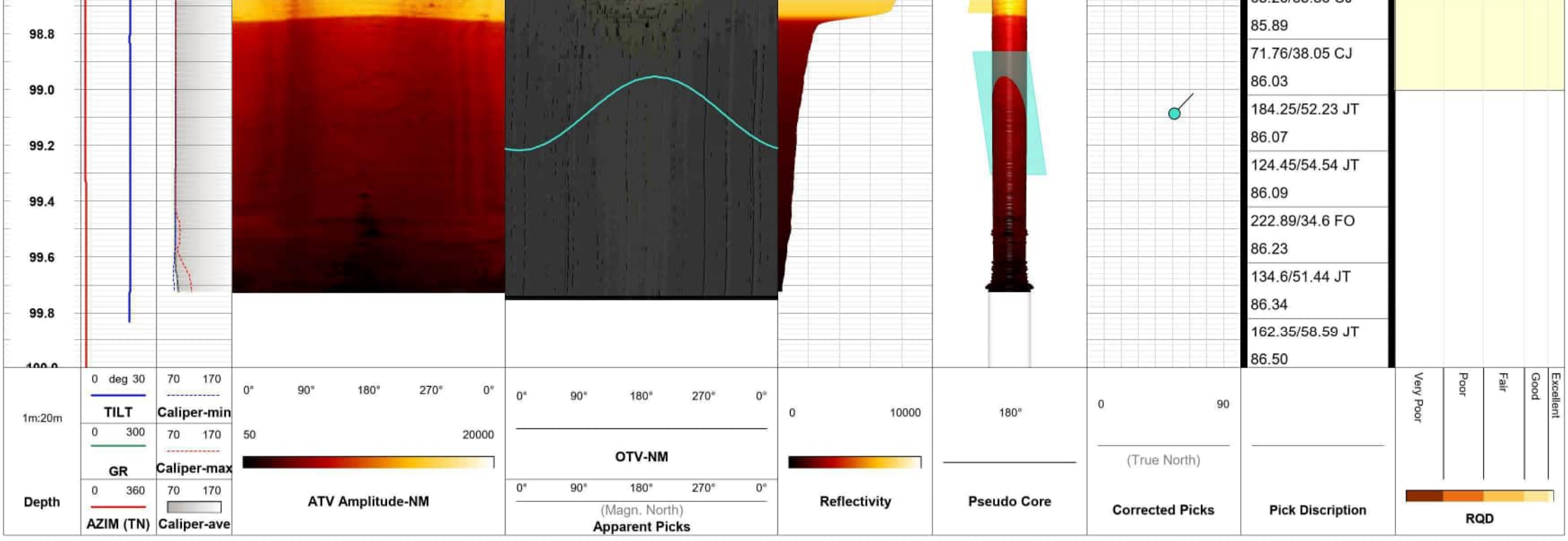

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60.2
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60.6
60.8
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61.2
61.4
61.6
61.8
62.0
62.2
62.4
62.6
62.8
63.0
63.2
63.4
63.6
63.8
64.0
64.2
64.4
64.6
64.8
65.0
65.2
65.4
65.6
65.8
66.0
66.2
66.4
66.6
51.74
232.12/20.59 FO
51.78
53.72/43.64 CJ
51.89
229.53/29.71 JT
52.15
48.58/45.18 CJ
52.38
96.6%
255.89/24.77 FO
52.54
192.7/84.83 CJ
52.83
261.92/24.22 FP
53.24
251.65/14.49 FO
53.64
264.85/14.43 FO
53.91
94.1%
344.48/34.54 JT
53.93
342.27/31.19 JT
54.13
14.95/33.76 JT
54.24
24.77/57.34 CJ
54.32
262.96/14.36 FP
54.39
95.6%
11.49/84.25 CJ
54.68
232.17/55.42 JT
54.79
268.11/12.56 FO
54.93
248.26/17.42 FP
55.04
15.09/87.11 CJ
55.19
94.8%
19.86/82.93 CJ
55.66
17.16/59.81 CJ
55.68
345.13/84.62 CJ
55.80
322.24/11.42 FO
55.89
355.3/2.25 JT
56.18
81.7%
33.42/2.74 JT
56.35
266.06/12.96 FO
56.49
7.81/26.87 JT
56.53
279.7/16.61 FP
56.77
253.41/13.91 FO
56.85
98.1%
159.43/44.39 JT
56.90
162.89/40.59 JT
57.04
289.9/6.68 FP
57.13
269.6/37.65 JT
57.15
241.98/58.76 JT
57.46
90.8%
206.94/41.44 FZ
57.70
216.56/35.35 JT
57.80
238.17/14.63 FO
57.97
195.6/34.87 JT
58.37
256.64/12.96 FO
58.69
86.6%
270.39/25.14 FO


66.8
67.0
67.2
67.4
67.6
67.8
68.0
68.2
68.4
68.6
68.8
69.0
69.2
69.4
69.6
69.8
70.0
70.2
70.4
70.6
70.8
71.0
71.2
71.4
71.6
71.8
72.0
72.2
72.4
72.6
72.8
73.0
73.2
73.4
73.6
73.8
74.0
74.2
74.4
74.6
58.75
156.81/53.99 JT
58.81
294.82/42.53 SH
58.84
232.56/20.09 SH
58.90
315.62/17.78 JT
59.03
204.8/56.01 JT
59.12
223.46/29.46 FP
59.21
220.86/30.28 FO
59.45
315.28/40.92 SH
59.51
225.77/27.84 FP
59.63
243.98/15.45 FO
59.79
284.59/14.38 FO
59.90
201.84/17.01 LF
60.06
114.53/73.22 JT
60.23
262.67/10.99 FO
60.76
215.39/18.75 FO
60.78
22.27/53.32 V
61.26
232.83/19.06 FO
61.71
166.51/84.88 CJ
61.75
171.51/82.81 CJ
61.79
260.9/10.44 FO
62.11
171.38/70.89 CJ
62.41
281.12/14.45 FO
62.53
164.61/82.12 CJ
62.69
175.84/84.99 CJ
62.88
240.64/27.76 FO
62.95
288.6/34.52 JT
63.06
175.86/61.54 JT
63.13
202.73/63.73 JT
63.18
171.15/57.37 JT
63.30
174.63/80.91 CJ
63.31
206.09/28.76 FP
63.43
210.65/23.67 FP
63.48
194.24/85.97 CJ
63.68
245.6/28.78 FO
63.81
3.66/89.49 CJ
63.90
29.34/30.74 V
63.98
41.65/31.93 V
64.12
205.1/27.66 FO
64.17
50.14/40.53 V
64.23
9.39/85.52 CJ
100.0%
91.2%
93.7%
81.9%
76.6%
92.8%
100.0%


74.8
75.0
75.2
75.4
75.6
75.8
76.0
76.2
76.4
76.6
76.8
77.0
77.2
77.4
77.6
77.8
78.0
78.2
78.4
78.6
78.8
79.0
79.2
79.4
79.6
79.8
80.0
80.2
80.4
80.6
80.8
81.0
81.2
81.4
81.6
81.8
82.0
82.2
82.4
82.6
64.37
221.28/36.14 V
64.55
251.34/32.22 FO
64.84
170.27/55.16 JT
64.86
24.77/59.92 JT
65.12
95.9%
223.19/18.54 FO
65.32
216.71/43.69 FZ
65.70
261.62/15.01 FO
65.87
353.88/12.86 JT
66.15
231.58/16.11 FO
66.43
83.6%
52.17/32.78 JT
66.52
219.19/34.71 JT
66.56
37.01/82.78 CJ
66.95
285.65/21.55 FO
67.33
237.17/13.23 FO
67.86
82.5%
199.59/89.54 CJ
67.93
270.78/6.07 FO
68.04
199.42/80.74 CJ
68.27
186.12/49.07 JT
68.36
210.91/32.05 JT
68.56
86.1%
233.99/19.44 JT
68.65
218.98/7.66 FO
68.82
176.12/83.52 CJ
68.98
182.43/82.2 CJ
69.02
323.95/12.48 FO
69.18
93.7%
184.53/86.08 CJ
69.26
176.62/87.57 CJ
69.32
238.24/3.39 FO
69.70
273.6/11.72 FO
69.87
207.17/47.84 JT
70.15
100.0%
265.04/13.38 FO
70.26
235.09/54.27 JT
70.46
236.86/45.34 JT
70.59
238.14/50.65 JT
70.71
285.83/12.91 FO
70.83
92.5%
192.37/67.14 CJ
71.18
183.02/65.88 CJ
71.24
271.52/15.41 FO
71.47
180.5/87.93 CJ
71.51
257.23/12.21 FO
71.61
99.9%
229.11/15.08 FP


82.8
83.0
83.2
83.4
83.6
83.8
84.0
84.2
84.4
84.6
84.8
85.0
85.2
85.4
85.6
85.8
86.0
86.2
86.4
86.6
86.8
87.0
87.2
87.4
87.6
87.8
88.0
88.2
88.4
88.6
88.8
89.0
89.2
89.4
89.6
89.8
90.0
90.2
90.4
90.6
71.74
259.19/41.77 JT
71.77
289.23/27.82 JT
71.80
281.09/27.82 JT
71.87
172.54/66.39 JT
71.98
237.56/37.18 JT
72.10
9.57/85.46 CJ
72.20
198.98/83.64 CJ
72.34
245.34/23.07 FO
72.35
197.97/87.61 CJ
72.58
63.44/45.45 V
72.86
204.21/40.93 JT
72.95
225.5/47.66 JT
72.99
224.61/23.46 FO
73.07
199.16/52.78 JT
73.37
261.85/23.64 FO
73.43
179.05/86.89 CJ
73.69
247.57/33.5 JT
73.86
246.87/16.34 FO
74.21
268.1/22.03 FO
74.72
195.85/15.53 FO
74.76
268.15/73.16 V
74.93
257.42/75 V
75.14
195.86/10.63 FO
75.26
63.27/58.44 V
75.61
280.15/60.69 V
75.96
191.71/74.64 CJ
76.10
235.68/31.71 FO
76.34
181.95/36.57 JT
76.41
182.62/34.45 JT
76.73
181.25/54.7 JT
76.90
257.29/14.31 JT
77.28
213.2/81.82 CJ
77.41
178/80.14 CJ
77.49
175.01/78.19 CJ
77.54
302.51/30.72 JT
77.58
174.51/77.12 CJ
77.76
256.17/19.61 FO
78.06
294.13/23.78 FP
78.09
190.8/40.19 JT
78.56
285.28/24.18 FP
93.7%
91.2%
86.1%
85.2%
78.9%
69.0%
44.9%
100.0%


90.8
91.0
91.2
91.4
91.6
91.8
92.0
92.2
92.4
92.6
92.8
93.0
93.2
93.4
93.6
93.8
94.0
94.2
94.4
94.6
94.8
95.0
95.2
95.4
95.6
95.8
96.0
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96.4
96.6
96.8
97.0
97.2
97.4
97.6
97.8
98.0
98.2
98.4
98.6
78.75
283.08/17.21 FO
78.95
214.04/77.54 CJ
79.06
325/39.98 SH
79.23
44.53/4.16 JT
79.35
193.85/0.48 JT
79.43
296.13/1.48 FO
79.63
317.06/1.27 FP
79.75
30.04/13.26 JT
79.86
300.69/1.39 FO
80.46
261.21/11.95 FO
80.75
265.2/15.78 FO
81.16
317.16/20.71 FO
81.24
314.5/54.01 FZ
81.54
248.6/35.65 JT
81.82
295.77/66.95 JT
81.89
252.02/13.03 FO
82.27
283.88/13.17 FO
82.51
239.47/19.56 FO
82.69
200.01/42.33 JT
83.00
190.59/53.65 JT
83.12
220.88/5.83 FO
83.47
49.32/54.74 CJ
83.65
266.42/16 FO
83.73
199.8/80.79 CJ
83.94
181.16/70.18 CJ
83.99
180.33/73.01 CJ
84.22
256.34/19.94 FO
84.35
187.21/30.74 JT
84.57
294.07/29.16 JT
84.58
181.47/79.91 CJ
84.69
253.61/39.85 JT
84.81
228.61/42.54 FO
84.92
199.81/53.89 JT
85.01
236.91/45.97 FO
85.05
187.98/66.05 JT
85.26
188.66/86.63 CJ
85.38
215.42/40.21 FO
85.61
326.47/48.41 JT
85.74
210.52/49.99 FO
85.80
98.0%
94.6%
73.8%
95.3%
75.7%
98.7%
100.0%


98.8
99.0
99.2
99.4
99.6
99.8
85.89
71.76/38.05 CJ
86.03
184.25/52.23 JT
86.07
124.45/54.54 JT
86.09
222.89/34.6 FO
86.23
134.6/51.44 JT
86.34
162.35/58.59 JT
86.50
1m:20m
Depth
0 deg 30
TILT
0 300
GR
0 360
AZIM (TN)
70 170
Caliper-min
70 170
Caliper-max
70 170
Caliper-ave
0° 90° 180° 270° 0°
50 20000
ATV Amplitude-NM
0° 90° 180° 270° 0°
OTV-NM
0° 90° 180° 270° 0°
(Magn. North)
Apparent Picks
0 10000
Reflectivity
180°
Pseudo Core
0 90
(True North)
Corrected Picks
Pick Discription
Very Poor
Poor
Fair
Good
Excellent
RQD

Well Name:	MDD502
Surveys:	ATV, OTV, GR
Location:	Bendigo
Company:	Santana

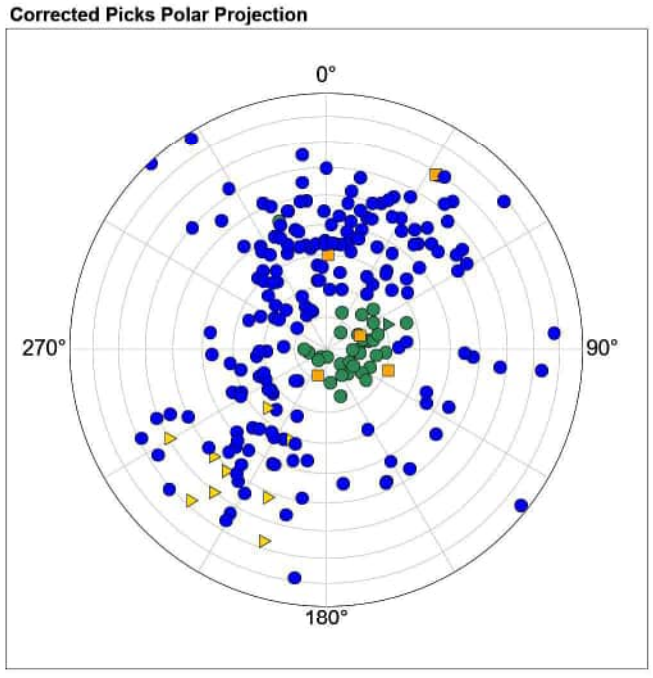
Service Company:	SPEIGHT DRILLING
Operator:	Gareth Speight
Date Logged:	14/02/2026
Drilling Company:	SPEIGHT DRILLING
Date Drilled:	
Field:	
County / Township:	
State / Province:	
Country:	

Log Measured From:	Ground Level		
Drilling Measured From:	Ground Level		
Driller Depth:	32	**Logger Depth:**	31.8
Inclination:	-67°	**Heading:**	207° (TN)
Easting:		**Northing:**	
Elevation:		**Grid:**	True North (22.5°)
Log Top:	0.4	**Log Bottom:**	31.8
Depth unit:	Meters	**Scale ratio:**	1 : 20

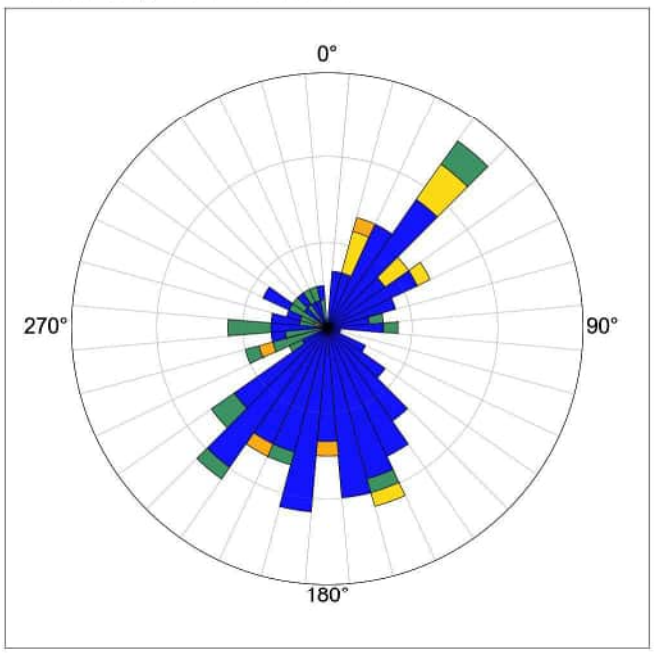
Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	32					
						Wireline Length:	Depth Factor:

Remarks:
Poor borehole conditions impacting structural interpretation confidence.

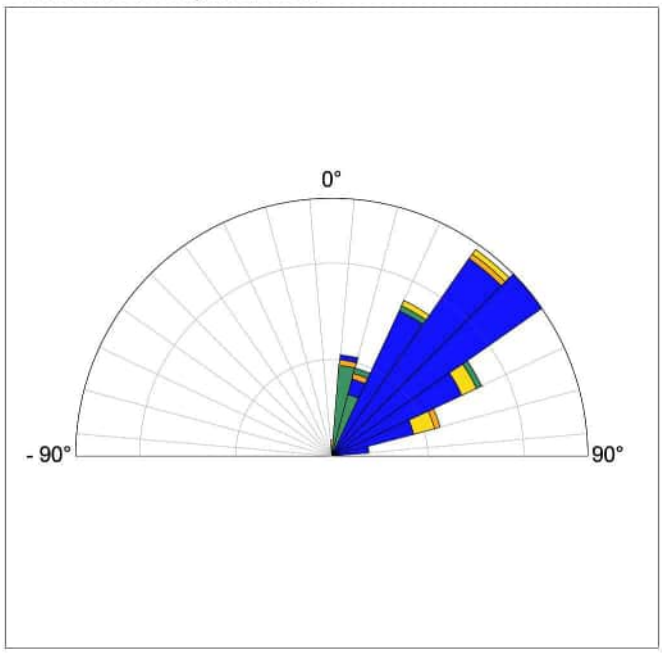
Corrected Picks Polar Projection



Corrected Picks Azimuth Distribution



Corrected Picks Dip Distribution

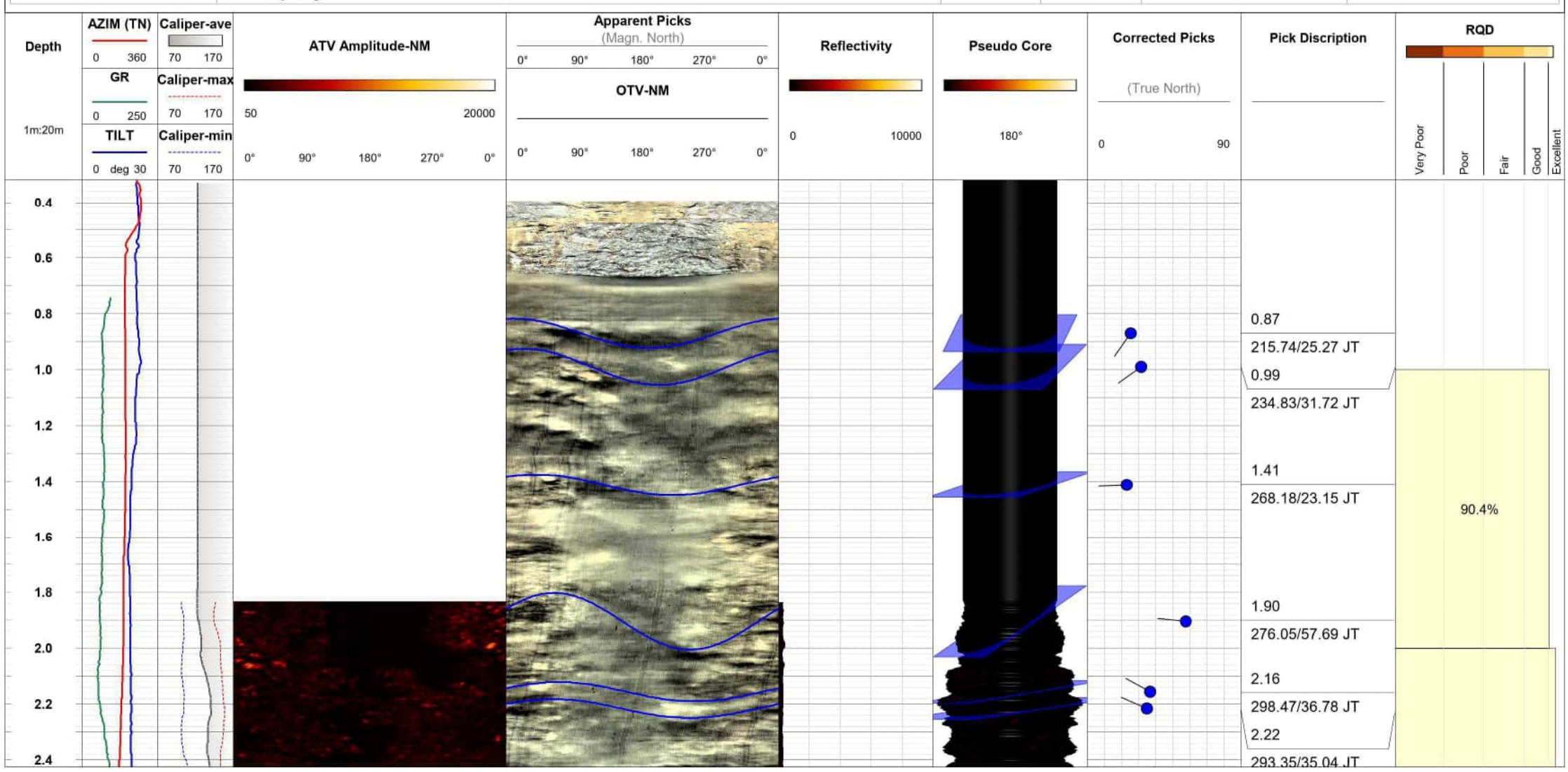


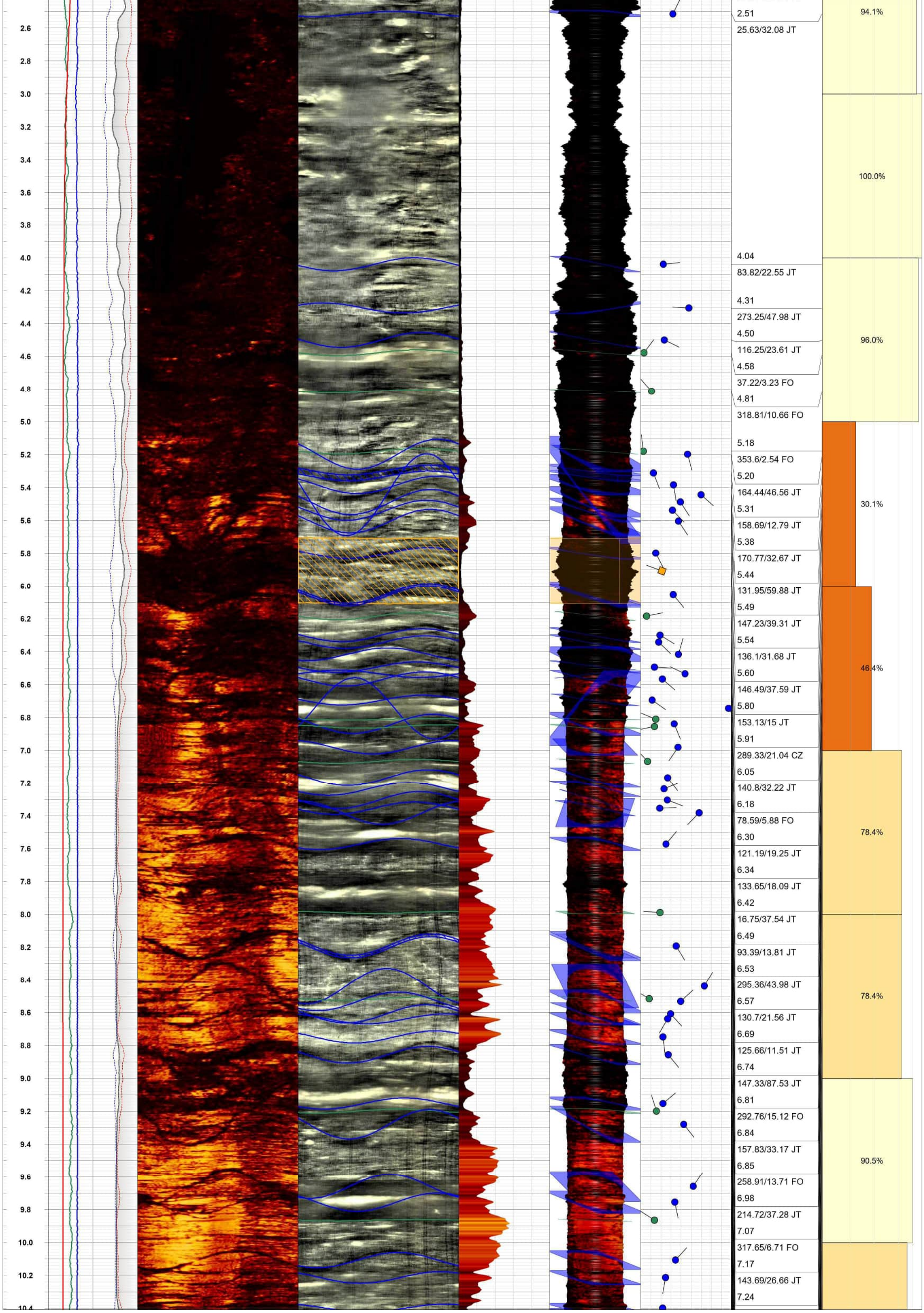
Legend:

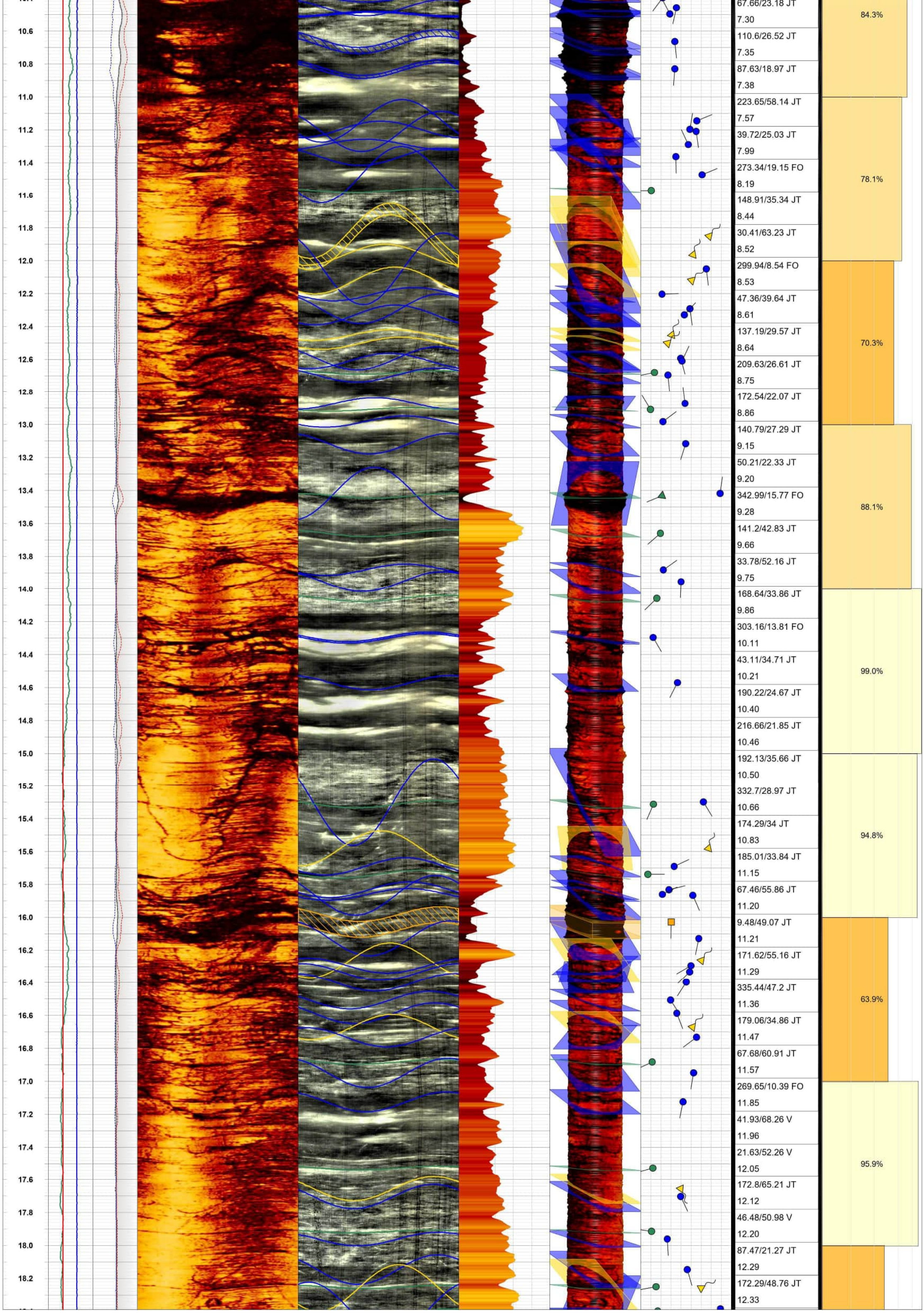
FO - Foliation | FP - Foliation Parting | JT - Joint | CZ - Crushed Zone | V - Vein

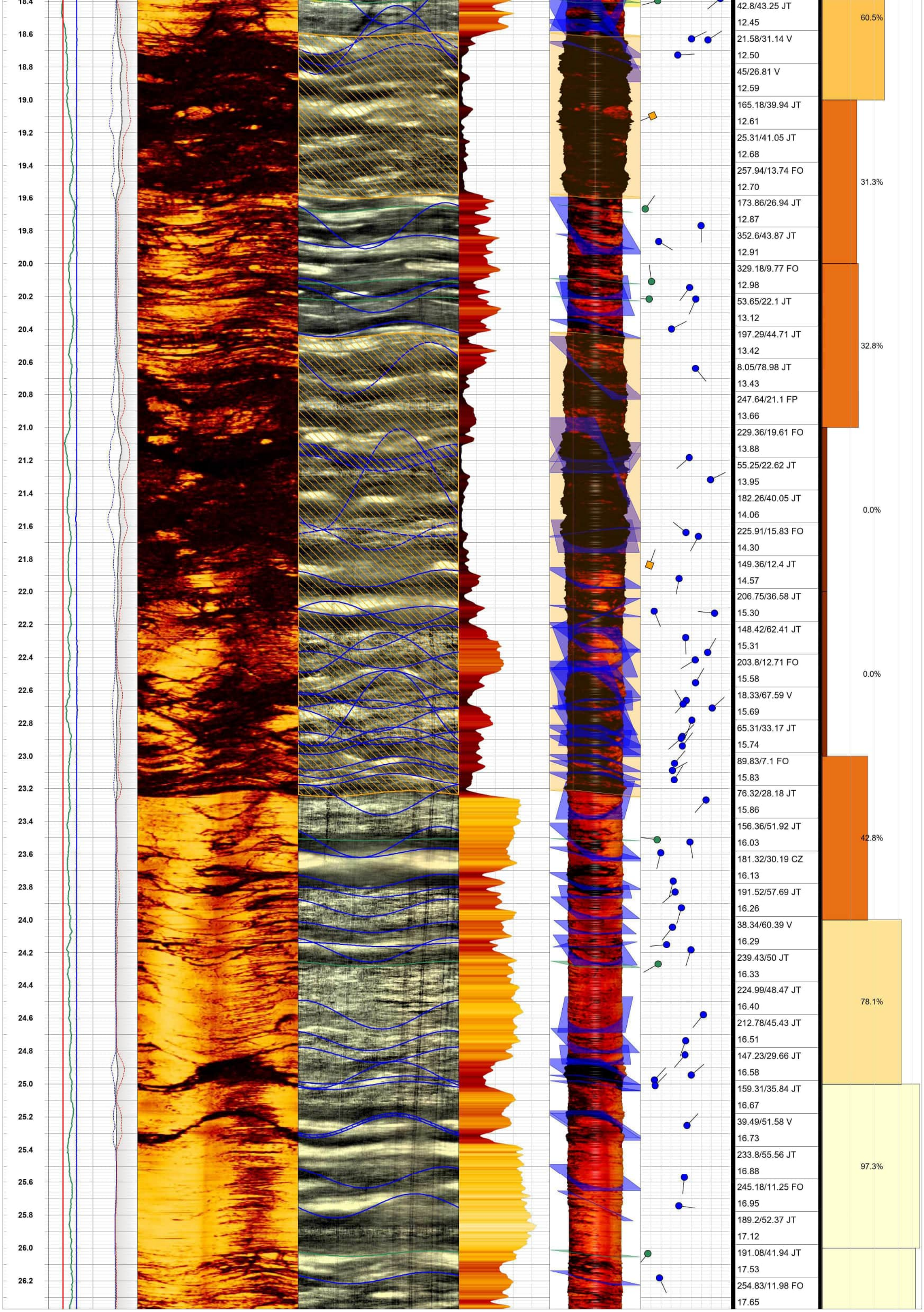
Curve Description:

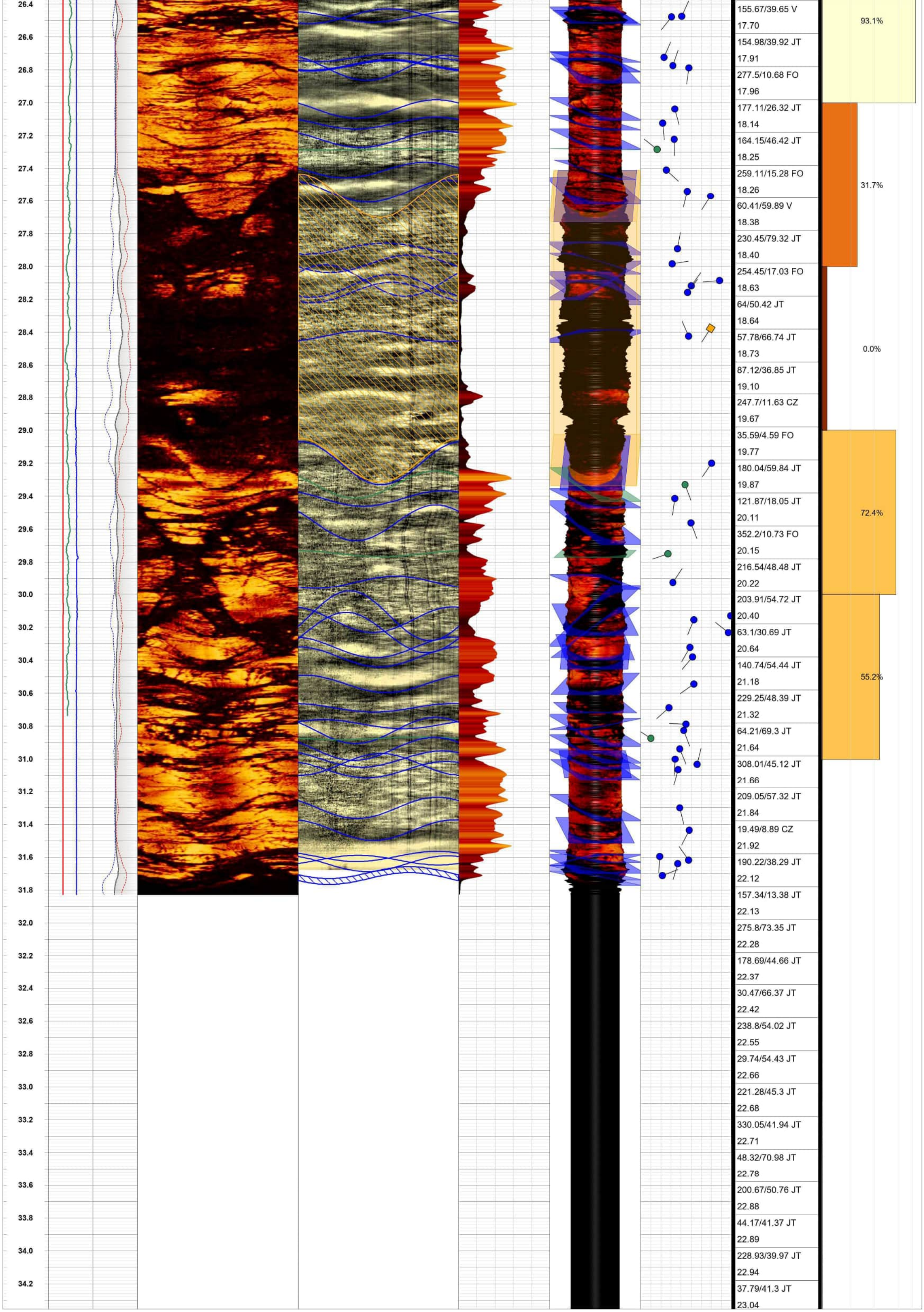
Title	Description	Top [m]	Base [m]	Tool s/n	Run / Date
Depth	Measured depth	0.4	31.8		
TVD	True vertical depth	0.4	31.8		
Tilt	Deviation from the vertical	0.4	31.8		
AZIM (TN)	Deviation from True North	0.4	31.8		
GR	Natural gamma ray	0.7	30.7	ABI/GR 220402	Run 2 & 3, 14/02/2026
Caliper	Borehole diameter from ATV traveltime, average, minimum, and maximum	1.8	31.8		
Apparent Picks	Uncorrected structure picks from ATV and OTV images	0.4	31.8		
ATV	ATV amplitude image (MN)	1.8	31.8	ABI/GR 220402	Run 2 & 3, 14/02/2026
OTV	OTV image (MN)	0.4	31.6	OBI 22204	Run 4, 14/02/2026
Reflectivity	Acoustic reflectivity of the rock	1.8	31.8		
Corrected Picks	Structure picks correxcted for borehole deviation (TN)	0.4	31.8		
Pick Discription	Structural pick discription, woth Azimuth, Dip Magnitude, and Type (TN)	0.4	31.8		
Pseudo Core	3D poresentation of ATV amp;litude, borehole radius and apparent picks	1.9	31.8		
RQD	Rock Quality Designation	1	31		




2.51
25.63/32.08 JT
94.1%
100.0%
4.04
83.82/22.55 JT
4.31
273.25/47.98 JT
4.50
116.25/23.61 JT
4.58
37.22/3.23 FO
4.81
318.81/10.66 FO
5.18
353.6/2.54 FO
5.20
164.44/46.56 JT
5.31
158.69/12.79 JT
5.38
170.77/32.67 JT
5.44
131.95/59.88 JT
5.49
147.23/39.31 JT
5.54
136.1/31.68 JT
5.60
146.49/37.59 JT
5.80
153.13/15 JT
5.91
289.33/21.04 CZ
6.05
140.8/32.22 JT
6.18
78.59/5.88 FO
6.30
121.19/19.25 JT
6.34
133.65/18.09 JT
6.42
16.75/37.54 JT
6.49
93.39/13.81 JT
6.53
295.36/43.98 JT
6.57
130.7/21.56 JT
6.69
125.66/11.51 JT
6.74
147.33/87.53 JT
6.81
292.76/15.12 FO
6.84
157.83/33.17 JT
6.85
258.91/13.71 FO
6.98
214.72/37.28 JT
7.07
317.65/6.71 FO
7.17
143.69/26.66 JT
7.24
96.0%
30.1%
46.4%
78.4%
78.4%
90.5%
2.6
2.8
3.0
3.2
3.4
3.6
3.8
4.0
4.2
4.4
4.6
4.8
5.0
5.2
5.4
5.6
5.8
6.0
6.2
6.4
6.6
6.8
7.0
7.2
7.4
7.6
7.8
8.0
8.2
8.4
8.6
8.8
9.0
9.2
9.4
9.6
9.8
10.0
10.2
10.4


10.6
10.8
11.0
11.2
11.4
11.6
11.8
12.0
12.2
12.4
12.6
12.8
13.0
13.2
13.4
13.6
13.8
14.0
14.2
14.4
14.6
14.8
15.0
15.2
15.4
15.6
15.8
16.0
16.2
16.4
16.6
16.8
17.0
17.2
17.4
17.6
17.8
18.0
18.2
67.66/23.18 JT
7.30
110.6/26.52 JT
7.35
87.63/18.97 JT
7.38
223.65/58.14 JT
7.57
39.72/25.03 JT
7.99
273.34/19.15 FO
8.19
148.91/35.34 JT
8.44
30.41/63.23 JT
8.52
299.94/8.54 FO
8.53
47.36/39.64 JT
8.61
137.19/29.57 JT
8.64
209.63/26.61 JT
8.75
172.54/22.07 JT
8.86
140.79/27.29 JT
9.15
50.21/22.33 JT
9.20
342.99/15.77 FO
9.28
141.2/42.83 JT
9.66
33.78/52.16 JT
9.75
168.64/33.86 JT
9.86
303.16/13.81 FO
10.11
43.11/34.71 JT
10.21
190.22/24.67 JT
10.40
216.66/21.85 JT
10.46
192.13/35.66 JT
10.50
332.7/28.97 JT
10.66
174.29/34 JT
10.83
185.01/33.84 JT
11.15
67.46/55.86 JT
11.20
9.48/49.07 JT
11.21
171.62/55.16 JT
11.29
335.44/47.2 JT
11.36
179.06/34.86 JT
11.47
67.68/60.91 JT
11.57
269.65/10.39 FO
11.85
41.93/68.26 V
11.96
21.63/52.26 V
12.05
172.8/65.21 JT
12.12
46.48/50.98 V
12.20
87.47/21.27 JT
12.29
172.29/48.76 JT
12.33
84.3%
78.1%
70.3%
88.1%
99.0%
94.8%
63.9%
95.9%


18.4
18.6
18.8
19.0
19.2
19.4
19.6
19.8
20.0
20.2
20.4
20.6
20.8
21.0
21.2
21.4
21.6
21.8
22.0
22.2
22.4
22.6
22.8
23.0
23.2
23.4
23.6
23.8
24.0
24.2
24.4
24.6
24.8
25.0
25.2
25.4
25.6
25.8
26.0
26.2
42.8/43.25 JT
12.45
21.58/31.14 V
12.50
45/26.81 V
12.59
165.18/39.94 JT
12.61
25.31/41.05 JT
12.68
257.94/13.74 FO
12.70
173.86/26.94 JT
12.87
352.6/43.87 JT
12.91
329.18/9.77 FO
12.98
53.65/22.1 JT
13.12
197.29/44.71 JT
13.42
8.05/78.98 JT
13.43
247.64/21.1 FP
13.66
229.36/19.61 FO
13.88
55.25/22.62 JT
13.95
182.26/40.05 JT
14.06
225.91/15.83 FO
14.30
149.36/12.4 JT
14.57
206.75/36.58 JT
15.30
148.42/62.41 JT
15.31
203.8/12.71 FO
15.58
18.33/67.59 V
15.69
65.31/33.17 JT
15.74
89.83/7.1 FO
15.83
76.32/28.18 JT
15.86
156.36/51.92 JT
16.03
181.32/30.19 CZ
16.13
191.52/57.69 JT
16.26
38.34/60.39 V
16.29
239.43/50 JT
16.33
224.99/48.47 JT
16.40
212.78/45.43 JT
16.51
147.23/29.66 JT
16.58
159.31/35.84 JT
16.67
39.49/51.58 V
16.73
233.8/55.56 JT
16.88
245.18/11.25 FO
16.95
189.2/52.37 JT
17.12
191.08/41.94 JT
17.53
254.83/11.98 FO
17.65
60.5%
31.3%
32.8%
0.0%
0.0%
42.8%
78.1%
97.3%


26.4
26.6
26.8
27.0
27.2
27.4
27.6
27.8
28.0
28.2
28.4
28.6
28.8
29.0
29.2
29.4
29.6
29.8
30.0
30.2
30.4
30.6
30.8
31.0
31.2
31.4
31.6
31.8
32.0
32.2
32.4
32.6
32.8
33.0
33.2
33.4
33.6
33.8
34.0
34.2
155.67/39.65 V
17.70
154.98/39.92 JT
17.91
277.5/10.68 FO
17.96
177.11/26.32 JT
18.14
164.15/46.42 JT
18.25
259.11/15.28 FO
18.26
60.41/59.89 V
18.38
230.45/79.32 JT
18.40
254.45/17.03 FO
18.63
64/50.42 JT
18.64
57.78/66.74 JT
18.73
87.12/36.85 JT
19.10
247.7/11.63 CZ
19.67
35.59/4.59 FO
19.77
180.04/59.84 JT
19.87
121.87/18.05 JT
20.11
352.2/10.73 FO
20.15
216.54/48.48 JT
20.22
203.91/54.72 JT
20.40
63.1/30.69 JT
20.64
140.74/54.44 JT
21.18
229.25/48.39 JT
21.32
64.21/69.3 JT
21.64
308.01/45.12 JT
21.66
209.05/57.32 JT
21.84
19.49/8.89 CZ
21.92
190.22/38.29 JT
22.12
157.34/13.38 JT
22.13
275.8/73.35 JT
22.28
178.69/44.66 JT
22.37
30.47/66.37 JT
22.42
238.8/54.02 JT
22.55
29.74/54.43 JT
22.66
221.28/45.3 JT
22.68
330.05/41.94 JT
22.71
48.32/70.98 JT
22.78
200.67/50.76 JT
22.88
44.17/41.37 JT
22.89
228.93/39.97 JT
22.94
37.79/41.3 JT
23.04
93.1%
31.7%
0.0%
72.4%
55.2%

34.4	40.31/33.68 JT
	23.09
34.6	61.08/31.49 JT
	23.14
34.8	30.91/33.15 JT
	23.27
35.0	220.57/64.8 JT
	23.51
35.2	277.9/16.26 FO
	23.53
35.4	169.92/48.83 JT
	23.59
35.6	194.37/19.76 JT
	23.76
35.8	194.22/32.24 JT
	23.83
36.0	228.8/34.37 JT
	23.93
36.2	196.73/40.29 JT
	24.04
36.4	217.91/31.65 JT
	24.15
36.6	264.41/25.81 JT
	24.18
36.8	197.74/50.02 JT
	24.27
37.0	240.63/17.18 FO
	24.58
37.2	219.27/62.13 JT
	24.74
37.4	199.35/44.67 JT
	24.82
37.6	220.25/44.15 JT
	24.95
37.8	50.02/50.14 JT
	24.98
38.0	42.24/13.72 JT
	25.01
38.2	44.44/14.24 JT
	25.25
38.4	43.58/46.1 JT
	25.57
38.6	185.66/43.36 JT
	25.74
38.8	98.47/37.97 JT
	26.03
39.0	219.58/7.15 FO
	26.18
39.2	154.63/18.43 JT
	26.47
39.4	24.3/40.89 JT
	26.48
39.6	218.59/30.79 JT
	26.72
39.8	23.97/23.29 JT
	26.77
40.0	18.42/31.92 JT
	26.79
40.2	188.37/48.03 JT
	27.04
40.4	164.85/33.91 JT
	27.12
40.6	173.9/21.94 JT
	27.22
40.8	178.91/33.38 JT
	27.28
41.0	308.36/16.18 FO
	27.41
41.2	132.37/25.31 JT
	27.54
41.4	193.86/46.3 JT
	27.57
41.6	212.74/69.45 JT
	27.89
41.8	10.02/36.47 JT
	27.98
42.0	81.14/31.33 JT
	28.09
42.2	265.92/78.36 JT
	28.12

Corrected Picks	Pick Discription
36.03/50.2 JT	
28.16	
36.5/46.54 JT	
28.38	
212.3/69.42 CZ	
28.42	
335.93/47.56 JT	
29.20	
214.54/70.28 JT	
29.33	
159.48/44.15 FO	
29.41	
188.03/33.76 JT	
29.56	
158.45/50.05 JT	
29.75	
251.75/27.18 FO	
29.92	
33.66/31.85 JT	
30.13	
136.51/89.48 JT	
30.15	
202.78/52.84 JT	
30.23	
308.67/87.08 JT	
30.32	
209.82/49.07 JT	
30.38	
219.96/51.47 JT	
30.54	
234.18/52.86 JT	
30.69	
228.22/28.16 JT	
30.79	
271.73/44.95 JT	
30.83	
159.3/42.79 JT	
30.87	
302.55/10.27 FO	
30.94	
157.24/38.77 JT	
31.00	
183.57/34.09 JT	
31.03	
13.98/56.07 JT	
31.06	
195.2/37.23 JT	
31.30	
166.58/38.65 JT	
31.44	
206.77/48.18 JT	
31.60	
183.16/18.94 JT	
31.62	
324.9/47.47 JT	
31.64	
196.8/36.93 JT	
31.71	
68.85/21.53 JT	

1m:20m

Depth

0 deg 30 — TILT

0 250 — GR

0 360 — AZIM (TN)

70 170 — Caliper-min

70 170 — Caliper-max

70 170 — Caliper-ave

0° 90° 180° 270° 0° — 50 20000 — ATV Amplitude-NM

0° 90° 180° 270° 0° — OTV-NM

0° 90° 180° 270° 0° — (Magn. North) — Apparent Picks

0 10000 — Reflectivity

180° — Pseudo Core

0 90 — (True North) — Corrected Picks

Pick Discription

Very Poor | Poor | Fair | Good | Excellent — RQD

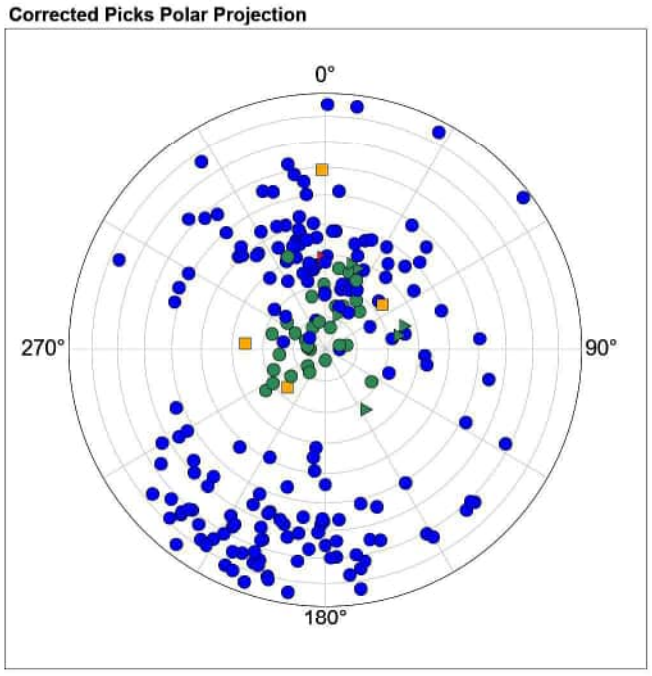
Well Name:	MDD506
Surveys:	ATV, GR
Location:	Bendigo
Company:	Santana

Service Company:	SPEIGHT DRILLING	**Log Measured From:**	Ground Level		
Operator:	Gareth Speight	**Drilling Measured From:**	Ground Level		
Date Logged:	24/02/2026	**Driller Depth:**	51.8	**Logger Depth:**	44.1
Drilling Company:	SPEIGHT DRILLING	**Inclination:**	-71°	**Heading:**	215° (TN)
Date Drilled:		**Easting:**		**Northing:**	
Field:		**Elevation:**		**Grid:**	True North (22.5°)
County / Township:		**Log Top:**	1.8	**Log Bottom:**	44.1
State / Province:					
Country:		**Depth unit:**	Meters	**Scale ratio:**	1 : 20

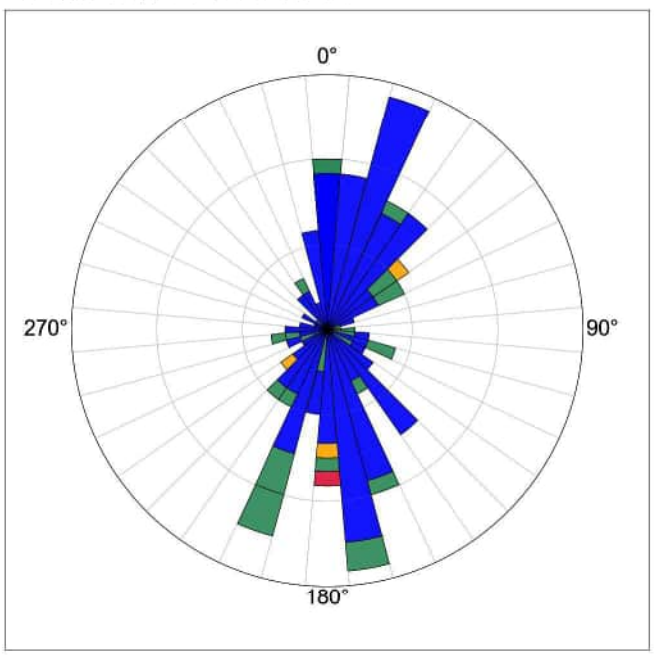
Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	51.8					
						Wireline Length:	Depth Factor:

Remarks:
Poor borehole conditions impacting structural interpretation confidence.

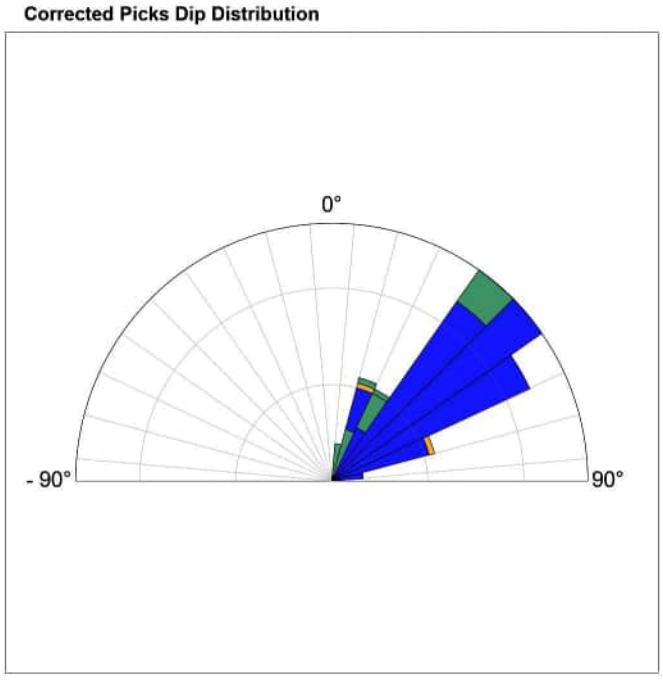
Corrected Picks Polar Projection



Corrected Picks Azimuth Distribution



Corrected Picks Dip Distribution

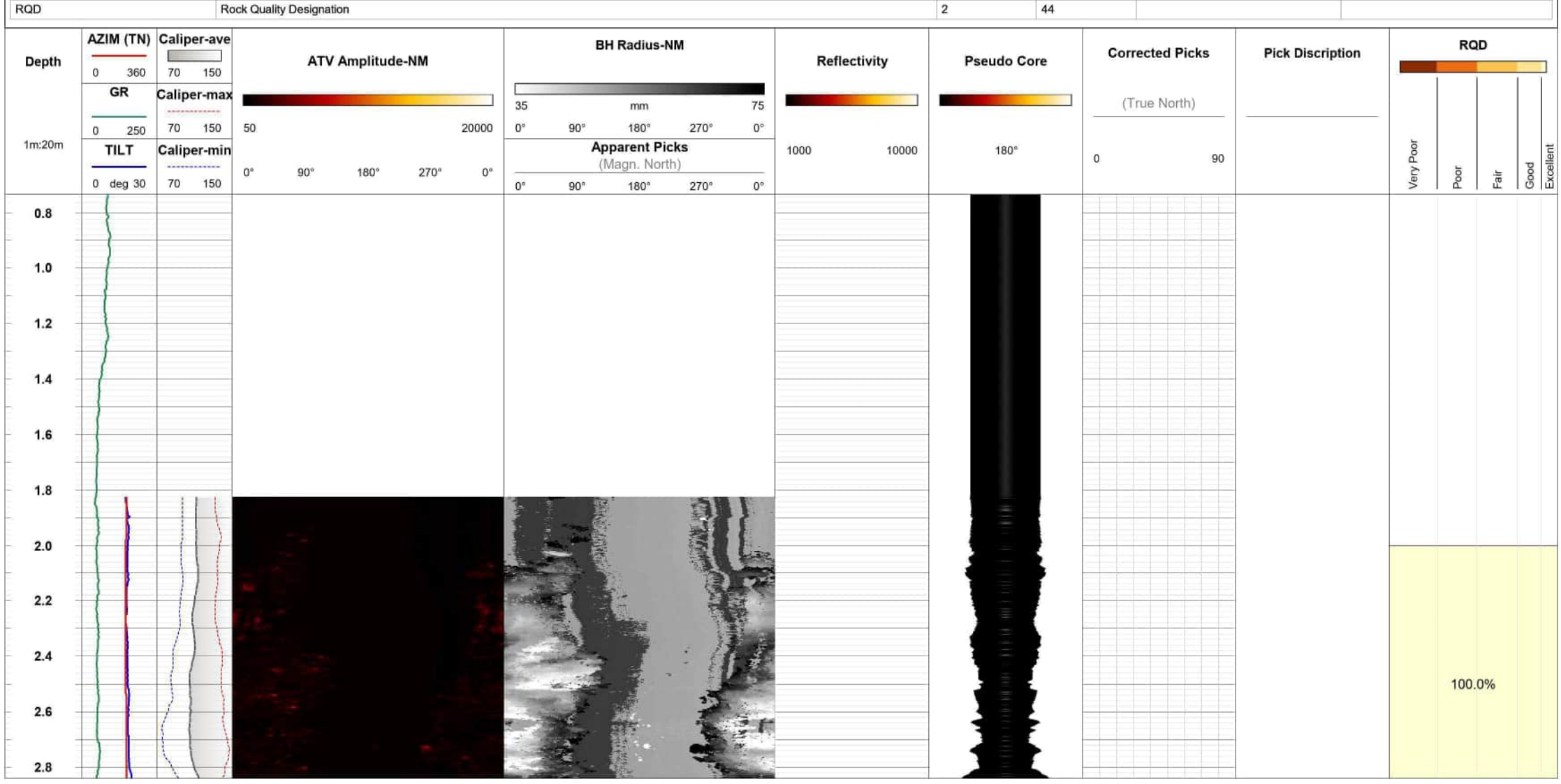


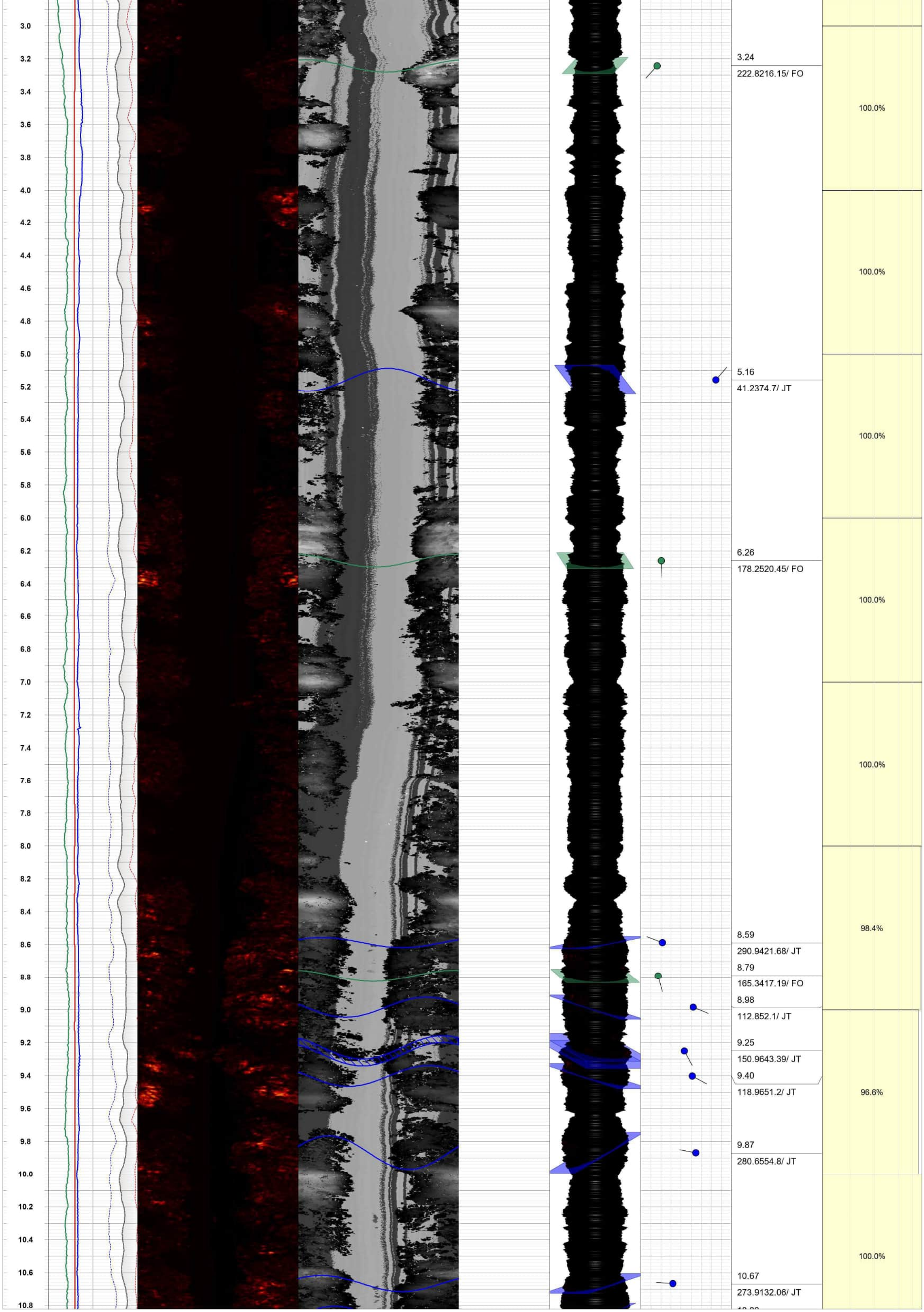
Legend:

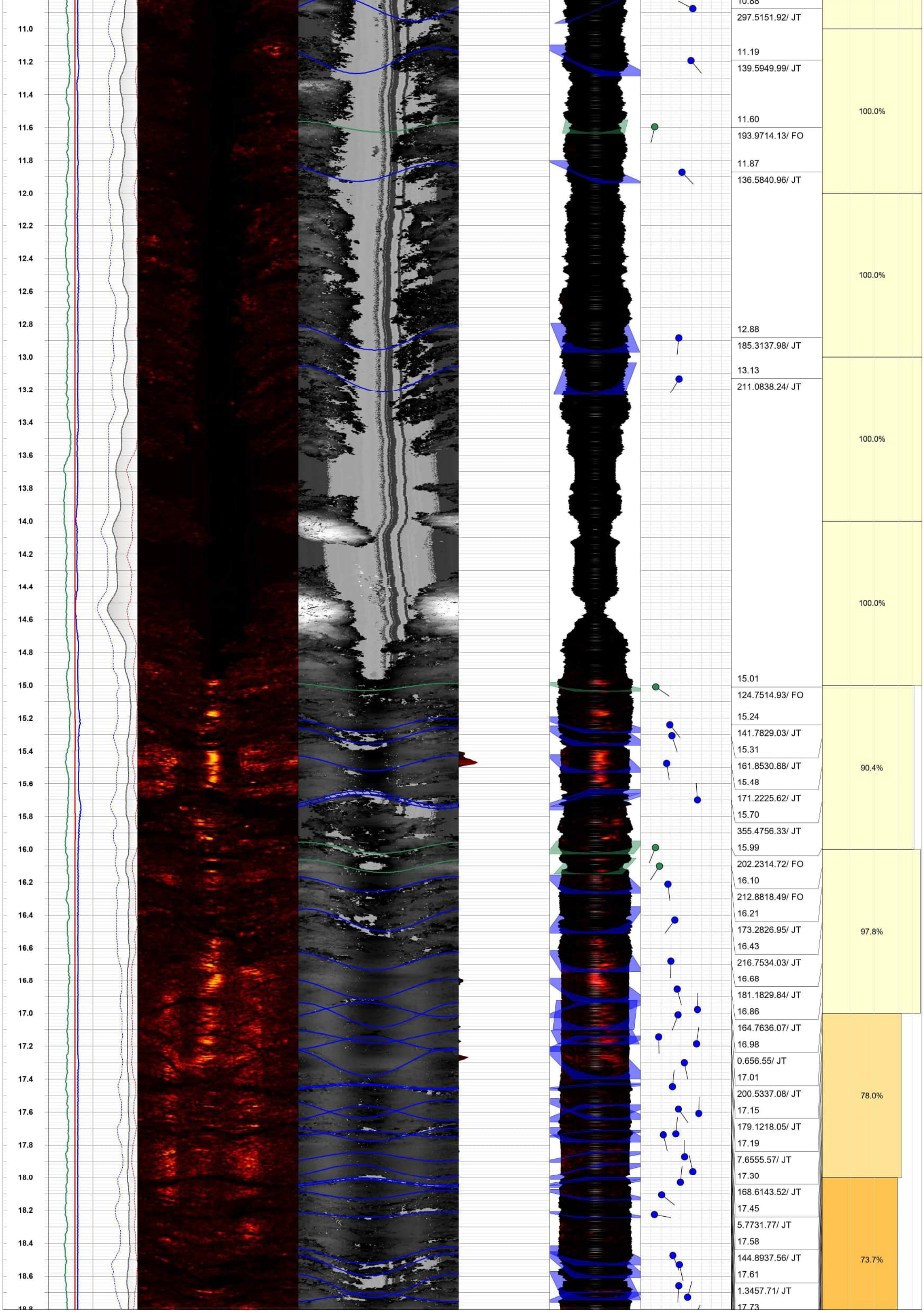
FO - Foliation | FP - Foliation Parting | JT - Joint | SH - Shear | CZ - Crushed Zone

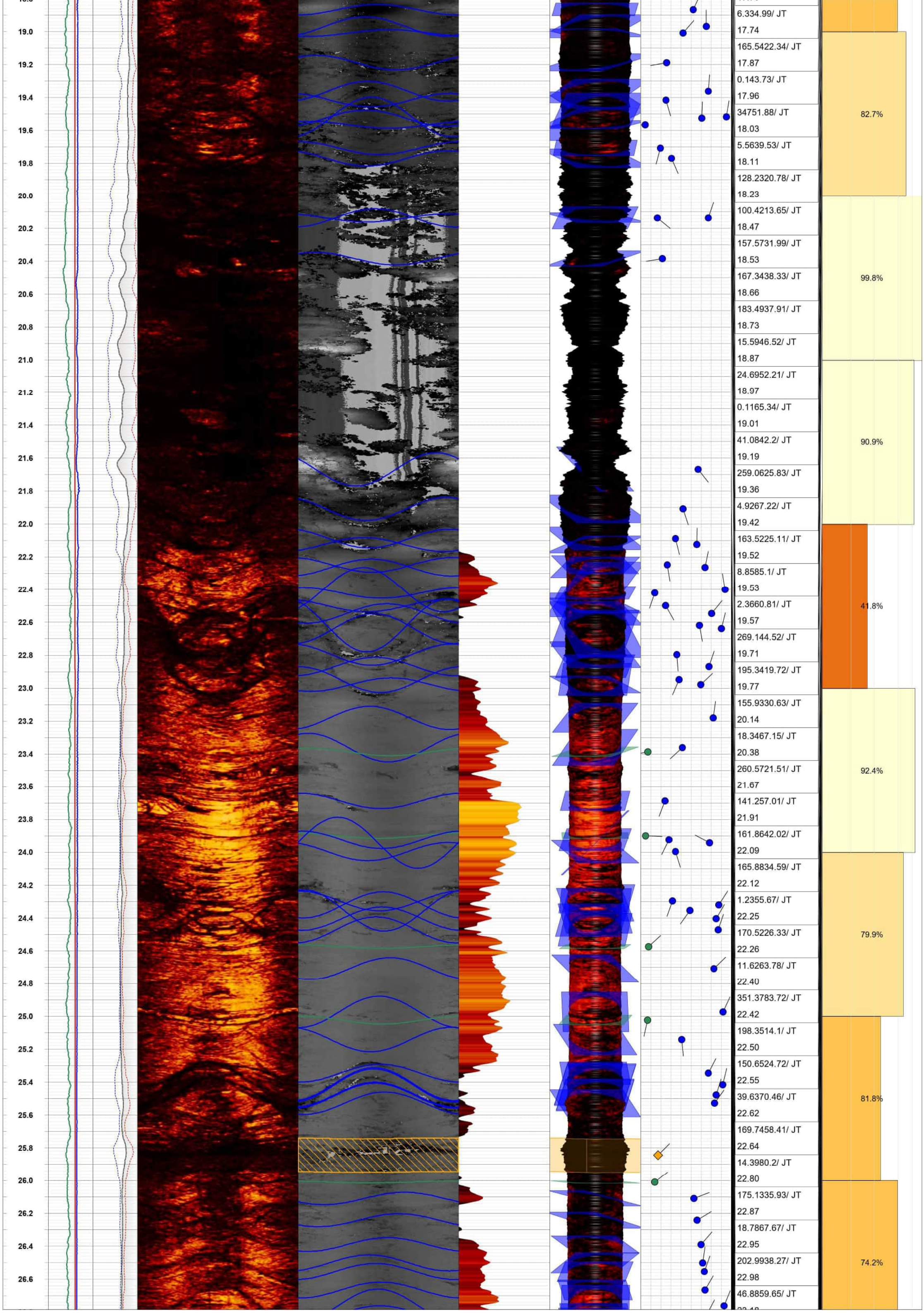
Curve Description:

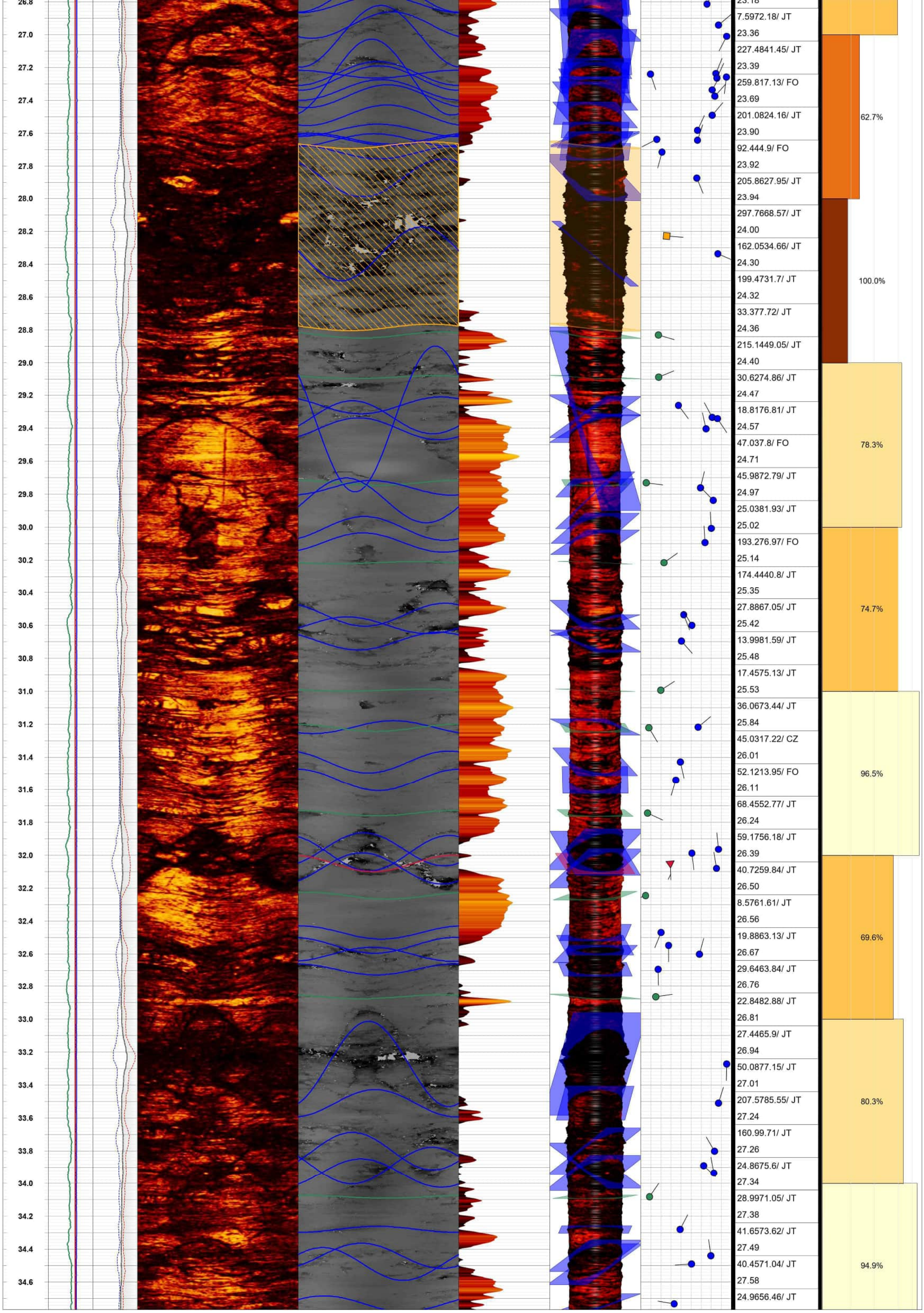
Title	Description	Top [m]	Base [m]	Tool s/n	Run / Date
Depth	Measured depth	1.8	44.1		
TVD	True vertical depth	1.8	44.1		
Tilt	Deviation from the vertical	1.8	44.1		
AZIM (TN)	Deviation from True North	1.8	44.1		
GR	Natural gamma ray	1	43	ABI/GR 220402	Run 4, 24/02/2026
Caliper	Borehole diameter from ATV traveltime, average, minimum, and maximum	1.8	44.1		
Apparent Picks	Uncorrected structure picks from ATV and OTV images	1.8	44.1		
ATV	ATV amplitude image (MN)	1.8	44.1	ABI/GR 220402	Run 4, 24/02/2026
OTV	OTV image (MN)	-	-		
Reflectivity	Acoustic reflectivity of the rock	1.8	44.1		
Corrected Picks	Structure picks correxcted for borehole deviation (TN)	1.8	44.1		
Pick Discription	Structural pick discription, woth Azimuth, Dip Magnitude, and Type (TN)	1.8	44.4		
Pseudo Core	3D poresentation of ATV amp;litude, borehole radius and apparent picks	1.8	44.1		
RQD	Rock Quality Designation	2	44		

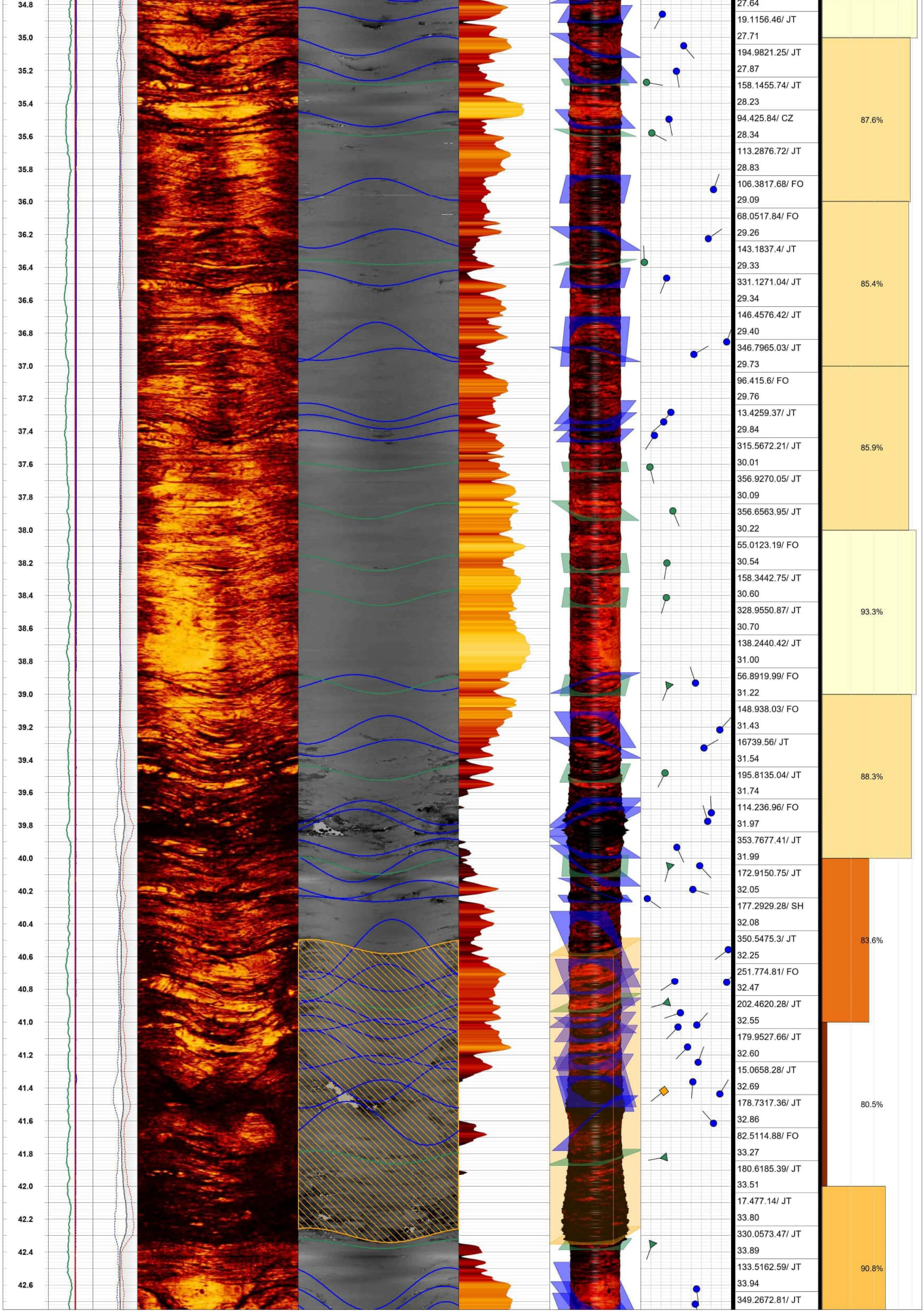


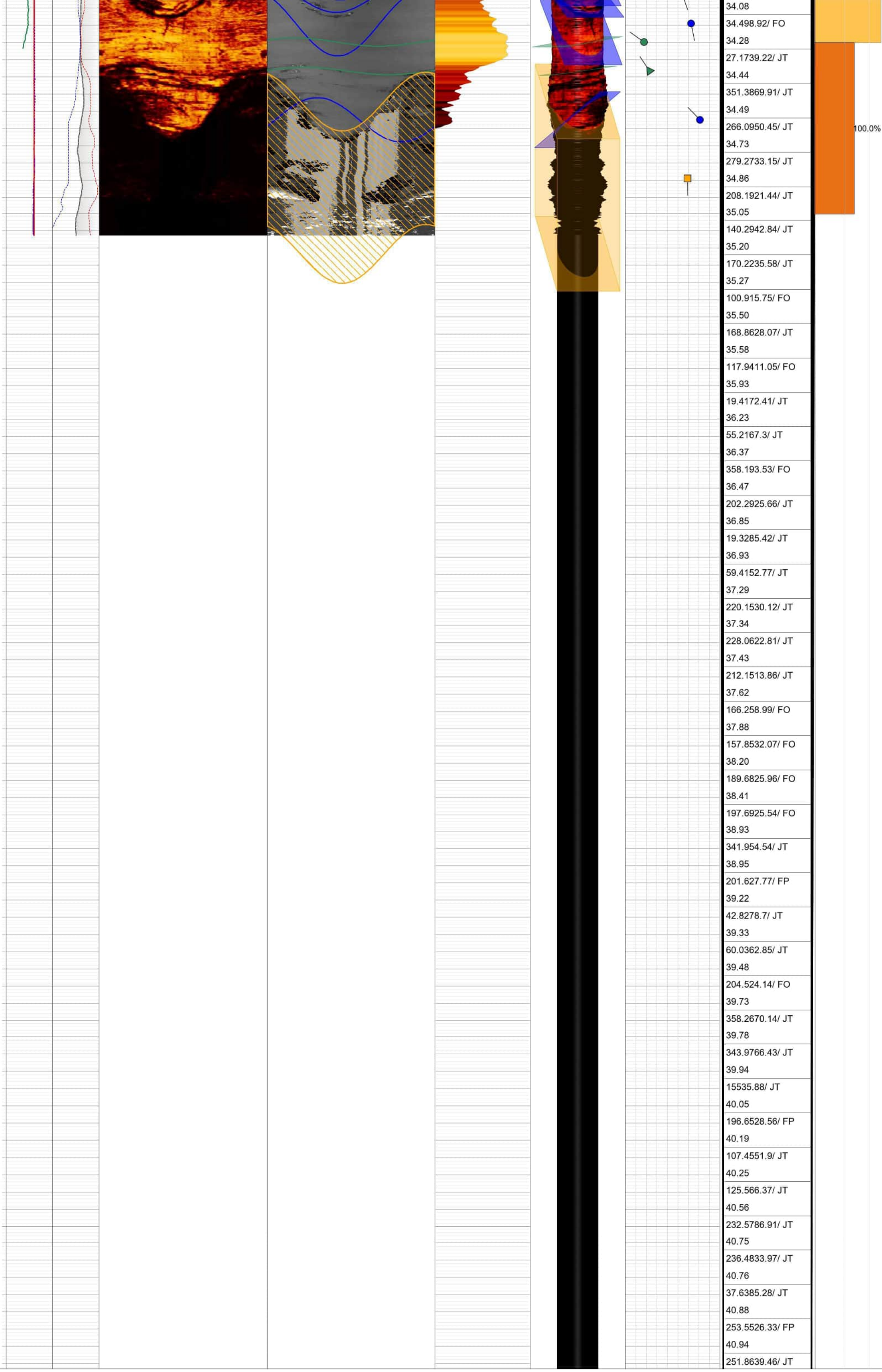

3.0
3.2
3.4
3.6
3.8
4.0
4.2
4.4
4.6
4.8
5.0
5.2
5.4
5.6
5.8
6.0
6.2
6.4
6.6
6.8
7.0
7.2
7.4
7.6
7.8
8.0
8.2
8.4
8.6
8.8
9.0
9.2
9.4
9.6
9.8
10.0
10.2
10.4
10.6
10.8
3.24
222.8216.15/ FO
100.0%
100.0%
5.16
41.2374.7/ JT
100.0%
6.26
178.2520.45/ FO
100.0%
98.4%
8.59
290.9421.68/ JT
8.79
165.3417.19/ FO
8.98
112.852.1/ JT
9.25
150.9643.39/ JT
9.40
118.9651.2/ JT
96.6%
9.87
280.6554.8/ JT
10.67
273.9132.06/ JT
100.0%


11.0
11.2
11.4
11.6
11.8
12.0
12.2
12.4
12.6
12.8
13.0
13.2
13.4
13.6
13.8
14.0
14.2
14.4
14.6
14.8
15.0
15.2
15.4
15.6
15.8
16.0
16.2
16.4
16.6
16.8
17.0
17.2
17.4
17.6
17.8
18.0
18.2
18.4
18.6
18.8
10.88
297.5151.92/ JT
11.19
139.5949.99/ JT
11.60
193.9714.13/ FO
11.87
136.5840.96/ JT
12.88
185.3137.98/ JT
13.13
211.0838.24/ JT
100.0%
100.0%
100.0%
15.01
124.7514.93/ FO
15.24
141.7829.03/ JT
15.31
161.8530.88/ JT
15.48
171.2225.62/ JT
15.70
355.4756.33/ JT
15.99
202.2314.72/ FO
16.10
212.8818.49/ FO
16.21
173.2826.95/ JT
16.43
216.7534.03/ JT
16.68
181.1829.84/ JT
16.86
164.7636.07/ JT
16.98
0.656.55/ JT
17.01
200.5337.08/ JT
17.15
179.1218.05/ JT
17.19
7.6555.57/ JT
17.30
168.6143.52/ JT
17.45
5.7731.77/ JT
17.58
144.8937.56/ JT
17.61
1.3457.71/ JT
17.73
90.4%
97.8%
78.0%
73.7%


19.0
19.2
19.4
19.6
19.8
20.0
20.2
20.4
20.6
20.8
21.0
21.2
21.4
21.6
21.8
22.0
22.2
22.4
22.6
22.8
23.0
23.2
23.4
23.6
23.8
24.0
24.2
24.4
24.6
24.8
25.0
25.2
25.4
25.6
25.8
26.0
26.2
26.4
26.6
6.334.99/ JT
17.74
165.5422.34/ JT
17.87
0.143.73/ JT
17.96
34751.88/ JT
18.03
5.5639.53/ JT
18.11
128.2320.78/ JT
18.23
100.4213.65/ JT
18.47
157.5731.99/ JT
18.53
167.3438.33/ JT
18.66
183.4937.91/ JT
18.73
15.5946.52/ JT
18.87
24.6952.21/ JT
18.97
0.1165.34/ JT
19.01
41.0842.2/ JT
19.19
259.0625.83/ JT
19.36
4.9267.22/ JT
19.42
163.5225.11/ JT
19.52
8.8585.1/ JT
19.53
2.3660.81/ JT
19.57
269.144.52/ JT
19.71
195.3419.72/ JT
19.77
155.9330.63/ JT
20.14
18.3467.15/ JT
20.38
260.5721.51/ JT
21.67
141.257.01/ JT
21.91
161.8642.02/ JT
22.09
165.8834.59/ JT
22.12
1.2355.67/ JT
22.25
170.5226.33/ JT
22.26
11.6263.78/ JT
22.40
351.3783.72/ JT
22.42
198.3514.1/ JT
22.50
150.6524.72/ JT
22.55
39.6370.46/ JT
22.62
169.7458.41/ JT
22.64
14.3980.2/ JT
22.80
175.1335.93/ JT
22.87
18.7867.67/ JT
22.95
202.9938.27/ JT
22.98
46.8859.65/ JT
82.7%
99.8%
90.9%
41.8%
92.4%
79.9%
81.8%
74.2%


26.8
27.0
27.2
27.4
27.6
27.8
28.0
28.2
28.4
28.6
28.8
29.0
29.2
29.4
29.6
29.8
30.0
30.2
30.4
30.6
30.8
31.0
31.2
31.4
31.6
31.8
32.0
32.2
32.4
32.6
32.8
33.0
33.2
33.4
33.6
33.8
34.0
34.2
34.4
34.6
23.18
7.5972.18/ JT
23.36
227.4841.45/ JT
23.39
259.817.13/ FO
23.69
201.0824.16/ JT
23.90
92.444.9/ FO
23.92
205.8627.95/ JT
23.94
297.7668.57/ JT
24.00
162.0534.66/ JT
24.30
199.4731.7/ JT
24.32
33.377.72/ JT
24.36
215.1449.05/ JT
24.40
30.6274.86/ JT
24.47
18.8176.81/ JT
24.57
47.037.8/ FO
24.71
45.9872.79/ JT
24.97
25.0381.93/ JT
25.02
193.276.97/ FO
25.14
174.4440.8/ JT
25.35
27.8867.05/ JT
25.42
13.9981.59/ JT
25.48
17.4575.13/ JT
25.53
36.0673.44/ JT
25.84
45.0317.22/ CZ
26.01
52.1213.95/ FO
26.11
68.4552.77/ JT
26.24
59.1756.18/ JT
26.39
40.7259.84/ JT
26.50
8.5761.61/ JT
26.56
19.8863.13/ JT
26.67
29.6463.84/ JT
26.76
22.8482.88/ JT
26.81
27.4465.9/ JT
26.94
50.0877.15/ JT
27.01
207.5785.55/ JT
27.24
160.99.71/ JT
27.26
24.8675.6/ JT
27.34
28.9971.05/ JT
27.38
41.6573.62/ JT
27.49
40.4571.04/ JT
27.58
24.9656.46/ JT
62.7%
100.0%
78.3%
74.7%
96.5%
69.6%
80.3%
94.9%


34.8
35.0
35.2
35.4
35.6
35.8
36.0
36.2
36.4
36.6
36.8
37.0
37.2
37.4
37.6
37.8
38.0
38.2
38.4
38.6
38.8
39.0
39.2
39.4
39.6
39.8
40.0
40.2
40.4
40.6
40.8
41.0
41.2
41.4
41.6
41.8
42.0
42.2
42.4
42.6
27.64
19.1156.46/ JT
27.71
194.9821.25/ JT
27.87
158.1455.74/ JT
28.23
94.425.84/ CZ
28.34
113.2876.72/ JT
28.83
106.3817.68/ FO
29.09
68.0517.84/ FO
29.26
143.1837.4/ JT
29.33
331.1271.04/ JT
29.34
146.4576.42/ JT
29.40
346.7965.03/ JT
29.73
96.415.6/ FO
29.76
13.4259.37/ JT
29.84
315.5672.21/ JT
30.01
356.9270.05/ JT
30.09
356.6563.95/ JT
30.22
55.0123.19/ FO
30.54
158.3442.75/ JT
30.60
328.9550.87/ JT
30.70
138.2440.42/ JT
31.00
56.8919.99/ FO
31.22
148.938.03/ FO
31.43
16739.56/ JT
31.54
195.8135.04/ JT
31.74
114.236.96/ FO
31.97
353.7677.41/ JT
31.99
172.9150.75/ JT
32.05
177.2929.28/ SH
32.08
350.5475.3/ JT
32.25
251.774.81/ FO
32.47
202.4620.28/ JT
32.55
179.9527.66/ JT
32.60
15.0658.28/ JT
32.69
178.7317.36/ JT
32.86
82.5114.88/ FO
33.27
180.6185.39/ JT
33.51
17.477.14/ JT
33.80
330.0573.47/ JT
33.89
133.5162.59/ JT
33.94
349.2672.81/ JT
87.6%
85.4%
85.9%
93.3%
88.3%
83.6%
80.5%
90.8%


42.8
43.0
43.2
43.4
43.6
43.8
44.0
44.2
44.4
44.6
44.8
45.0
45.2
45.4
45.6
45.8
46.0
46.2
46.4
46.6
46.8
47.0
47.2
47.4
47.6
47.8
48.0
48.2
48.4
48.6
48.8
49.0
49.2
49.4
49.6
49.8
50.0
50.2
50.4
50.6
34.08
34.498.92/ FO
34.28
27.1739.22/ JT
34.44
351.3869.91/ JT
34.49
266.0950.45/ JT
34.73
279.2733.15/ JT
34.86
208.1921.44/ JT
35.05
140.2942.84/ JT
35.20
170.2235.58/ JT
35.27
100.915.75/ FO
35.50
168.8628.07/ JT
35.58
117.9411.05/ FO
35.93
19.4172.41/ JT
36.23
55.2167.3/ JT
36.37
358.193.53/ FO
36.47
202.2925.66/ JT
36.85
19.3285.42/ JT
36.93
59.4152.77/ JT
37.29
220.1530.12/ JT
37.34
228.0622.81/ JT
37.43
212.1513.86/ JT
37.62
166.258.99/ FO
37.88
157.8532.07/ FO
38.20
189.6825.96/ FO
38.41
197.6925.54/ FO
38.93
341.954.54/ JT
38.95
201.627.77/ FP
39.22
42.8278.7/ JT
39.33
60.0362.85/ JT
39.48
204.524.14/ FO
39.73
358.2670.14/ JT
39.78
343.9766.43/ JT
39.94
15535.88/ JT
40.05
196.6528.56/ FP
40.19
107.4551.9/ JT
40.25
125.566.37/ JT
40.56
232.5786.91/ JT
40.75
236.4833.97/ JT
40.76
37.6385.28/ JT
40.88
253.5526.33/ FP
40.94
251.8639.46/ JT
100.0%

Depth	TILT	GR	AZIM (TN)	Caliper-min	Caliper-max	Caliper-ave	ATV Amplitude-NM	BH Radius-NM	Reflectivity	Pseudo Core	Corrected Picks	Pick Discription	RQD
50.8												41.02	
51.0												41.4755.85/ JT 41.03	
51.2												223.7137.04/ JT 41.15	
51.4												224.7346.7/ JT 41.25	
51.6												19.3357.14/ JT 41.36	
51.8												184.9151.77/ JT 41.42	
52.0												232.123.27/ CZ 41.44	
52.2												31.4578.59/ JT 41.61	
52.4												318.572.44/ JT 41.82	
52.6												259.0523.74/ FP 42.35	
52.8												200.0211.42/ FP 42.63	
53.0												172.4755.38/ JT 42.72	
53.2												161.4554.17/ JT 42.89	
53.4												168.4962.72/ JT 43.00	
53.6												305.5618.03/ FO 43.17	
53.8												326.3523.18/ FP 43.45	
54.0												316.2371.19/ JT 43.79	
												178.6459.16/ CZ	
1m:20m	0 deg 30	0 250	0 360	70 150	70 150	70 150	0° 90° 180° 270° 0° 50 20000	0° 90° 180° 270° 0° (Magn. North) Apparent Picks 0° 90° 180° 270° 0° 35 mm 75	1000 10000	180°	0 90 (True North)		Very Poor Poor Fair Good Excellent

Well Name:	MDD515
Surveys:	ATV-GR & OTV
Location:	Bendigo
Company:	Santana

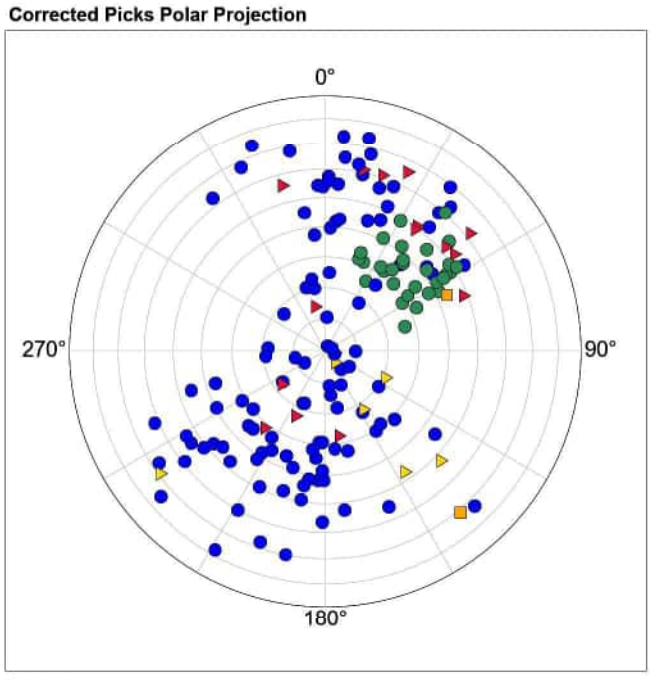
Service Company:	Speight Drilling
Operator:	Gareth Speight
Date Logged:	15/03/2026
Drilling Company:	Speight Drilling
Date Drilled:	
Field:	
County / Township:	
State / Province:	
Country:	

Log Measured From:	Ground Level		
Drilling Measured From:	Ground Level		
Driller Depth:	21	**Logger Depth:**	20.5
Inclination:	-88.5°	**Heading:**	027°(TN)
Easting:		**Northing:**	
Elevation:		**Grid:**	True North (22.5°)
Log Top:	0.4	**Log Bottom:**	20.5
Depth unit:	Metre (m)	**Scale ratio:**	1 : 10

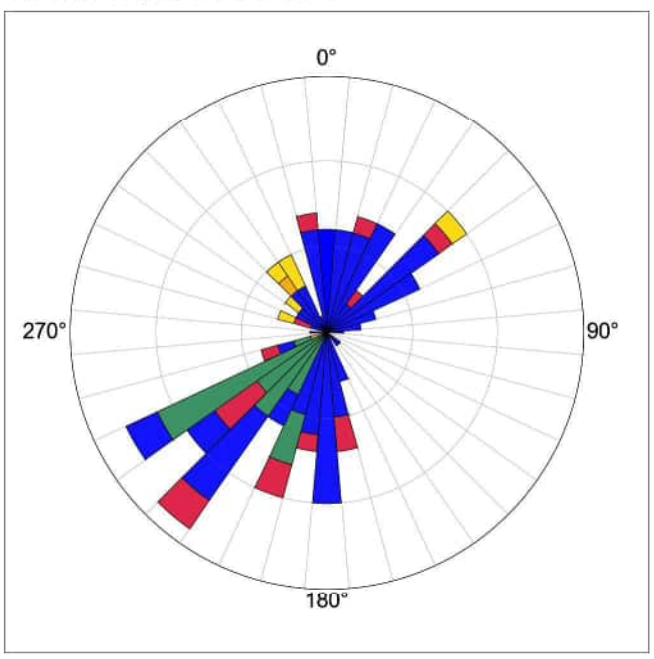
Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	21				334970	334G-042
						Wireline Length:	**Depth Factor:**
						1800	10501/1m

Remarks:

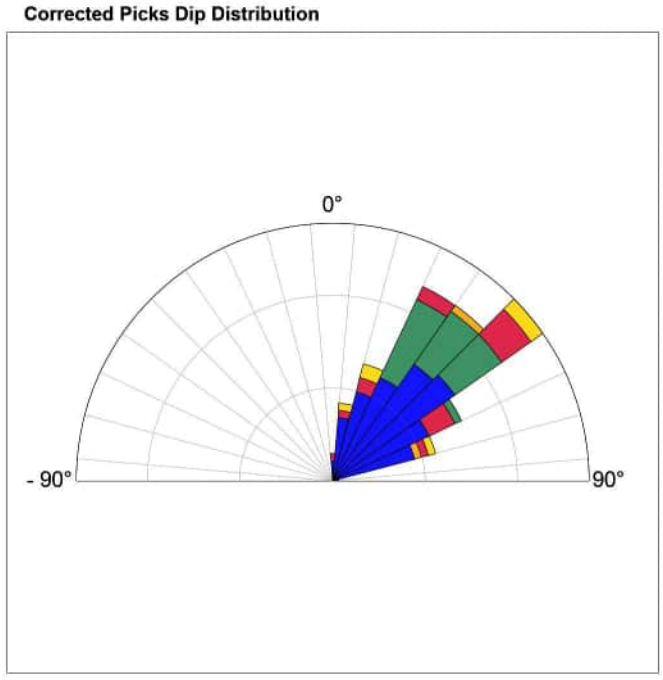
Corrected Picks Polar Projection



Corrected Picks Azimuth Distribution



Corrected Picks Dip Distribution

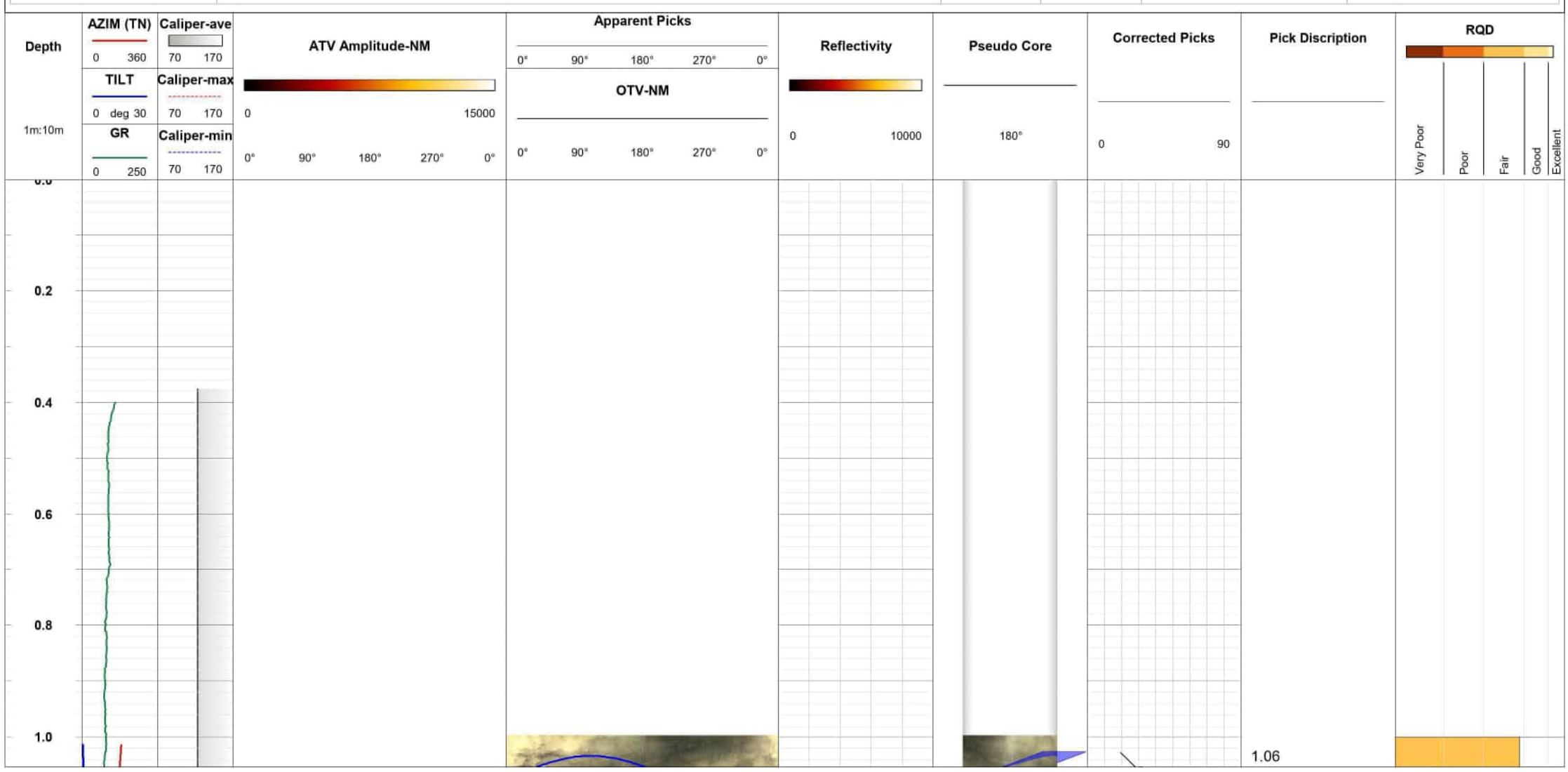


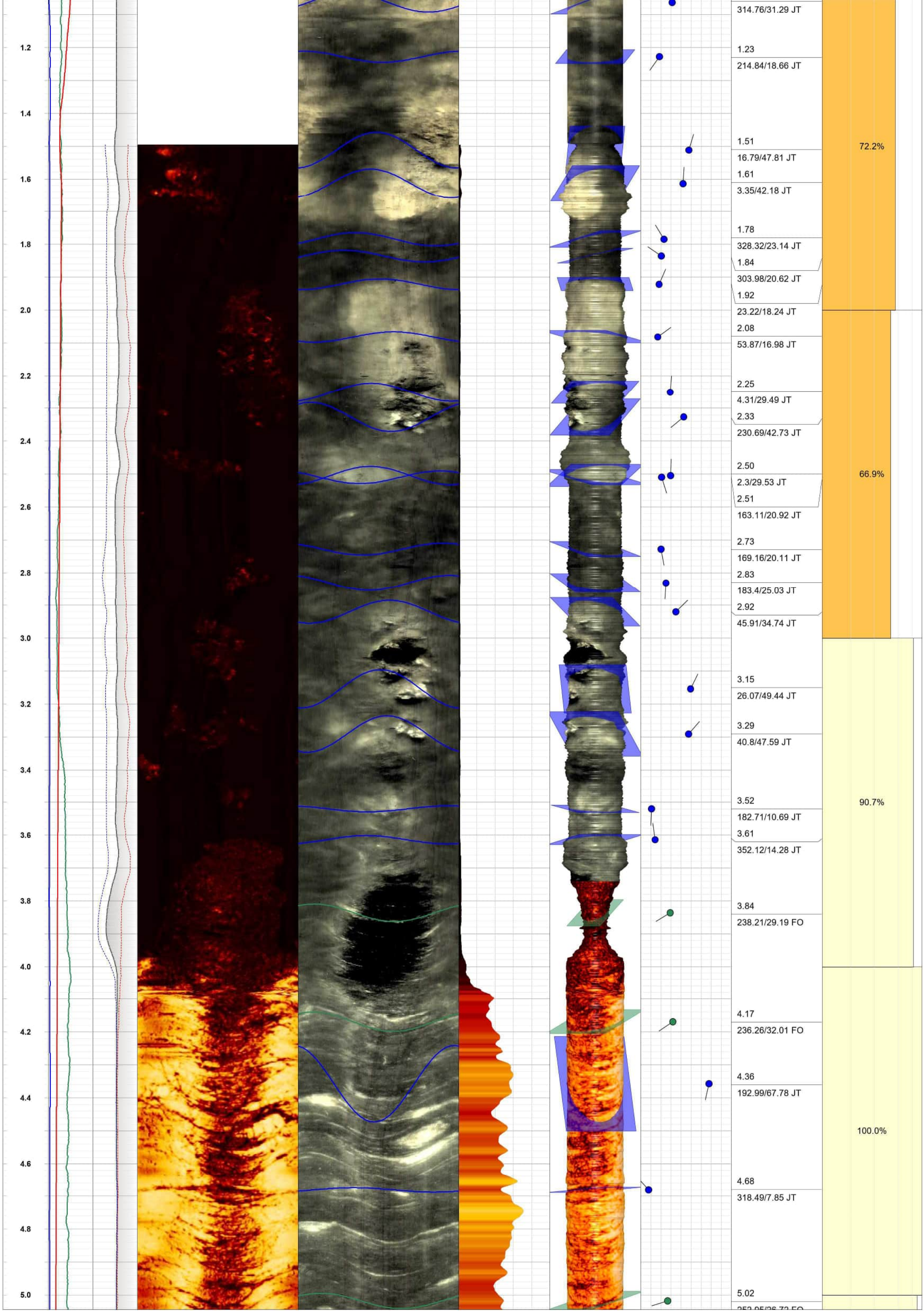
Legend:

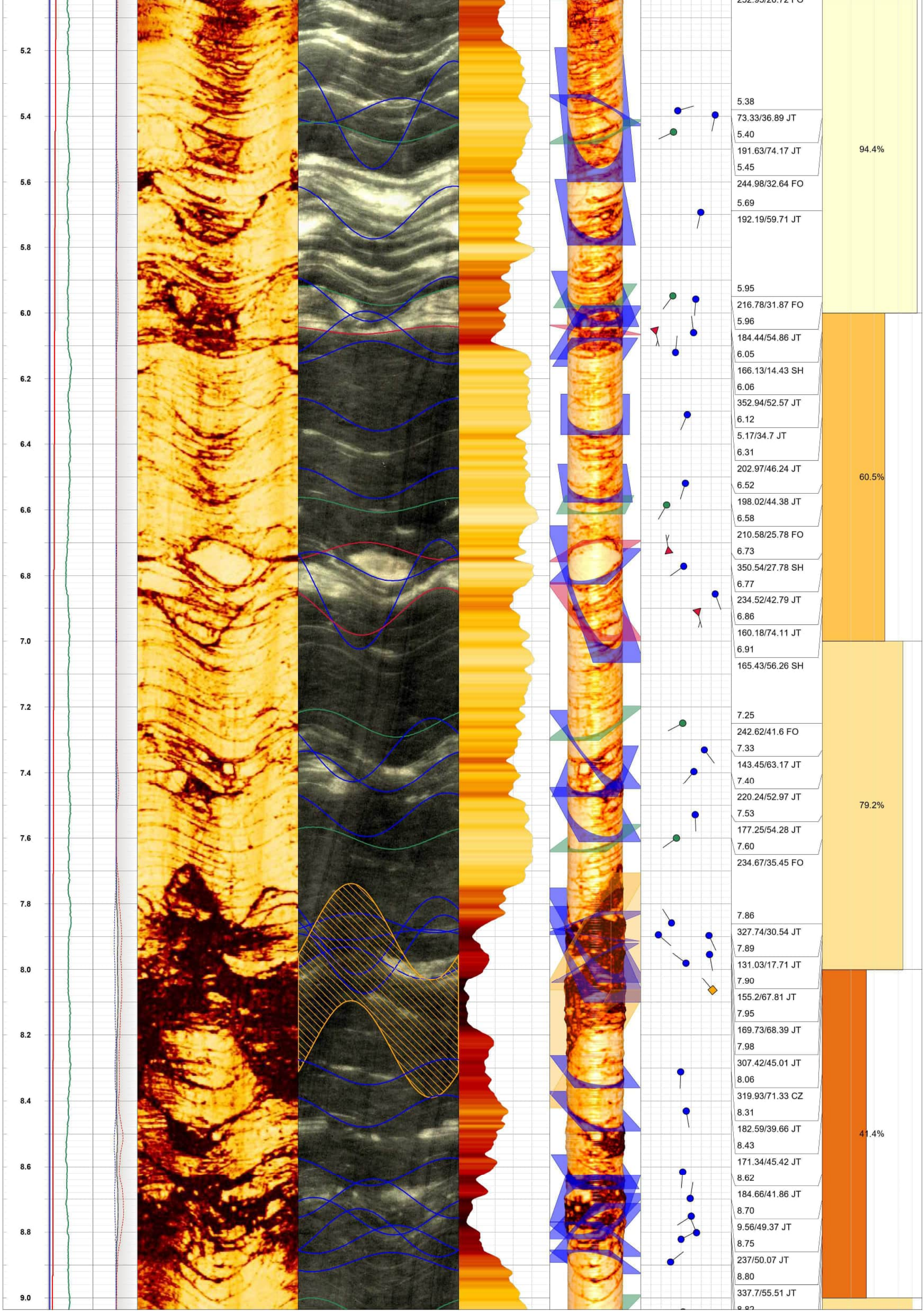
FO - Foliation | JT - Joint | SH - Shear | CZ - Crushed Zone | V - Vein

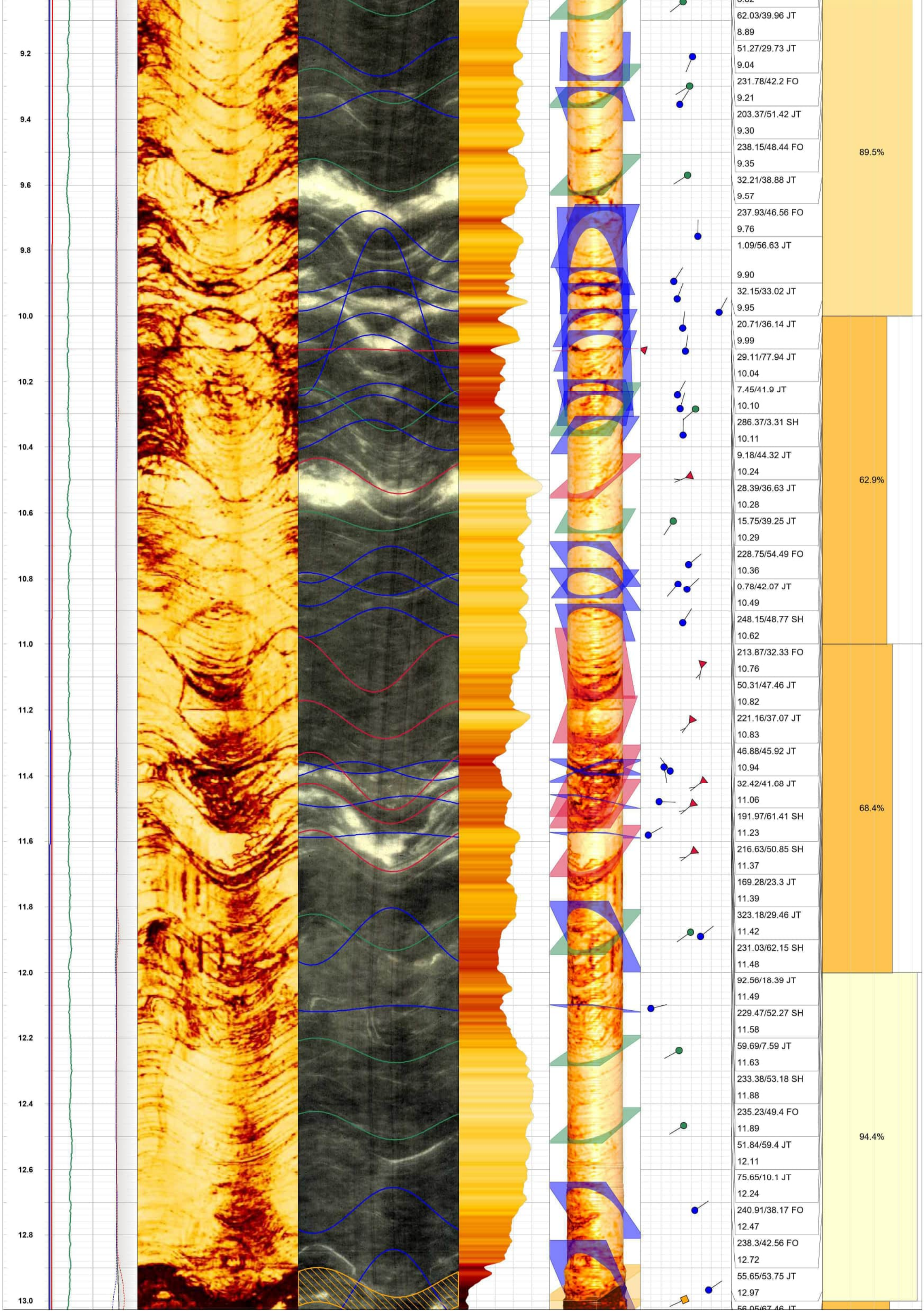
Curve Description:

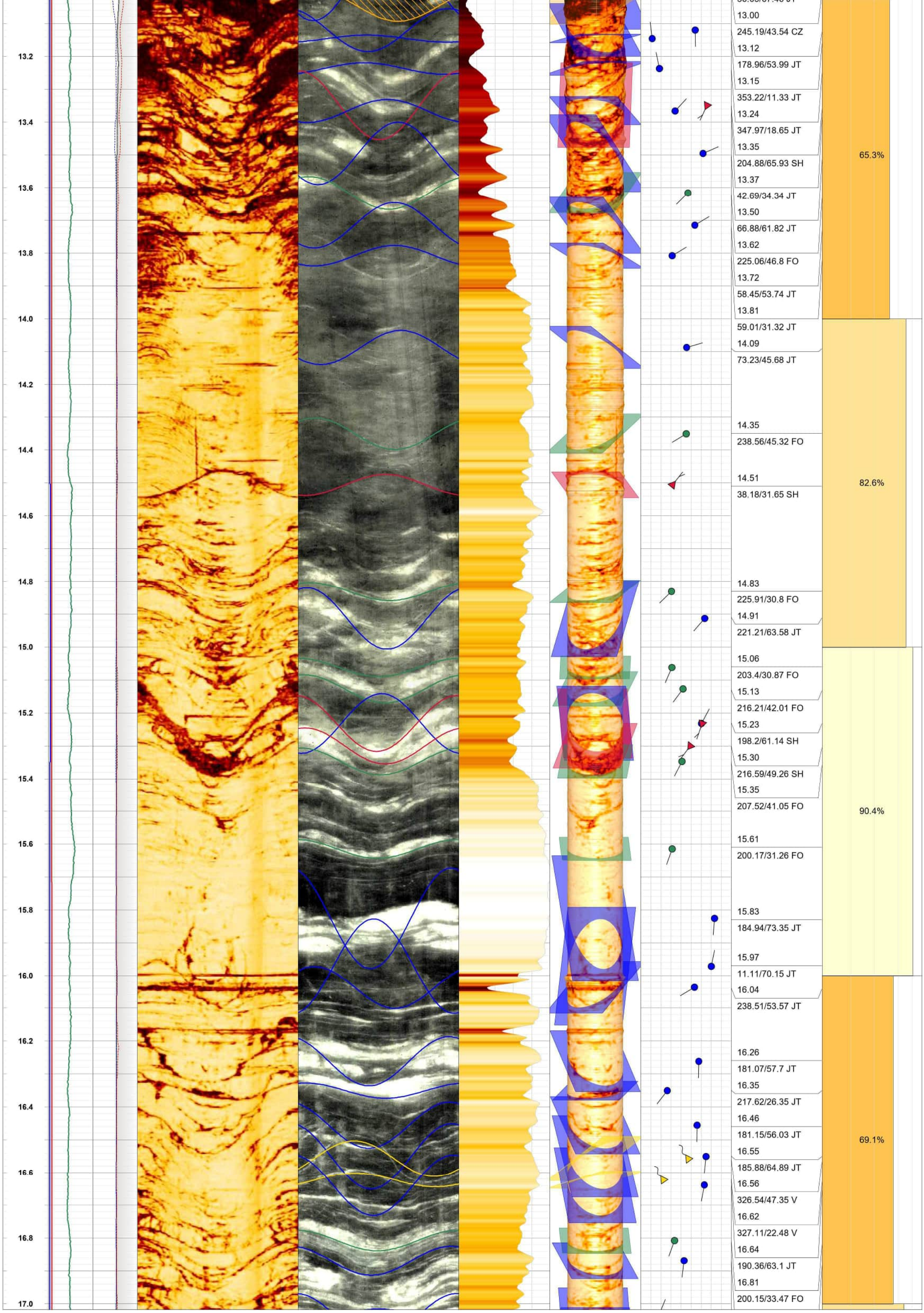
Title	Description	Top [m]	Base [m]	Tool s/n	Run / Date
Reflectivity	Acoustic reflectivity of the rock, relative/pseudo rock hardness	1.5	20.5	ABI/GR 2204023	
Pseudo Core	3D Illustration of the televiewer image	0.4	20.5	ABI/GR 2204023 & OBI22204	
Caliper-min	Minimum borehole caliper [mm]	1.5	20.5	ABI/GR 2204023	
Caliper-max	Max borehole caliper [mm]	1.5	20.5	ABI/GR 2204023	
Caliper-ave	Average borehole caliper [mm]	0.4	20.5	ABI/GR 2204023	1/04/2025
ATV Amplitude-NM	Amplitude televiewer image, oriented to magnetic North	1.5	20.5	ABI/GR 2204023	
Corrected Picks	Corrected Picks, corrected for borehole tilt	1.1	20.0		
GR	Natural Gamma Ray [API]	0.4	19.4	ABI/GR 220402	1/04/2025
OTV-NM	Optical televiewer image, oriented to magnetic North	1.0	19.5	OBI222204	1/04/2025
Apparent Picks	Apparent Picks	1.1	20.0		
Pick Discription	Corrected picks description, Azimuth/Dip & Type	1.1	20.0		
RQD	Rock quality designation derived from apparent structure picks, 1m interval [%]	1.0	20.0		
TILT	Borehole deviation from the vertical, 0 - 90 [deg]	1	20.5		

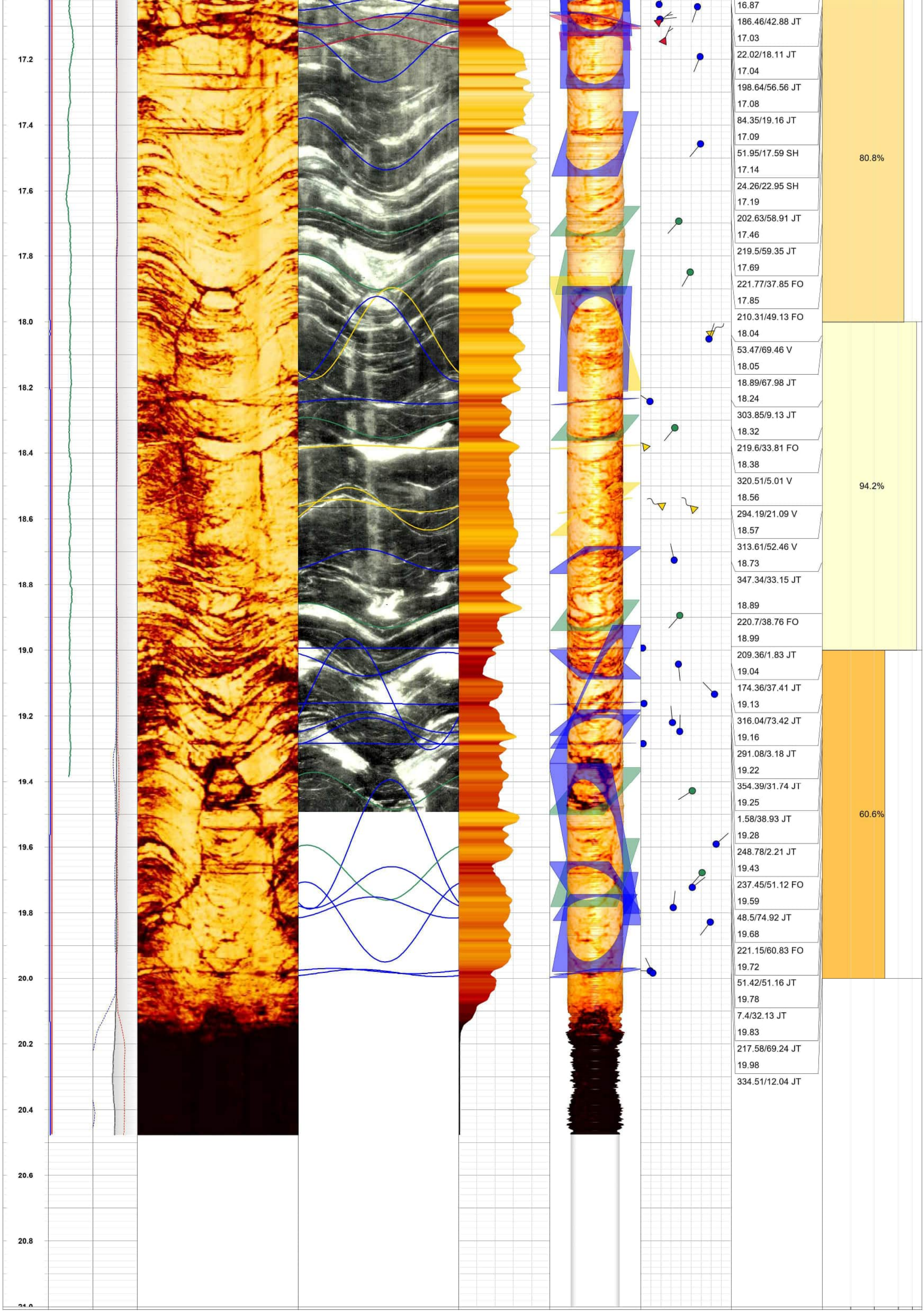


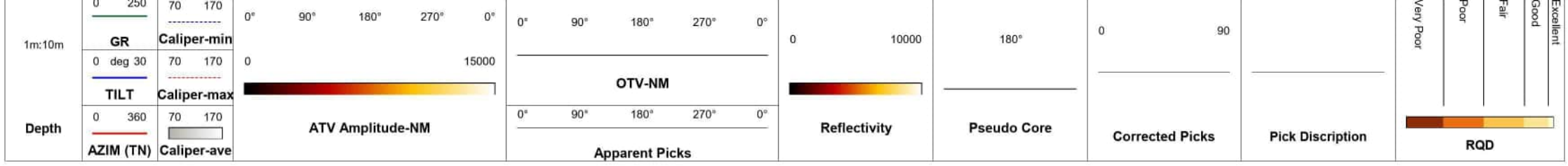

1.2
1.4
1.6
1.8
2.0
2.2
2.4
2.6
2.8
3.0
3.2
3.4
3.6
3.8
4.0
4.2
4.4
4.6
4.8
5.0
314.76/31.29 JT
1.23
214.84/18.66 JT
1.51
16.79/47.81 JT
1.61
3.35/42.18 JT
1.78
328.32/23.14 JT
1.84
303.98/20.62 JT
1.92
23.22/18.24 JT
2.08
53.87/16.98 JT
2.25
4.31/29.49 JT
2.33
230.69/42.73 JT
2.50
2.3/29.53 JT
2.51
163.11/20.92 JT
2.73
169.16/20.11 JT
2.83
183.4/25.03 JT
2.92
45.91/34.74 JT
3.15
26.07/49.44 JT
3.29
40.8/47.59 JT
3.52
182.71/10.69 JT
3.61
352.12/14.28 JT
3.84
238.21/29.19 FO
4.17
236.26/32.01 FO
4.36
192.99/67.78 JT
4.68
318.49/7.85 JT
5.02
72.2%
66.9%
90.7%
100.0%


5.2
5.4
5.6
5.8
6.0
6.2
6.4
6.6
6.8
7.0
7.2
7.4
7.6
7.8
8.0
8.2
8.4
8.6
8.8
9.0
5.38
73.33/36.89 JT
5.40
191.63/74.17 JT
5.45
244.98/32.64 FO
5.69
192.19/59.71 JT
5.95
216.78/31.87 FO
5.96
184.44/54.86 JT
6.05
166.13/14.43 SH
6.06
352.94/52.57 JT
6.12
5.17/34.7 JT
6.31
202.97/46.24 JT
6.52
198.02/44.38 JT
6.58
210.58/25.78 FO
6.73
350.54/27.78 SH
6.77
234.52/42.79 JT
6.86
160.18/74.11 JT
6.91
165.43/56.26 SH
7.25
242.62/41.6 FO
7.33
143.45/63.17 JT
7.40
220.24/52.97 JT
7.53
177.25/54.28 JT
7.60
234.67/35.45 FO
7.86
327.74/30.54 JT
7.89
131.03/17.71 JT
7.90
155.2/67.81 JT
7.95
169.73/68.39 JT
7.98
307.42/45.01 JT
8.06
319.93/71.33 CZ
8.31
182.59/39.66 JT
8.43
171.34/45.42 JT
8.62
184.66/41.86 JT
8.70
9.56/49.37 JT
8.75
237/50.07 JT
8.80
337.7/55.51 JT
94.4%
60.5%
79.2%
41.4%


9.2
9.4
9.6
9.8
10.0
10.2
10.4
10.6
10.8
11.0
11.2
11.4
11.6
11.8
12.0
12.2
12.4
12.6
12.8
13.0
62.03/39.96 JT
8.89
51.27/29.73 JT
9.04
231.78/42.2 FO
9.21
203.37/51.42 JT
9.30
238.15/48.44 FO
9.35
32.21/38.88 JT
9.57
237.93/46.56 FO
9.76
1.09/56.63 JT
9.90
32.15/33.02 JT
9.95
20.71/36.14 JT
9.99
29.11/77.94 JT
10.04
7.45/41.9 JT
10.10
286.37/3.31 SH
10.11
9.18/44.32 JT
10.24
28.39/36.63 JT
10.28
15.75/39.25 JT
10.29
228.75/54.49 FO
10.36
0.78/42.07 JT
10.49
248.15/48.77 SH
10.62
213.87/32.33 FO
10.76
50.31/47.46 JT
10.82
221.16/37.07 JT
10.83
46.88/45.92 JT
10.94
32.42/41.68 JT
11.06
191.97/61.41 SH
11.23
216.63/50.85 SH
11.37
169.28/23.3 JT
11.39
323.18/29.46 JT
11.42
231.03/62.15 SH
11.48
92.56/18.39 JT
11.49
229.47/52.27 SH
11.58
59.69/7.59 JT
11.63
233.38/53.18 SH
11.88
235.23/49.4 FO
11.89
51.84/59.4 JT
12.11
75.65/10.1 JT
12.24
240.91/38.17 FO
12.47
238.3/42.56 FO
12.72
55.65/53.75 JT
12.97
89.5%
62.9%
68.4%
94.4%


13.2
13.4
13.6
13.8
14.0
14.2
14.4
14.6
14.8
15.0
15.2
15.4
15.6
15.8
16.0
16.2
16.4
16.6
16.8
17.0
13.00
245.19/43.54 CZ
13.12
178.96/53.99 JT
13.15
353.22/11.33 JT
13.24
347.97/18.65 JT
13.35
204.88/65.93 SH
13.37
42.69/34.34 JT
13.50
66.88/61.82 JT
13.62
225.06/46.8 FO
13.72
58.45/53.74 JT
13.81
59.01/31.32 JT
14.09
73.23/45.68 JT
14.35
238.56/45.32 FO
14.51
38.18/31.65 SH
14.83
225.91/30.8 FO
14.91
221.21/63.58 JT
15.06
203.4/30.87 FO
15.13
216.21/42.01 FO
15.23
198.2/61.14 SH
15.30
216.59/49.26 SH
15.35
207.52/41.05 FO
15.61
200.17/31.26 FO
15.83
184.94/73.35 JT
15.97
11.11/70.15 JT
16.04
238.51/53.57 JT
16.26
181.07/57.7 JT
16.35
217.62/26.35 JT
16.46
181.15/56.03 JT
16.55
185.88/64.89 JT
16.56
326.54/47.35 V
16.62
327.11/22.48 V
16.64
190.36/63.1 JT
16.81
200.15/33.47 FO
65.3%
82.6%
90.4%
69.1%


17.2
17.4
17.6
17.8
18.0
18.2
18.4
18.6
18.8
19.0
19.2
19.4
19.6
19.8
20.0
20.2
20.4
20.6
20.8
16.87
186.46/42.88 JT
17.03
22.02/18.11 JT
17.04
198.64/56.56 JT
17.08
84.35/19.16 JT
17.09
51.95/17.59 SH
17.14
24.26/22.95 SH
17.19
202.63/58.91 JT
17.46
219.5/59.35 JT
17.69
221.77/37.85 FO
17.85
210.31/49.13 FO
18.04
53.47/69.46 V
18.05
18.89/67.98 JT
18.24
303.85/9.13 JT
18.32
219.6/33.81 FO
18.38
320.51/5.01 V
18.56
294.19/21.09 V
18.57
313.61/52.46 V
18.73
347.34/33.15 JT
18.89
220.7/38.76 FO
18.99
209.36/1.83 JT
19.04
174.36/37.41 JT
19.13
316.04/73.42 JT
19.16
291.08/3.18 JT
19.22
354.39/31.74 JT
19.25
1.58/38.93 JT
19.28
248.78/2.21 JT
19.43
237.45/51.12 FO
19.59
48.5/74.92 JT
19.68
221.15/60.83 FO
19.72
51.42/51.16 JT
19.78
7.4/32.13 JT
19.83
217.58/69.24 JT
19.98
334.51/12.04 JT
80.8%
94.2%
60.6%


1m:10m
Depth
0 250
GR
0 deg 30
TILT
0 360
AZIM (TN)
70 170
Caliper-min
70 170
Caliper-max
70 170
Caliper-ave
0° 90° 180° 270° 0°
0 15000
ATV Amplitude-NM
0° 90° 180° 270° 0°
OTV-NM
0° 90° 180° 270° 0°
Apparent Picks
0 10000
Reflectivity
180°
Pseudo Core
0 90
Corrected Picks
Pick Discription
Very Poor
Poor
Fair
Good
Excellent
RQD

Well Name:	MDD519
Surveys:	ATV-GR & OTV
Location:	Bendigo
Company:	Santana

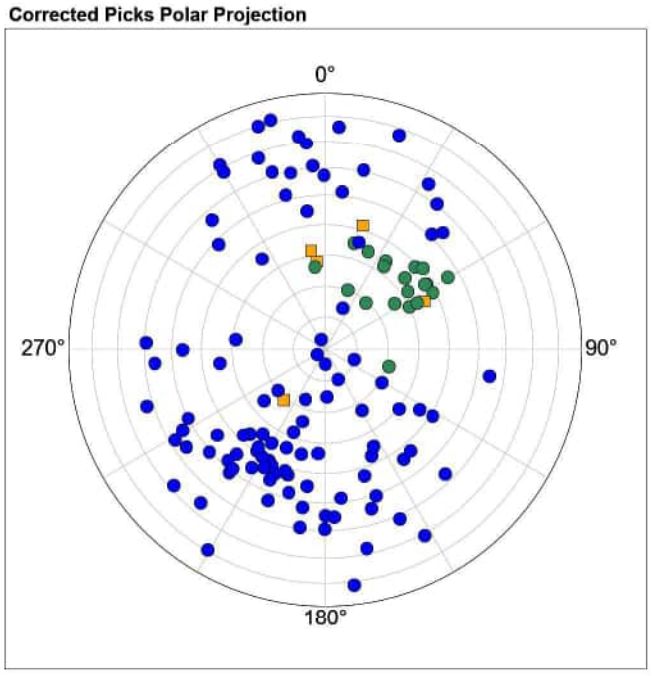
Service Company:	Speight Drilling
Operator:	Gareth Speight
Date Logged:	23/03/2026
Drilling Company:	Speight Drilling
Date Drilled:	
Field:	
County / Township:	
State / Province:	
Country:	

Log Measured From:	Ground Level		
Drilling Measured From:	Ground Level		
Driller Depth:	21	**Logger Depth:**	19.2
Inclination:	-88.8°	**Heading:**	055°(TN)
Easting:		**Northing:**	
Elevation:		**Grid:**	True North (22.5°)
Log Top:	0.2	**Log Bottom:**	19.2
Depth unit:	Metre (m)	**Scale ratio:**	1 : 10

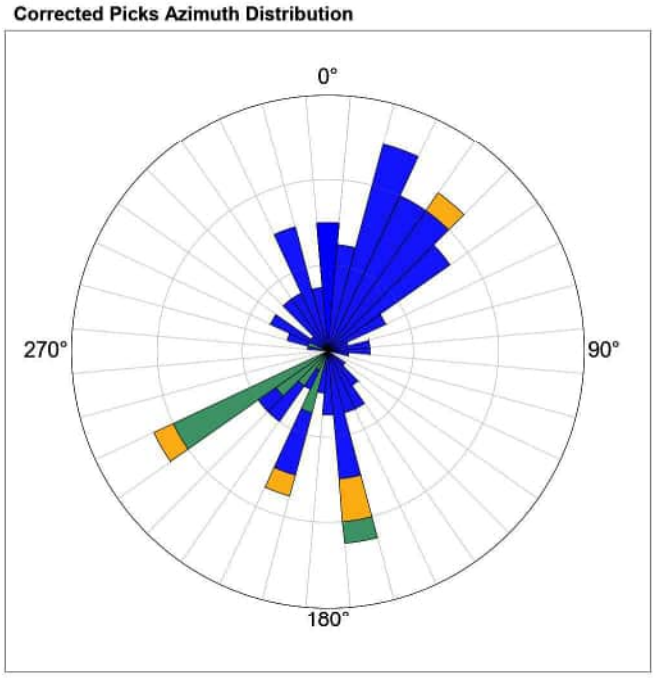
Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	21				334970	334G-042
						Wireline Length:	**Depth Factor:**
						1800	10501/1m

Remarks:

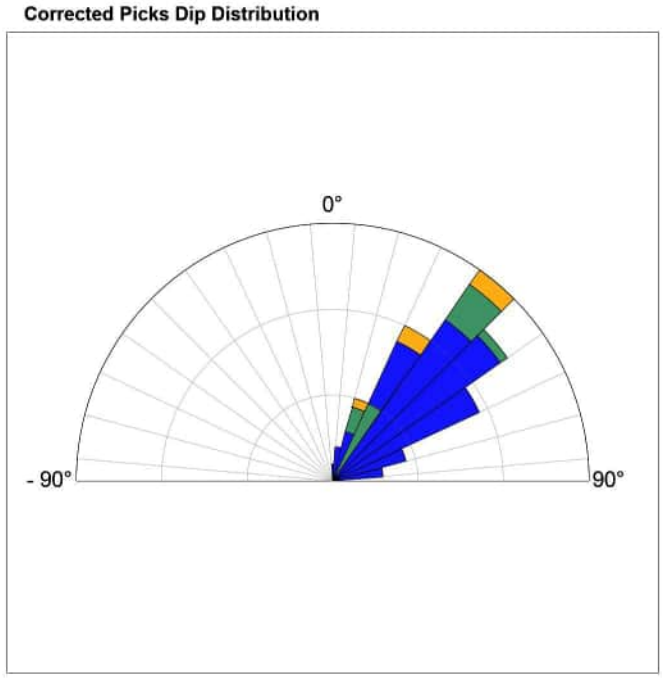
Corrected Picks Polar Projection



Corrected Picks Azimuth Distribution



Corrected Picks Dip Distribution

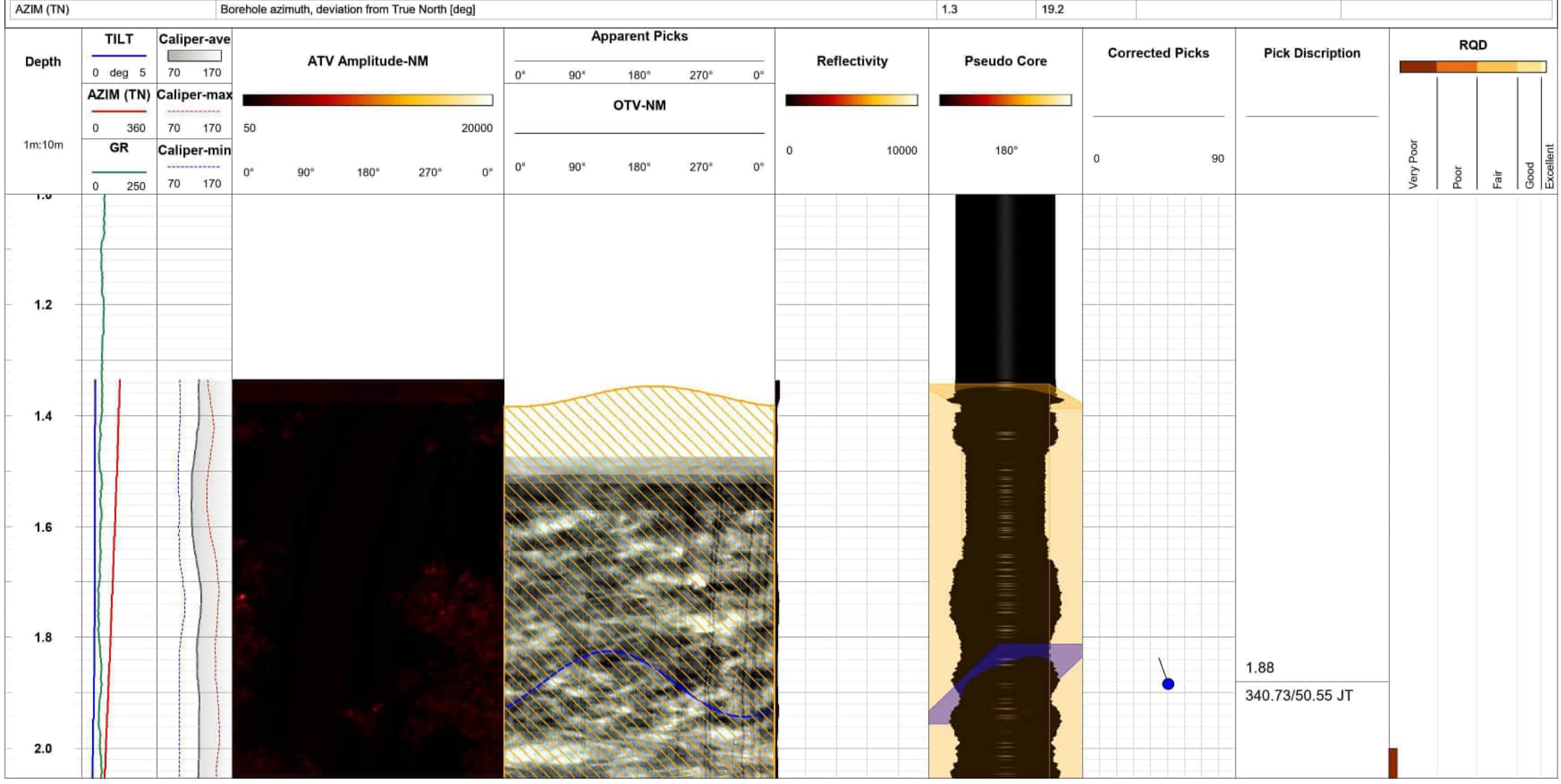


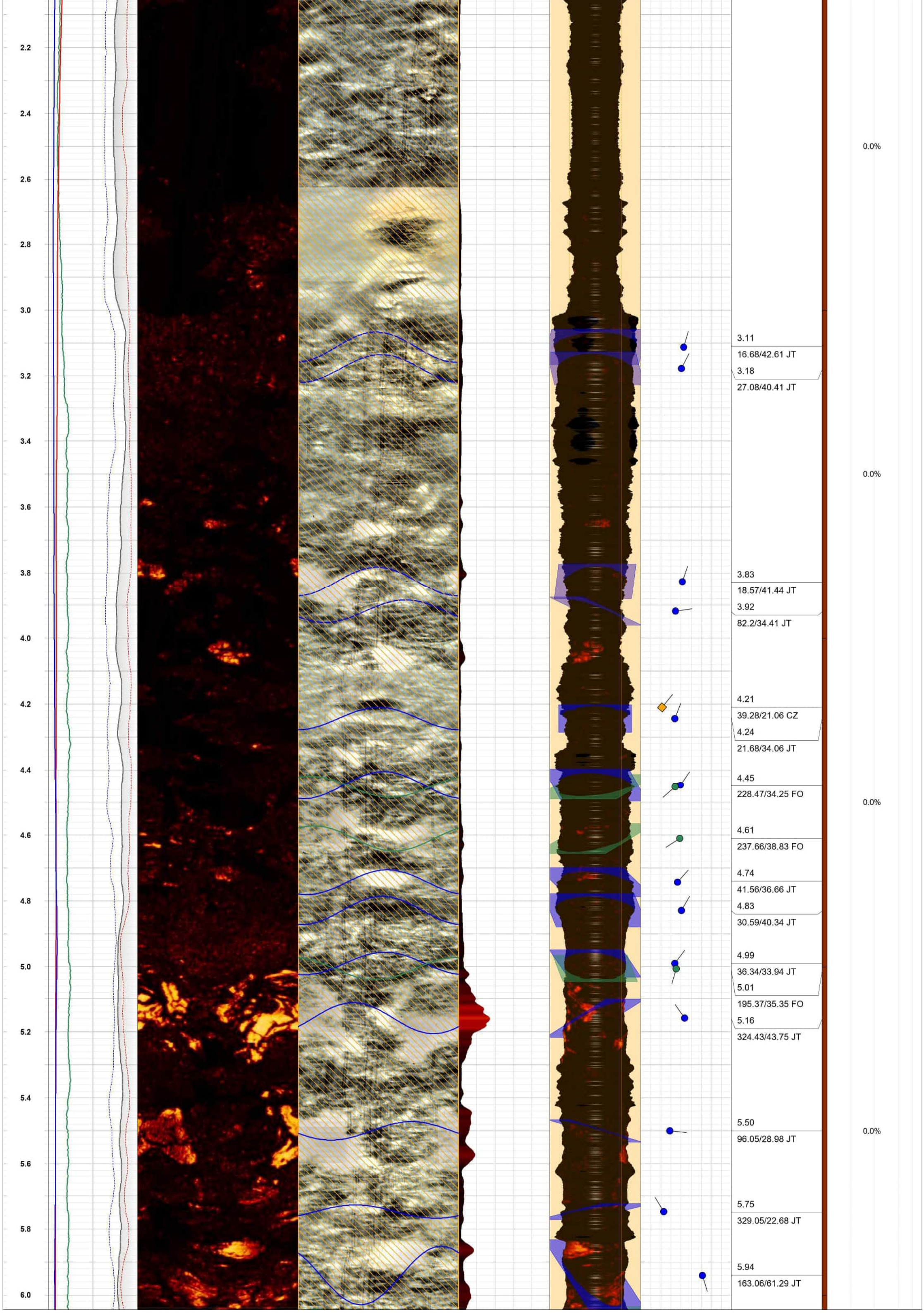
Legend:

FO - Foliation JT - Joint CZ - Crushed Zone

Curve Description:

Title	Description	Top [m]	Base [m]	Tool s/n	Run / Date
Reflectivity	Acoustic reflectivity of the rock, relative/pseudo rock hardness	1.3	19.2	ABI/GR 220402	Run 2, 23/03/2026
Pseudo Core	3D Illustration of the televiewer image	1.3	19.2	ABI/GR 220402	Run 2, 23/03/2026
Caliper-min	Minimum borehole caliper [mm]	1.3	19.2	ABI/GR 220402	Run 2, 23/03/2026
Caliper-max	Max borehole caliper [mm]	1.3	19.2	ABI/GR 220402	Run 2, 23/03/2026
Caliper-ave	Average borehole caliper [mm]	1.3	19.2	ABI/GR 220402	Run 2, 23/03/2026
ATV Amplitude-NM	Acoustic televiewer image, oriented to magnetic North [deg]	1.3	19.2	ABI/GR 220402	Run 2, 23/03/2026
Corrected Picks	Corrected Picks, corrected for borehole tilt	1.9	19.0		
AZIM (MN)	Borehole azimuth, deviation from Magnetic North [deg]	1.3	19.2	ABI/GR 220402	Run 2, 23/03/2026
GR	Natural Gamma Ray [API]	0.2	18.2	ABI/GR 220402	Run 2, 23/03/2026
OTV-NM	Optical televiewer image, oriented to magnetic North [deg]	1.5	19.1	OBI 22204	Run 3, 23/03/2026
Apparent Picks	Apparent Picks	1.9	19.0		
Pick Discription	Corrected picks description, Azimuth/Dip & Type	1.9	19.0		
RQD	Rock quality designation derived from apparent structure picks, 1m interval [%]	2.0	19.0		
AZIM (TN)	Borehole azimuth, deviation from True North [deg]	1.3	19.2		

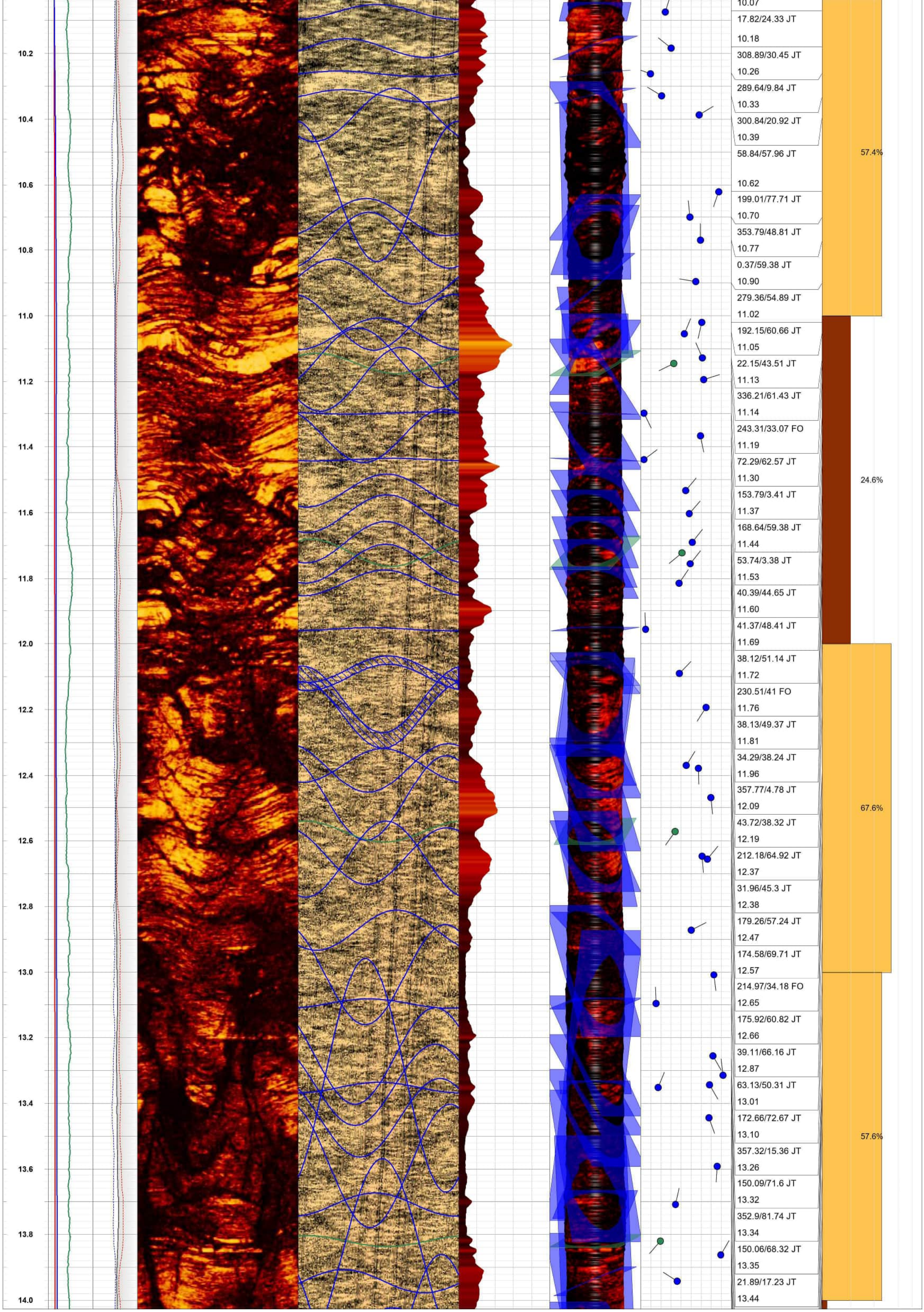


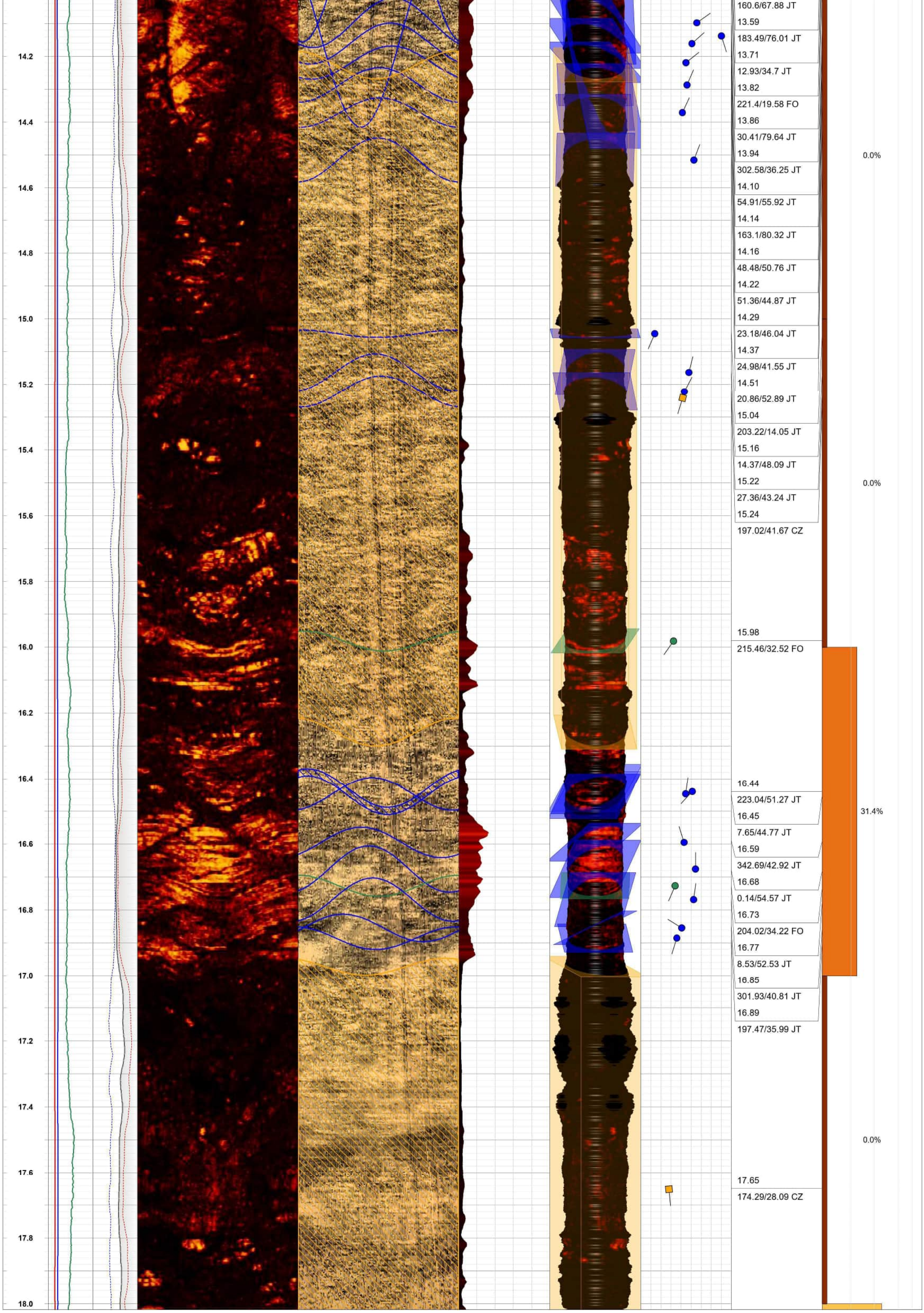

2.2
2.4
2.6
2.8
3.0
3.2
3.4
3.6
3.8
4.0
4.2
4.4
4.6
4.8
5.0
5.2
5.4
5.6
5.8
6.0
3.11
16.68/42.61 JT
3.18
27.08/40.41 JT
3.83
18.57/41.44 JT
3.92
82.2/34.41 JT
4.21
39.28/21.06 CZ
4.24
21.68/34.06 JT
4.45
228.47/34.25 FO
4.61
237.66/38.83 FO
4.74
41.56/36.66 JT
4.83
30.59/40.34 JT
4.99
36.34/33.94 JT
5.01
195.37/35.35 FO
5.16
324.43/43.75 JT
5.50
96.05/28.98 JT
5.75
329.05/22.68 JT
5.94
163.06/61.29 JT
0.0%
0.0%
0.0%
0.0%

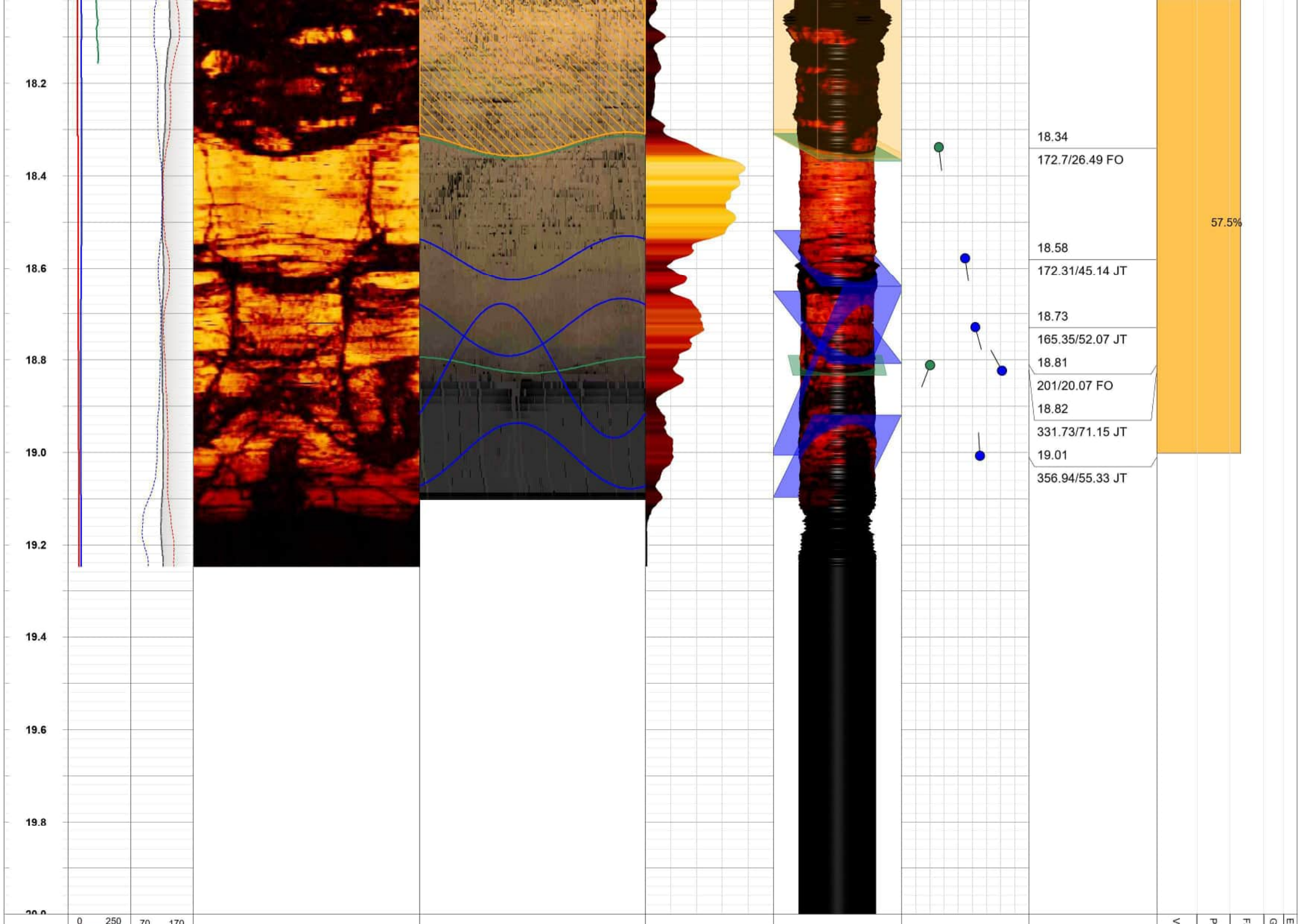
6.08
242.24/39.04 FO
6.10
144.6/35.43 JT
6.59
186.25/51.48 JT
6.78
217.86/60.63 JT
7.04
48.12/68.64 JT
7.06
49.22/20.09 JT
7.13
239.76/46.15 FO
7.32
8.3/59.51 JT
7.37
4/33.63 JT
7.42
320.11/42.89 JT
7.50
237.15/38.29 FO
7.54
60.3/54.12 JT
7.66
235.09/32.34 FO
7.80
89.45/46.49 JT
7.81
166.57/81.35 JT
7.86
84.98/56.58 JT
7.94
171.44/31.76 CZ
8.02
92.11/59.51 JT
8.11
49.77/25.61 JT
8.22
227.88/39.32 FO
8.40
21.32/28.55 JT
8.43
138.59/56.58 JT
8.52
236.65/26.62 FO
8.57
336.42/37.55 JT
8.64
336.49/10.65 JT
8.72
333.54/34.95 JT
8.85
315.98/57.12 JT
8.86
243.34/30.23 FO
9.44
244.27/35.55 CZ
9.45
343.85/54.46 JT
9.55
348.17/68.19 JT
9.63
30.31/34.83 JT
9.77
285.61/21.14 FO
9.79
225.39/54.41 JT

0.0%
56.5%
56.8%
0.0%

6.2
6.4
6.6
6.8
7.0
7.2
7.4
7.6
7.8
8.0
8.2
8.4
8.6
8.8
9.0
9.2
9.4
9.6
9.8
10.0


10.2
10.4
10.6
10.8
11.0
11.2
11.4
11.6
11.8
12.0
12.2
12.4
12.6
12.8
13.0
13.2
13.4
13.6
13.8
14.0
10.07
17.82/24.33 JT
10.18
308.89/30.45 JT
10.26
289.64/9.84 JT
10.33
300.84/20.92 JT
10.39
58.84/57.96 JT
10.62
199.01/77.71 JT
10.70
353.79/48.81 JT
10.77
0.37/59.38 JT
10.90
279.36/54.89 JT
11.02
192.15/60.66 JT
11.05
22.15/43.51 JT
11.13
336.21/61.43 JT
11.14
243.31/33.07 FO
11.19
72.29/62.57 JT
11.30
153.79/3.41 JT
11.37
168.64/59.38 JT
11.44
53.74/3.38 JT
11.53
40.39/44.65 JT
11.60
41.37/48.41 JT
11.69
38.12/51.14 JT
11.72
230.51/41 FO
11.76
38.13/49.37 JT
11.81
34.29/38.24 JT
11.96
357.77/4.78 JT
12.09
43.72/38.32 JT
12.19
212.18/64.92 JT
12.37
31.96/45.3 JT
12.38
179.26/57.24 JT
12.47
174.58/69.71 JT
12.57
214.97/34.18 FO
12.65
175.92/60.82 JT
12.66
39.11/66.16 JT
12.87
63.13/50.31 JT
13.01
172.66/72.67 JT
13.10
357.32/15.36 JT
13.26
150.09/71.6 JT
13.32
352.9/81.74 JT
13.34
150.06/68.32 JT
13.35
21.89/17.23 JT
13.44
57.4%
24.6%
67.6%
57.6%


14.2
14.4
14.6
14.8
15.0
15.2
15.4
15.6
15.8
16.0
16.2
16.4
16.6
16.8
17.0
17.2
17.4
17.6
17.8
18.0
160.6/67.88 JT
13.59
183.49/76.01 JT
13.71
12.93/34.7 JT
13.82
221.4/19.58 FO
13.86
30.41/79.64 JT
13.94
302.58/36.25 JT
14.10
54.91/55.92 JT
14.14
163.1/80.32 JT
14.16
48.48/50.76 JT
14.22
51.36/44.87 JT
14.29
23.18/46.04 JT
14.37
24.98/41.55 JT
14.51
20.86/52.89 JT
15.04
203.22/14.05 JT
15.16
14.37/48.09 JT
15.22
27.36/43.24 JT
15.24
197.02/41.67 CZ
15.98
215.46/32.52 FO
16.44
223.04/51.27 JT
16.45
7.65/44.77 JT
16.59
342.69/42.92 JT
16.68
0.14/54.57 JT
16.73
204.02/34.22 FO
16.77
8.53/52.53 JT
16.85
301.93/40.81 JT
16.89
197.47/35.99 JT
17.65
174.29/28.09 CZ
0.0%
0.0%
31.4%
0.0%



1m:10m

Depth

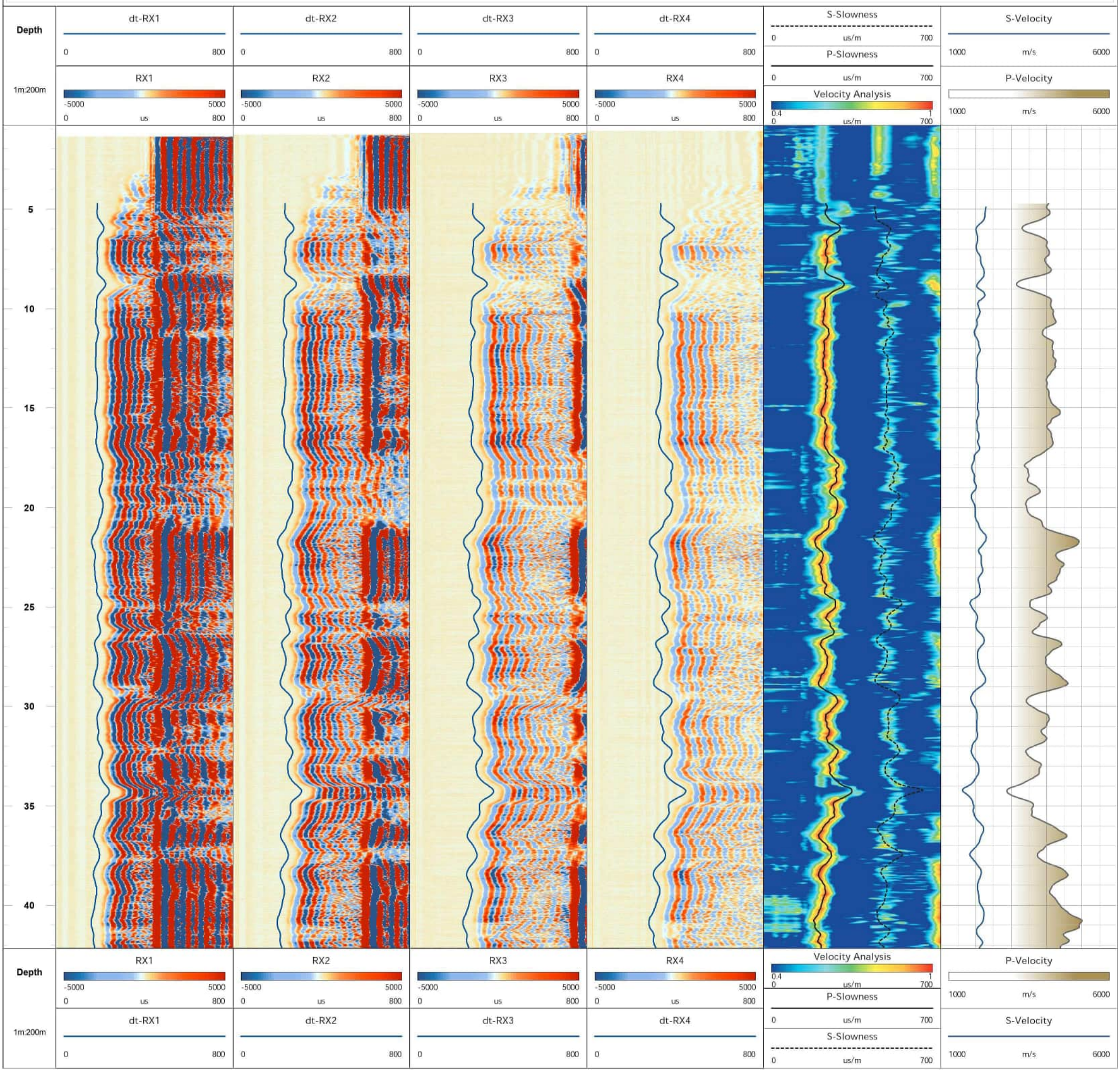
0 250	70 170	0° 90° 180° 270° 0°	0° 90° 180° 270° 0°	0 10000	180°	0 90		Very Poor / Poor / Fair / Good / Excellent		
GR	Caliper-min									
0 360	70 170	50 20000	OTV-NM							
AZIM (TN)	Caliper-max									
0 deg 5	70 170	ATV Amplitude-NM	0° 90° 180° 270° 0°	Reflectivity	Pseudo Core	Corrected Picks	Pick Discription	RQD		
TILT	Caliper-ave		Apparent Picks							

Well Name:	MDD333
Surveys:	Full Waveform Sonic
Location:	
Company:	

Service Company:	SPEIGHT DRILLING LTD	Log Measured From:	Ground Level		
Operator:	Gareth	Drilling Measured From:	Ground Level		
Date Logged:	15 June 2024	Driller Depth:		Logger Depth:	
Drilling Company:		Inclination:	-88.7°	Heading:	324.4° (MN)
Date Drilled:		Easting:		Northing:	
Field:		Elevation:		Grid:	
County / Township:		Log Top:	0.78	Log Bottom:	42.16
State / Province:					
Country:		Depth unit:	Meters	Scale ratio:	1 : 200

Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
						334970	334G-042
						Wireline Length:	Depth Factor:
						1800	10501/1m

Remarks:

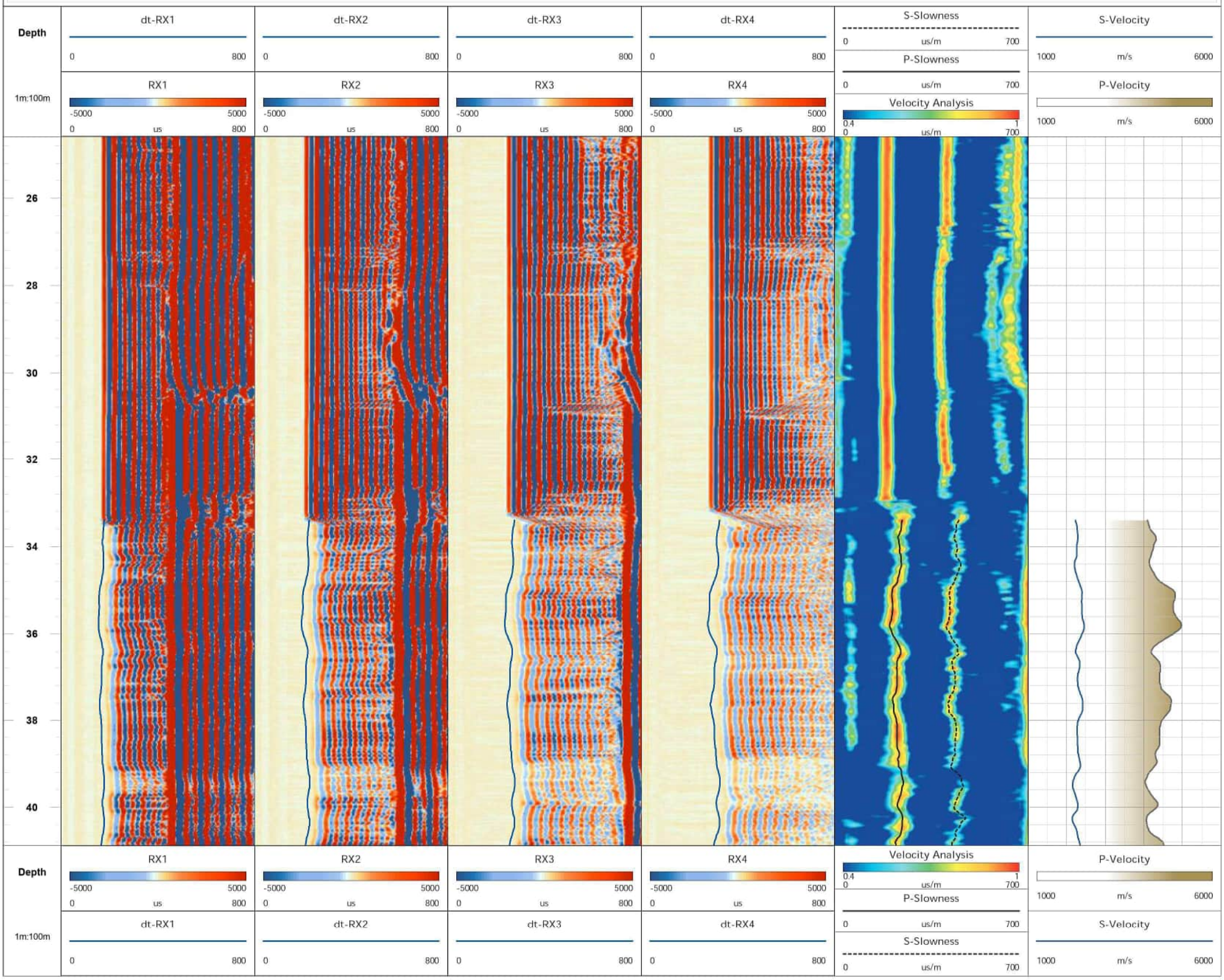


Well Name:	MDD365
Surveys:	Full Waveform Sonic
Location:	
Company:	

Service Company:	SPEIGHT DRILLING LTD	Log Measured From:	Ground Level		
Operator:	Gareth	Drilling Measured From:	Ground Level		
Date Logged:	18 Sep 2024	Driller Depth:	44.3	Logger Depth:	42.2
Drilling Company:		Inclination:		Heading:	
Date Drilled:		Easting:		Northing:	
Field:		Elevation:		Grid:	
County / Township:		Log Top:	24.6	Log Bottom:	40.9
State / Province:					
Country:		Depth unit:	Meters	Scale ratio:	1 : 100

Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
						334970	334G-042
						Wireline Length:	Depth Factor:
						1800	10501/1m

Remarks:
Hole blocked several times around 27.7m and 28.9m; casing installed down to 33m.



Well Name:	MDD394
Surveys:	FWS
Location:	Bendigo
Company:	Santana

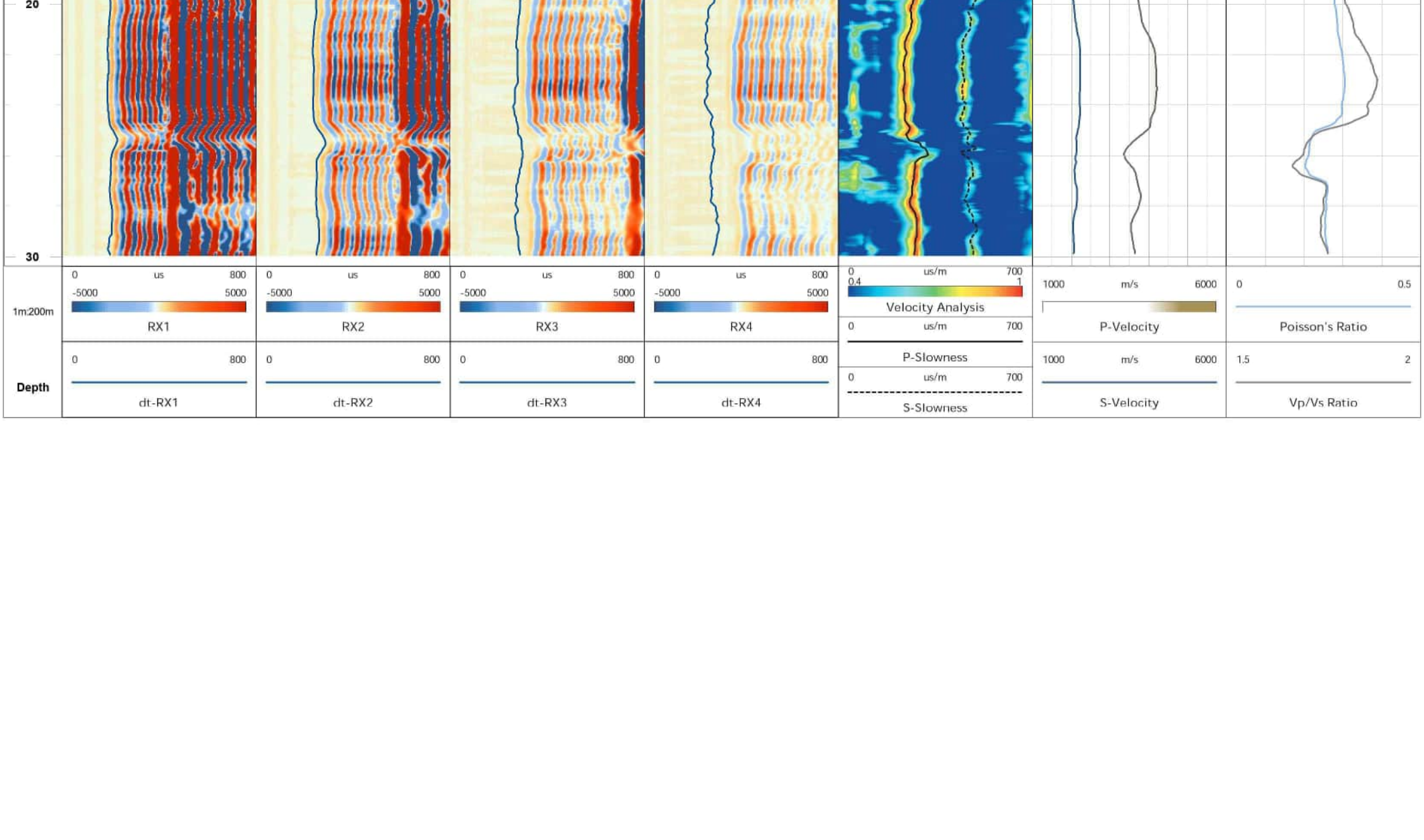
Service Company:	Speight Drilling
Operator:	Gareth Speight
Date Logged:	10/12/2024
Drilling Company:	Speight Drilling
Date Drilled:	
Field:	
County / Township:	
State / Province:	
Country:	

Log Measured From:	Ground Level		
Drilling Measured From:	Ground Level		
Driller Depth:		Logger Depth:	29.4
Inclination:	-88.5°	Heading:	002° (MN)
Easting:		Northing:	
Elevation:		Grid:	
Log Top:	7.4	Log Bottom:	29.4
Depth unit:	m	Scale ratio:	1 : 200

Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
HQ	0	30					
						Wireline Length:	Depth Factor:

Remarks:

Disclaimer:

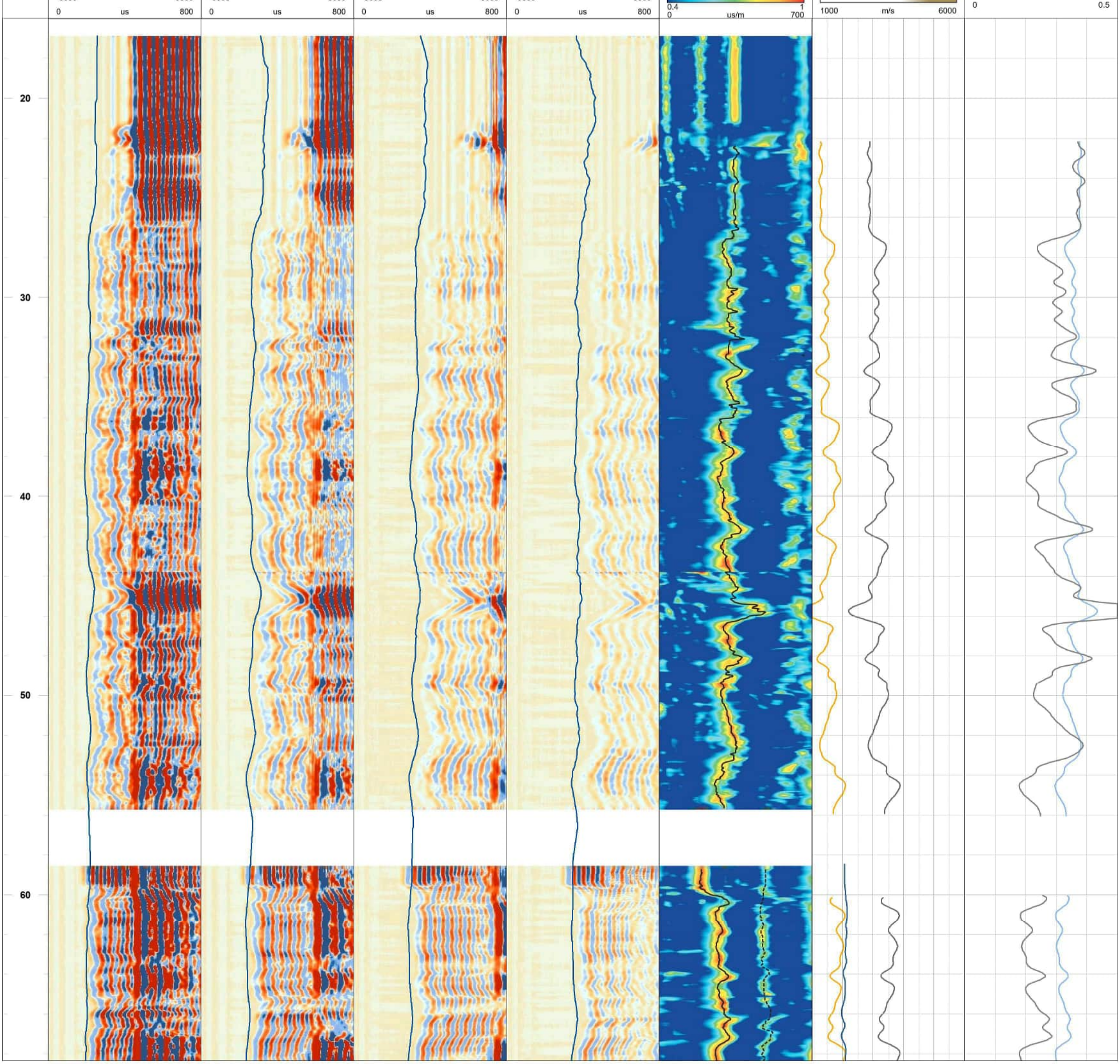


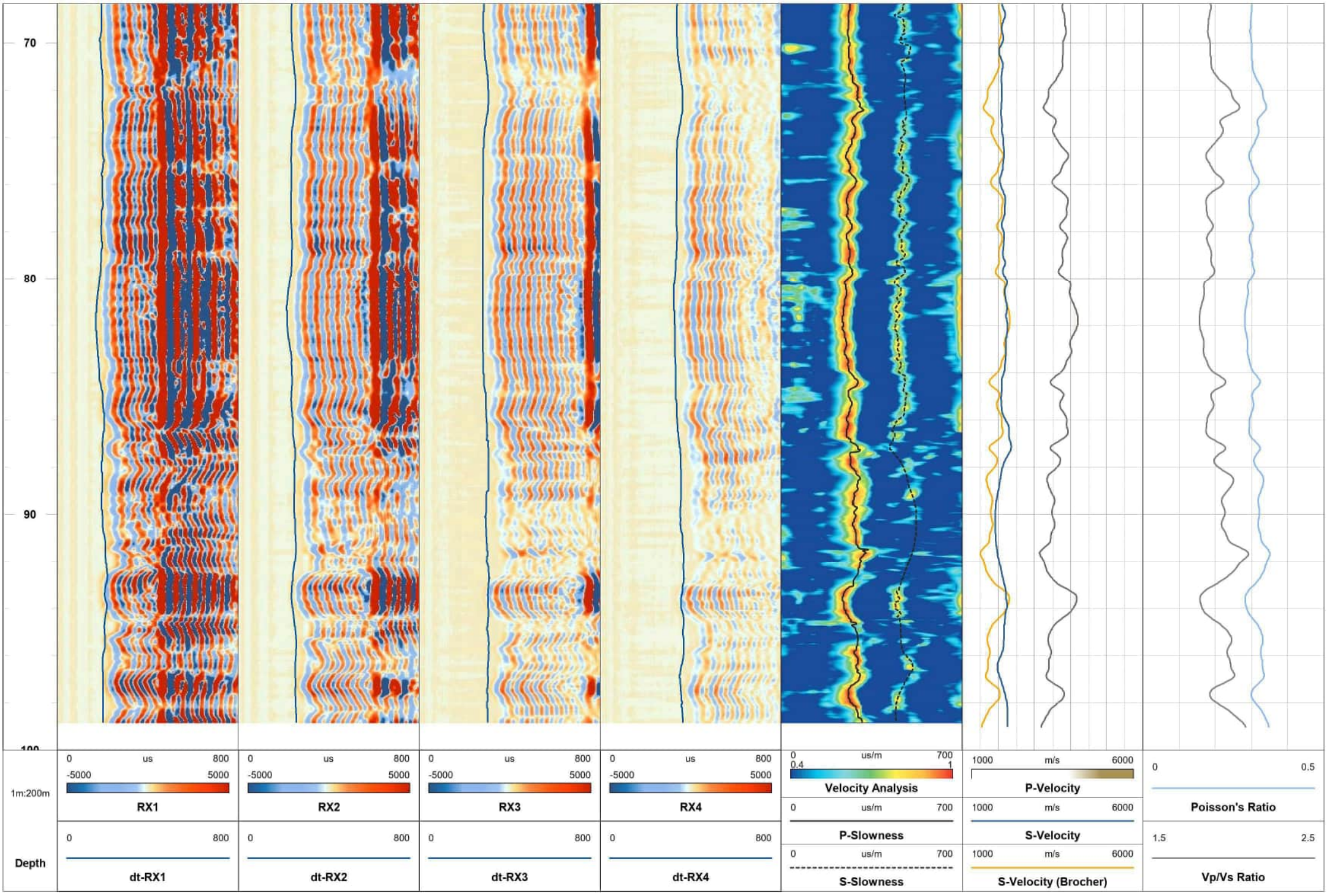
Well Name:	MDD491
Surveys:	FWS
Location:	Bendigo
Company:	Santana

Service Company:	Speight Drilling	**Log Measured From:**	Ground Level		
Operator:	Gareth Speight	**Drilling Measured From:**	Ground Level		
Date Logged:	1/04/2025	**Driller Depth:**	100	**Logger Depth:**	99
Drilling Company:	Speight Drilling	**Inclination:**	-71°	**Heading:**	338° (MN)
Date Drilled:		**Easting:**		**Northing:**	
Field:		**Elevation:**		**Grid:**	
County / Township:		**Log Top:**	16.9	**Log Bottom:**	98.9
State / Province:					
Country:		**Depth unit:**		**Scale ratio:**	1 : 200

Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	60					
HQ	60	100				Wireline Length:	Depth Factor:

Remarks:
No observable s-slowness for velocity analysis in the top section. Empirical approach after Brocher has been applied.



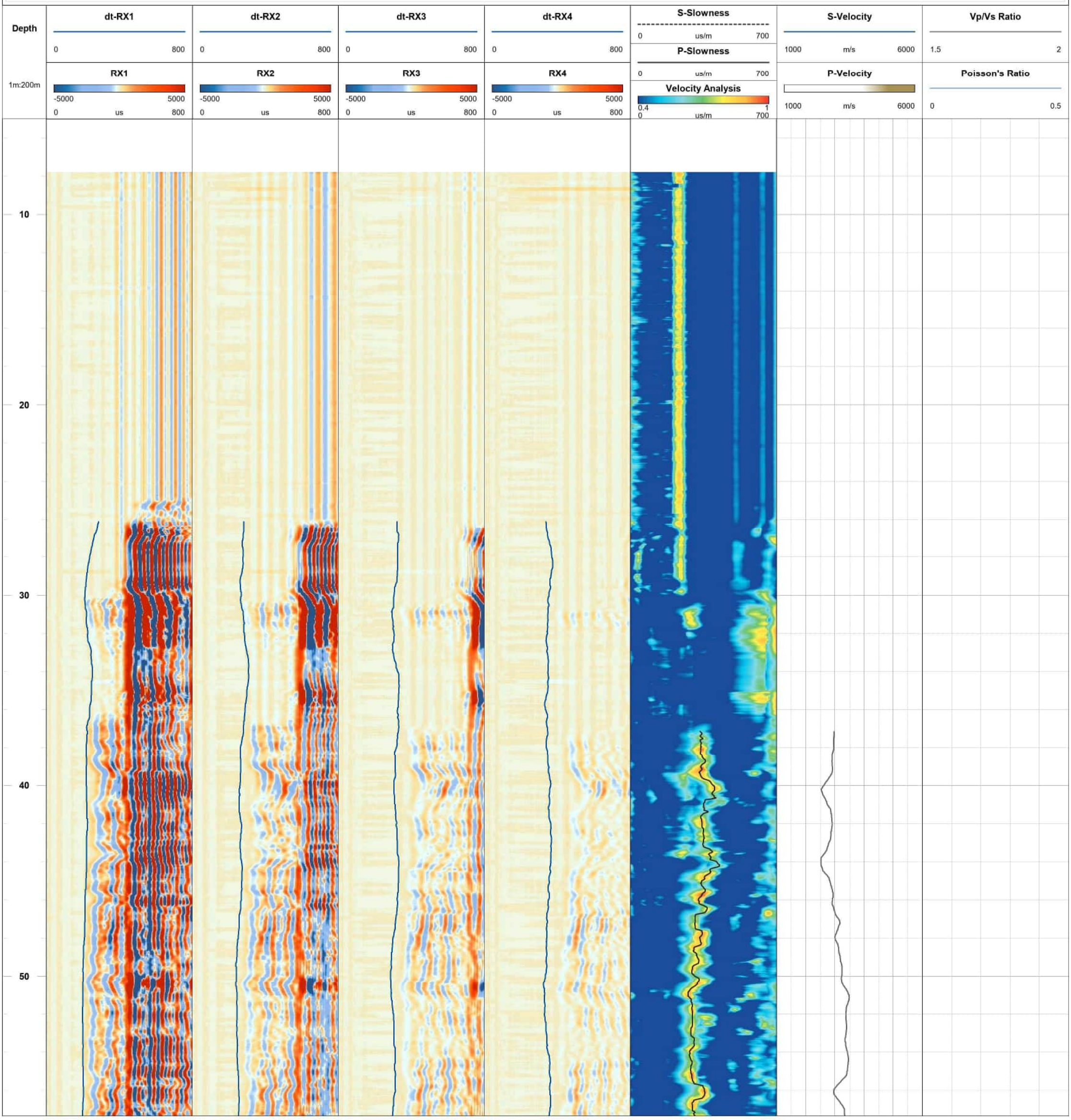

70
80
90
100
1m:200m
Depth
0 us 800
-5000 5000
RX1
RX2
RX3
RX4
0 800
dt-RX1
dt-RX2
dt-RX3
dt-RX4
0 us/m 700
0.4 1
Velocity Analysis
P-Slowness
S-Slowness
1000 m/s 6000
P-Velocity
S-Velocity
S-Velocity (Brocher)
0 0.5
Poisson's Ratio
1.5 2.5
Vp/Vs Ratio

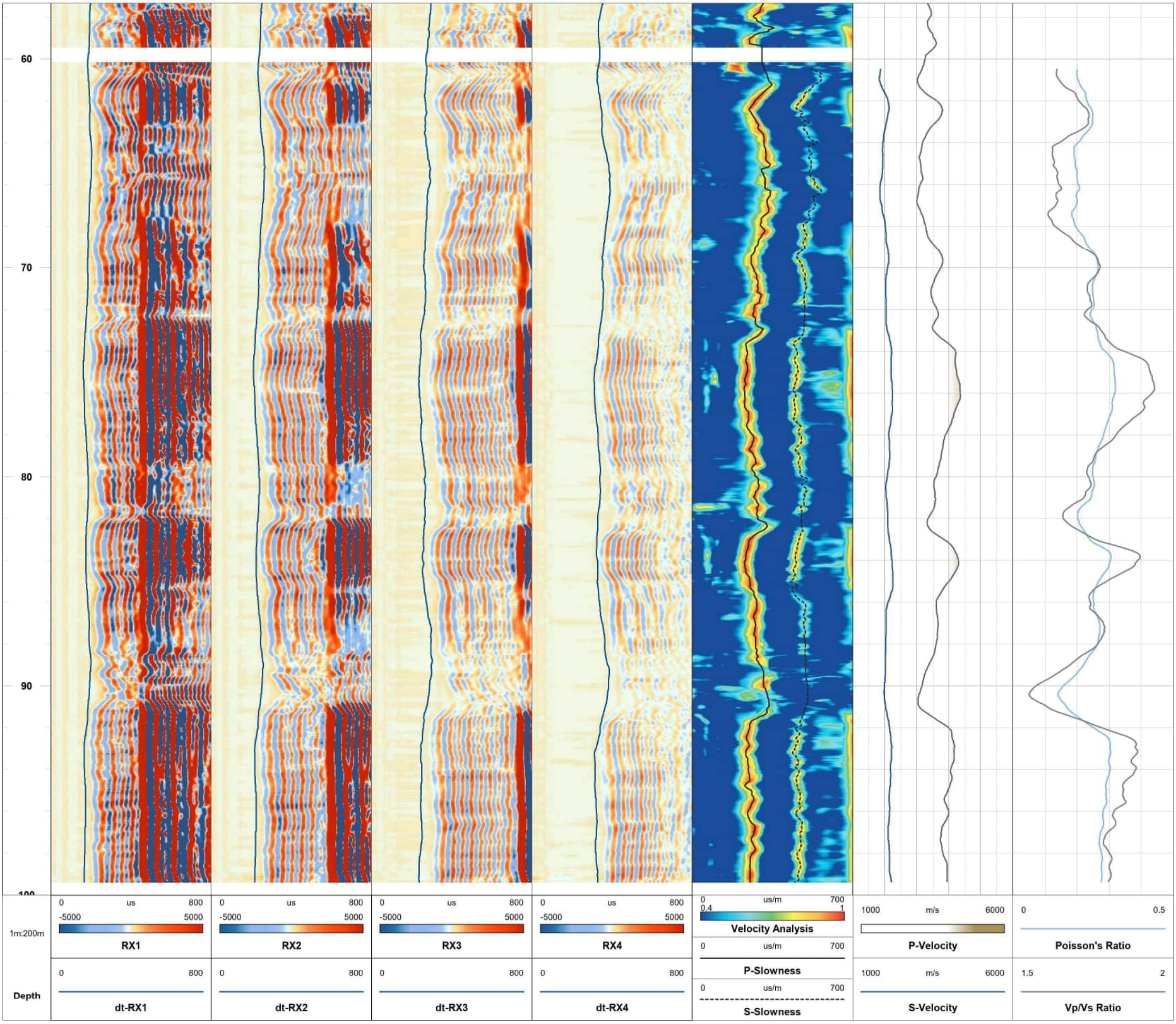
Well Name:	MDD493
Surveys:	FWS
Location:	Bendigo
Company:	Santana

Service Company:	Speight Drilling	**Log Measured From:**	Ground Level		
Operator:	Gareth Speight	**Drilling Measured From:**	Ground Level		
Date Logged:	16/01/2026	**Driller Depth:**	100	**Logger Depth:**	100
Drilling Company:	Speight Drilling	**Inclination:**	-69°	**Heading:**	150° (MN)
Date Drilled:		**Easting:**		**Northing:**	
Field:		**Elevation:**		**Grid:**	
County / Township:		**Log Top:**	7.84	**Log Bottom:**	99.7
State / Province:					
Country:		**Depth unit:**		**Scale ratio:**	1 : 200

Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	60					
HQ	60	100				Wireline Length:	Depth Factor:

Remarks:



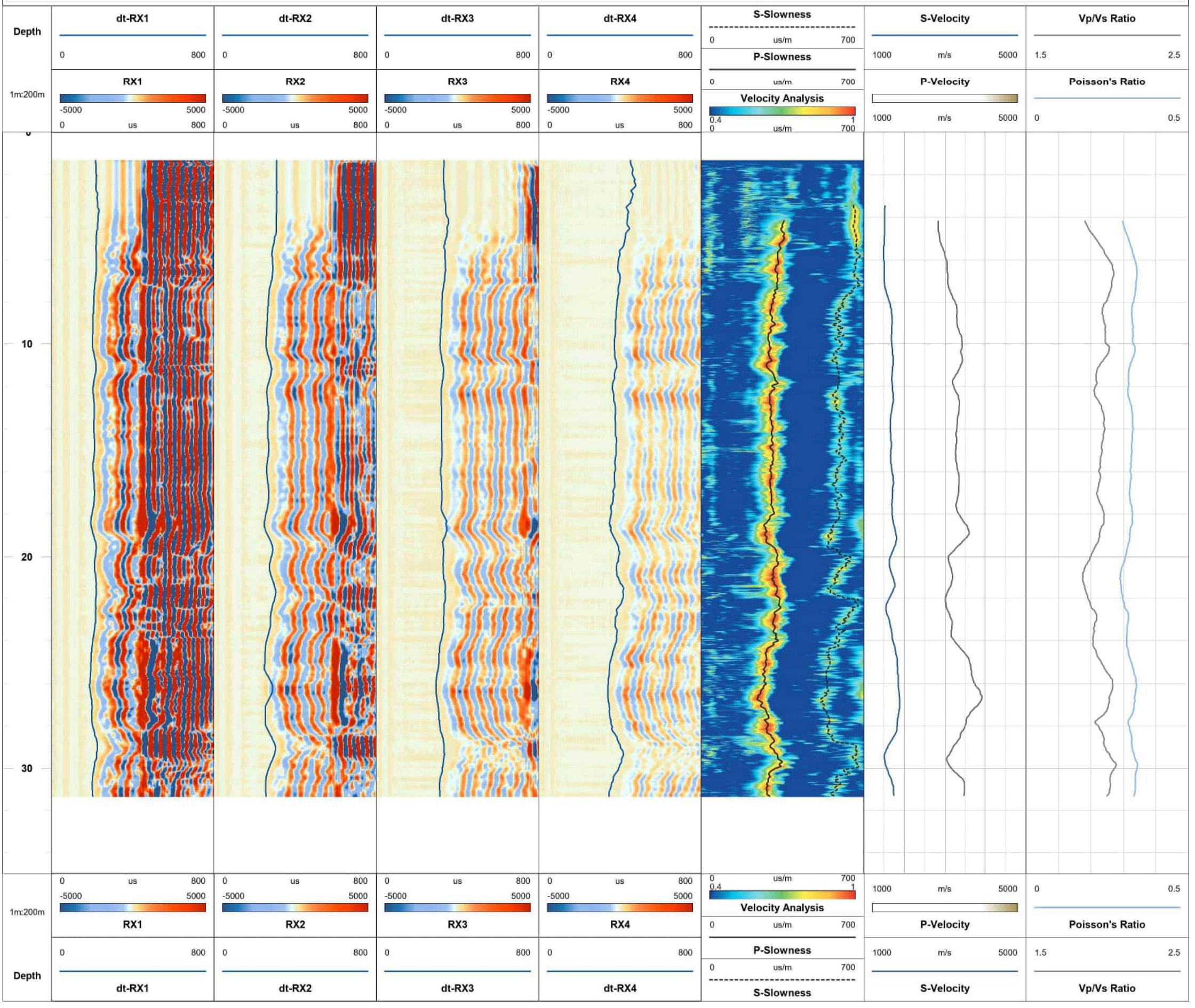

60
70
80
90
100
1m:200m
Depth
0 us 800
-5000 5000
RX1
RX2
RX3
RX4
0 us/m 700
0.4 1
Velocity Analysis
P-Slowness
S-Slowness
1000 m/s 6000
P-Velocity
S-Velocity
0 0.5
Poisson's Ratio
1.5 2
Vp/Vs Ratio
dt-RX1
dt-RX2
dt-RX3
dt-RX4

Well Name:	MDD502
Surveys:	FWS
Location:	Bendigo
Company:	Santana

Service Company:	Speight Drilling	**Log Measured From:**	Ground Level		
Operator:	Gareth Speight	**Drilling Measured From:**	Ground Level		
Date Logged:	14/02/2026	**Driller Depth:**	32	**Logger Depth:**	31.3
Drilling Company:	Speight Drilling	**Inclination:**	-64°	**Heading:**	207° (TN)
Date Drilled:		**Easting:**		**Northing:**	
Field:		**Elevation:**		**Grid:**	
County / Township:		**Log Top:**	1.3	**Log Bottom:**	31.3
State / Province:					
Country:		**Depth unit:**		**Scale ratio:**	1 : 200

Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	32					
						Wireline Length:	Depth Factor:

Remarks:



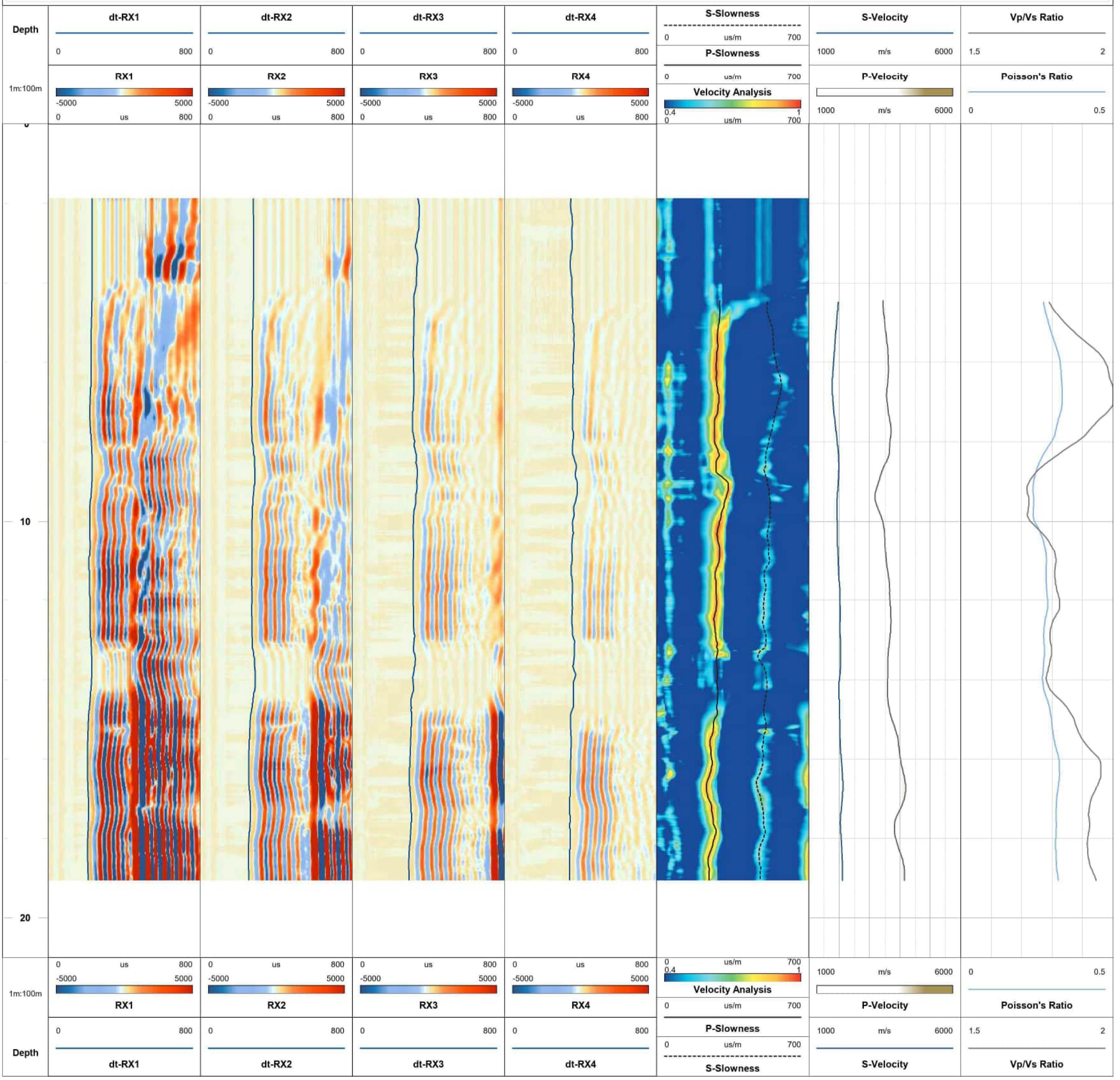
Well Name:	MDD515
Surveys:	FWS
Location:	Bendigo
Company:	Santana

Service Company:	Speight Drilling
Operator:	Gareth Speight
Date Logged:	15/03/2026
Drilling Company:	Speight Drilling
Date Drilled:	
Field:	
County / Township:	
State / Province:	
Country:	

Log Measured From:	Ground Level		
Drilling Measured From:	Ground Level		
Driller Depth:	21	**Logger Depth:**	19.1
Inclination:	-88.5°	**Heading:**	027°(TN)
Easting:		**Northing:**	
Elevation:		**Grid:**	True North (22.5°)
Log Top:	0.0	**Log Bottom:**	19.1
Depth unit:	Metre (m)	**Scale ratio:**	1 : 100

Bit Size:	Start Depth:	End Depth:	Casing:	Start Depth:	End Depth:	Winch Model:	Winch Serial:
PQ	0	21				334970	334G-042
						Wireline Length:	**Depth Factor:**
						1800	10501/1m

Remarks:



Geophysical Investigations

Geophysical Survey: Downhole Shear Wave (DHVs) and Multi-Channel Analysis of Surface Waves (MASW) Survey Bendigo - Ophir

Report prepared for Matakanui Gold Ltd



Southern Geophysical

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Data collected and report prepared for Southern Geophysical Limited by:

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Capability Statement

Southern Geophysical experienced team provides geophysical contracting and consulting services to clients in the mineral, energy, geotechnical, civil engineering and environmental sectors. We have one of the largest equipment resources for shallow geophysical surveys in the independent private sector in New Zealand.

We are proudly Canterbury owned and operated and have been since our beginnings in 2004. We operate in New Zealand, the Pacific Islands, and Antarctica. The geophysical methods most often employed include:

- Downhole Seismic Testing
  - Accurate shear wave (Vs) profiles and Vs30 measurements
- Multi-channel Analysis of Surface Waves (MASW)
  - Shallow bedrock profiling
  - Near surface shear wave velocity profiling and rippability determination
- Crosshole Seismic Testing
  - Best available method for accurate Vs assessment
- Seismic Reflection
  - Identifying lithological boundaries (20–600 m)
- Shear Wave Reflection
  - Bedrock profiling and identifying lithological boundaries (< 50 m)
- Seismic Refraction
  - Bedrock profiling
- Ground Penetrating Radar (GPR)
  - High resolution imaging of near surface stratigraphy
  - Detection of placer gold paleo channels
  - Mapping near surface coal and mineral deposits
  - Gravel resource characterisation
- Electrical Resistivity Tomography (ERT)
  - Identification of ore bodies through electrical resistivity
  - Lithological mapping through changes in electrical properties
- Induced Polarisation (IP)
  - Identification of ore bodies through electrical chargeability

Our team is confident and capable of utilising the widest range of geophysical systems. We have run numerous large scale MASW surveys over the last 17 years. The team is highly skilled in the processing of all data acquired, reporting in the way the client requests and being at the end of the phone or an email to respond to queries which may arise.

SGL Job Reference: 3068
Version 1 (Issued March 13th, 2026)

Internally reviewed by:
M. Finnemore (PhD), Senior Geophysicist

1 Executive Summary

Southern Geophysical undertook a Downhole Shear Wave (DHVs) survey along with a Multi-Channel Analysis of Surface Waves (MASW) survey at the mill processing site, Bendigo on the 24th and 25th of February 2026 (Figures 1 & 2). Testing was undertaken in borehole EGL06B to a depth of 30 m (maximum borehole depth), with data acquired at 1 m intervals. Two MASW lines were also acquired intersecting the borehole location (Figure 3). The aim of the survey was to determine shear wave velocities (Vs) to 30 m depth. Alongside two MASW surveys lines, used to characterise the near-surface Vs structure to ~12 m depth, for correlation with the downhole data and to assist in identifying the bedrock horizon.

The two MASW lines successfully imaged shear-wave velocities to ~12 m depth, increasing from around 200 m/s near surface to over 900 m/s approaching the interpreted schist bedrock horizon (Figure 4). The downhole results from EGL06B indicate velocities of approximately 250 m/s within the upper ~11 m, which correlate well with the MASW profiles. At greater depths the downhole arrivals indicate a clear increase in velocity consistent with competent schist bedrock, with apparent velocities exceeding ~2000 m/s below approximately 14 m (Figure 5). However, within the rock interval the high shear-wave velocities result in wavelengths significantly longer than the 1 to 2 m receiver spacing used in the downhole probe, meaning the interval velocity method is not suitable for resolving true velocities at this scale. As a result, interval velocity estimates within the bedrock should be treated with caution, with interpretation instead based on the overall measured velocity trend within the rock unit.

2 Site Description

The site is located approximately 7 km Southeast of Lindis Crossing, Bendigo (Figure 1).



Figure 1: Site Location, in red rectangle.

Geological mapping by GNS identifies the area as variably foliated and segregated Haast Schist (TZ III to TZ IV) (Figure 2).

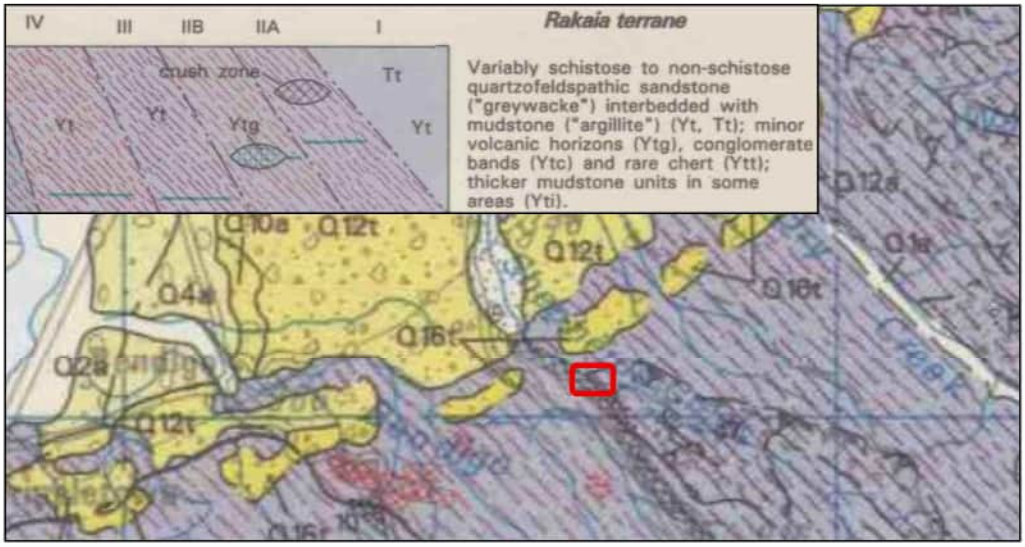


Figure 2: Site geology (GNS Science QMAP database), red rectangle.

3 Methodology

3.1 DHVs survey design

The DHVs survey was conducted according to the guidelines in the standard ASTM D74001[1] and the QuakeCentre Invasive Seismic Testing – A Summary of Methods and Good Practice, F. Wentz 2019[2].

The borehole was installed with a 50 mm inside diameter PVC pipe (backfilled with grout). The downhole seismic test was undertaken by lowering a four-geophone probe (30 Hz sensors with 1 m probe separation) down the borehole and recording the surface-generated shear wave signal at 1 m increments to the bottom of the hole. The probe consists of three horizontally orientated geophones spaced at 1 m intervals and one vertical geophone located in the same section of the probe as the lowest horizontal sensor. This configuration allows shear wave arrivals to be recorded at multiple depths and enables a true interval velocity measurement over 1 and 2 m separations between the upper and lower horizontal sensors. The downhole probe uses a non-flexible rod system with a gyroscopic sensor to maintain the optimum orientation to the surface shear wave source.

The geophone tool was fixed in place at each depth interval using a three-bladder air clamping system. A timber sleeper (0.15 × 0.2 × 0.8 m), weighed down with a 1500 kg utility vehicle, acted as the shear wave source. The source was offset from the borehole by 800 mm. The timber beam was struck at alternative ends with a 7 lb sledgehammer to generate opposite

polarity shear wave signals. Data files were stacked between two and six times to improve the signal to noise ratio.

The shear wave arrival times were measured on the horizontal geophones on channels 1, 2 and 3. Interval velocities were calculated using the travel time difference between the upper and lower horizontal sensors (2 m separation). Compressional wave arrivals were recorded on the vertical geophone (channel 4). Triggering was captured on channel 5 to identify, if present, false triggering events.

All the data was recorded using a Geometrics Geode Seismograph, with acquisition parameters for the DHVs survey set with a 0.125 ms sample interval, 1 s record length, 36 dB pre-amp gain, and an electrical trigger system. Processing of field records and interval velocity calculations were completed using the REFLEXW © seismic processing package and Microsoft Excel © spreadsheets.

The field data was recorded in SEG-2 format. At each depth, a stacked file was collected for each polarity of the shear wave source. All field files were first converted to ReflexW standard format. For the orthogonal geophones, two separate and opposite polarity seismograms were produced and overlaid to improve the accuracy of the shear wave arrival picks. Shear wave arrival times were based on the first consistent V_S wavelet intersection that could be picked across the seismogram.

Compressional wave velocity data was also acquired down the borehole at 1 m intervals using the vertical geophone (channel 4) in accordance with standard borehole seismic survey methodologies, but these results have not been included in this report and can be supplied if required.

3.2 MASW survey design

MASW is a seismic method that is used to evaluate ground stiffness by measuring the shear wave velocities (Vs) of the subsurface through the analysis of the dispersion properties of Rayleigh surface waves. Data is collected by placing an array of sensors on the ground and recording the surface waves generated by seismic sources (active or passive). The propagation velocities of the surface waves are then analysed to model the shear wave velocity distribution in the subsurface.

The MASW method exploits the dispersive nature of the ground roll. The frequency components of the surface Rayleigh wave will have a different propagation velocities (phase velocity). By plotting the phase velocity as a function of frequency we can generate a dispersion curve at each shot location (Xia et al., 1999[4]). A 1D profile of the shear wave velocity versus depth can then be calculated from the dispersion curve. Multiple 1D profiles

can be combined, to produce a 2D cross-section of the shear wave velocities along the MASW line (Figure 4).

3.2.1 MASW Acquisition Parameters

The MASW lines in this survey were collected using:

- 48-channel towed seismic array (4.5 Hz geophones on plates).
- Geophone spacing of 0.5 m.
- Shot spacing of 4 m.
- Shot offsets of 8 m.
- Sample rate of 0.125 ms.
- Record length of 1.25 s.
- Preamp gains High.
- Stacked 3 - 4 times.
- Source was a 7 lb sledgehammer impacting an aluminium plate.
- An electrical trigger was used.

3.2.2 MASW Processing

The field records were processed using the Kansas Geological Survey software package SurfSeis6.5++ ©. The geometry for each point was set according to the survey parameters, and the dispersion curves were generated and edited. The inversions were run using a 10-layer variable depth model. The velocity data was interpolated into 2D profiles showing Vs variations with depth (Figure 4). The output shear wave velocity data is included as data files (CSV format) supplementary to this report. Survey positions were recorded using an EMLID Reach RS3+ system capable of real time kinematic corrections using the NZGD2000 datum. Results have been output in New Zealand Transverse Mercator 2000 (NZTM2000), with heights in Mean Sea Level (MSL). Accuracy of corrected GNSS +/-0.3 m.

4 Limitations

As with all testing methods, there are limitations with downhole seismic and MASW testing that should be considered when evaluating the results.

4.1 DHVs Limitations

- The reference arrival times used are for the time from the source impact to the arrival at the receivers. The source is offset from the bore hole by ~1 m. Therefore, near the surface the wave path is assumed to be a straight line or slant distance from the source to receiver. This assumption is not always correct, and the wave travel path could be significantly more complex due to near surface heterogeneity, refractions or near surface effects. The

borehole tube grouting is also likely to be poorer at the surface than deeper down due to the lower confining pressures and heterogeneity of the near surface (reworking and younger age of sediments etc). For these reasons the velocities in the depth range 0 to 3 m should be treated with caution.

- High velocity layers are difficult to accurately measure for velocity/thickness as the travel time across them may be very fast. Downhole seismic testing defines slow velocities and thick units more accurately.

True interval velocity plots will show large velocity variation when using small depth intervals. Increasing the interval will decrease the "noise" in the interval velocity plots but reduce the ability to "see" rapid changes in shear wave velocity. Often a balance between resolution and accuracy is required. In many situations a more useful output from downhole seismic test results is a basic linear best fit model of the main lithological units. An arrival time vs depth graph is usually broken into sections where obvious changes in slope of the time vs depth graph is seen or where supplementary data from borehole logs or CPT tip resistance show likely important seismic shear wave units.

4.2 MASW Limitations

The MASW method of modelling shear wave velocity typically produces results that are comparable with directly measuring shear waves in most scenarios (Wotherspoon et al., 2021[5]). However, there are some subsurface geological conditions that result in difficulty inverting Rayleigh wave velocity to a shear wave velocity model. Such conditions include fluid-solid interfaces, anisotropic media, sharp lateral discontinuities, and density inversions (Berryman, 2007[6]). In these scenarios, the compressional wave velocity component of the Rayleigh wave may be higher than expected, the shear wave velocity may be underestimated, or the layer thickness may be underestimated. Other geological conditions that result in uncertainties are where waves travelling through a media have a much longer wavelength than the length of the array. This primarily occurs when crystalline bedrock material is close to the surface.

The capabilities of a MASW system to confidently model shear wave velocities with depth is dependent on the frequency of the geophones used, the spacing between the geophones, the distance of the shot offset, and the frequency and velocity of the surface waves at any given point. Designing the MASW system for a survey is a balancing act between achieving good resolution in the near surface, while still achieving the required target depths. The limitations of the MASW method should be considered when evaluating these results.

5 Results and Interpretations

Shear wave velocities were measured at 1 m intervals over the length of borehole EGL06B (30 m).

Two MASW lines (total 180 m in length) were undertaken adjacent to the borehole location (Figure 3). The MASW lines utilised a 24 m long geophone array, allowing confident modelling of near-surface shear wave velocities to approximately 12 m depth (approximately half the array length). Both MASW lines produced clear dispersion curves at the higher frequencies required for near-surface imaging (Figure 4 and Appendix B). The MASW profiles exhibited increasing shear wave velocities with depth, with relatively few processing artefacts. The interpreted shear wave velocities ranged from approximately 190 m/s to around 1000 m/s. The interpreted Schist contact is visible within the MASW profiles and shows good correlation with the downhole seismic results.

The results from borehole EGL06B are summarised in Figure 5 which includes three graphs:

Graph A: The true interval velocity profiles were derived by measuring the interval travel time between the receiver depths (1 m separation between adjacent sensors), with interval velocities calculated over the 2 m separation between channels 1 and 3. The figure includes the interval velocity profile, the average interval velocity from channels 1, 2 and 3. An example seismogram with interval picks for channels 1, 2 and 3 is provided in Appendix D for EGL06.

Graph B: The corrected shear wave arrival times measured for channel 3 (lower horizontal geophone within the downhole probe). This represents a reference point on the wave train that could be confidently traced down the entire seismograms. An example seismogram with first positive peak arrival “picks” is provided in Appendix D channels 2.

Graph C: The shear wave velocity profile derived using the slope method to define linear trends and clear changes in slope within the data. The shear wave velocities were calculated by fitting a series of best fit lines to the corrected shear wave arrival times where clear breaks in slope were identified.

A clear increase in shear wave velocities is observed below approximately 11 m depth, indicating a transition into more competent material. This Vs increase aligns well with the MASW profiles, which show a corresponding increase in shear wave velocities indicative of the onset of the interpreted bedrock / Schist layer (>600 m/s).

6 Conclusions

The DHVs data was of acceptable quality, with generally consistent trends observed between the orthogonal geophones (1 m spacing between sensors and a 2 m separation between channels 1 and 3 used for interval velocity calculations). Some traces required additional stacking and careful review during the arrival picking process, which can occur in downhole seismic testing where variations in casing grout conditions influence signal transmission within the borehole. Overall, the dataset allowed reliable identification of the shear wave velocities with depth.

The slope method model provides a more consistent velocity profile and is considered a better representation of the shear wave velocity structure with respect to the main lithological units (Graph C, Figure 5).

The MASW data produced high quality dispersion curves which allowed reliable modelling of the near-surface shear wave velocities to approximately 12 m depth (Figure 4). The MASW results correlate well with the DHVs data and available borehole information, and together the datasets indicate the depth to the interpreted bedrock / Schist horizon.

7 Closure

We hope this report addresses your current requirements and should you want to discuss the report further I can be contacted on [redacted]



Sincerely,

Jack Fleming (BSc), Geophysicist

8 References

[1]ASTM D7400 / D7400M-19, Standard Test Methods for Downhole Seismic Testing, ASTM International, West Conshohocken, PA, 2019, www.astm.org.

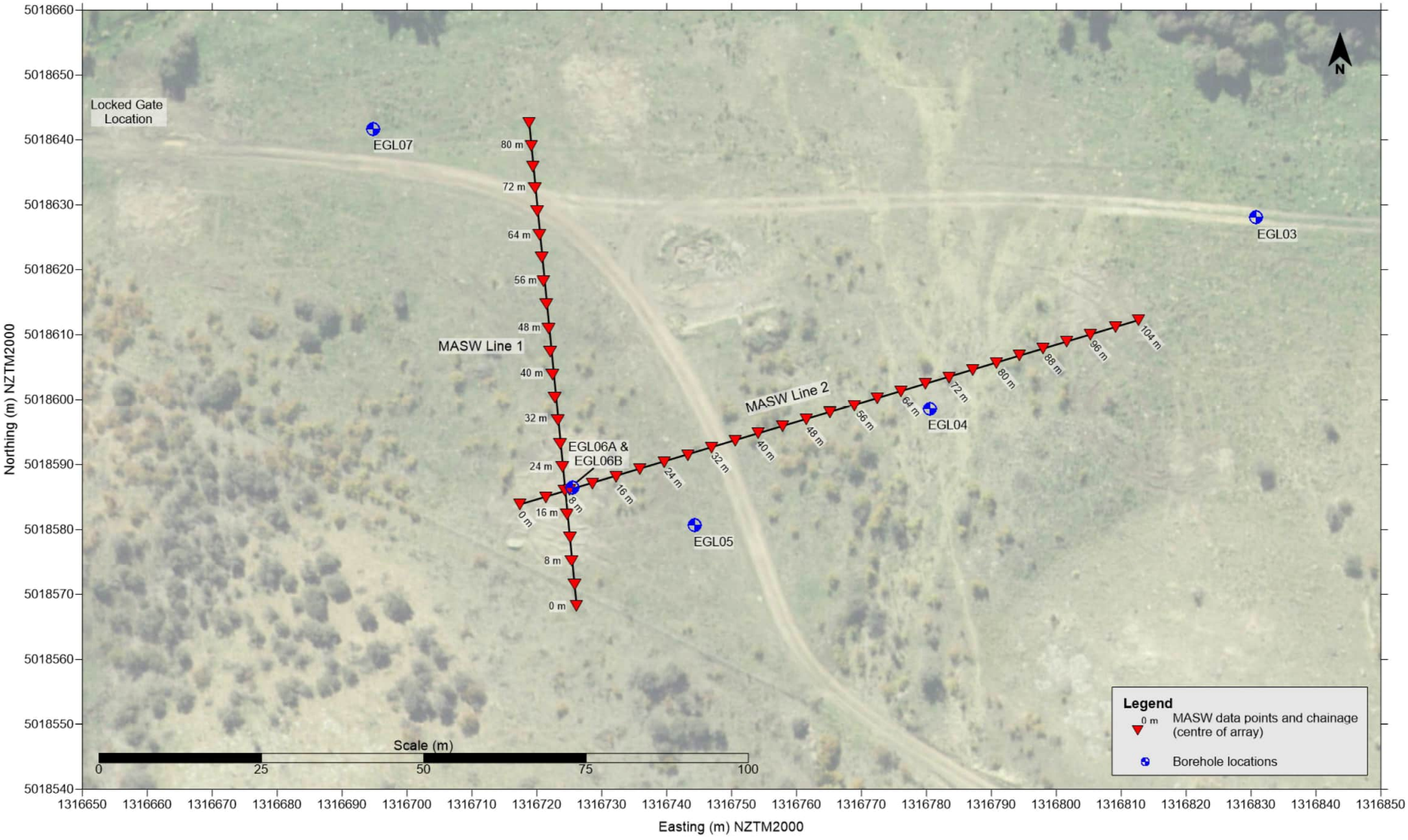
[2]QuakeCentre Invasive Seismic Testing – A Summary of Methods and Good Practice, F. Wentz 2019.

[3]*Stolte, A., Wotherspoon, L., & Wentz, R.* (2023). Providing robust Vs30 estimates for seismic site classification in New Zealand. New Zealand Geotechnical Society, 105, 0111 - 6851.

[4]*Xia, J., Miller, R. D., & Park, C. B.* (1999). Estimation of near surface shear-wave velocity by inversion of Rayleigh waves. Geophysics, 64(3), 691-700.

[5]*Wotherspoon, L. M., Wentz, R., Cox, B. R., & Stolte, A. C.* (2021). Assessing the quality and uncertainty of in-situ seismic investigation methods. In 2021 New Zealand Geotechnical Society Symposium (pp. 24-26).

[6]*Berryman, J. G.* (2007). Seismic waves in rocks with fluids and fractures. Geophysical Journal International, 171(2), 954-974.



REV. HISTORY			
DRAWN BY	MH	DATE	03/03/2026
CHECKED BY	JF	DATE	13/03/2026

Notes:

All MASW data points are displayed but not all chainage values shown for clairity.

All GPS locations were collected and then differentially corrected, in post processing.

Borehole locations as per provided MGL survey.

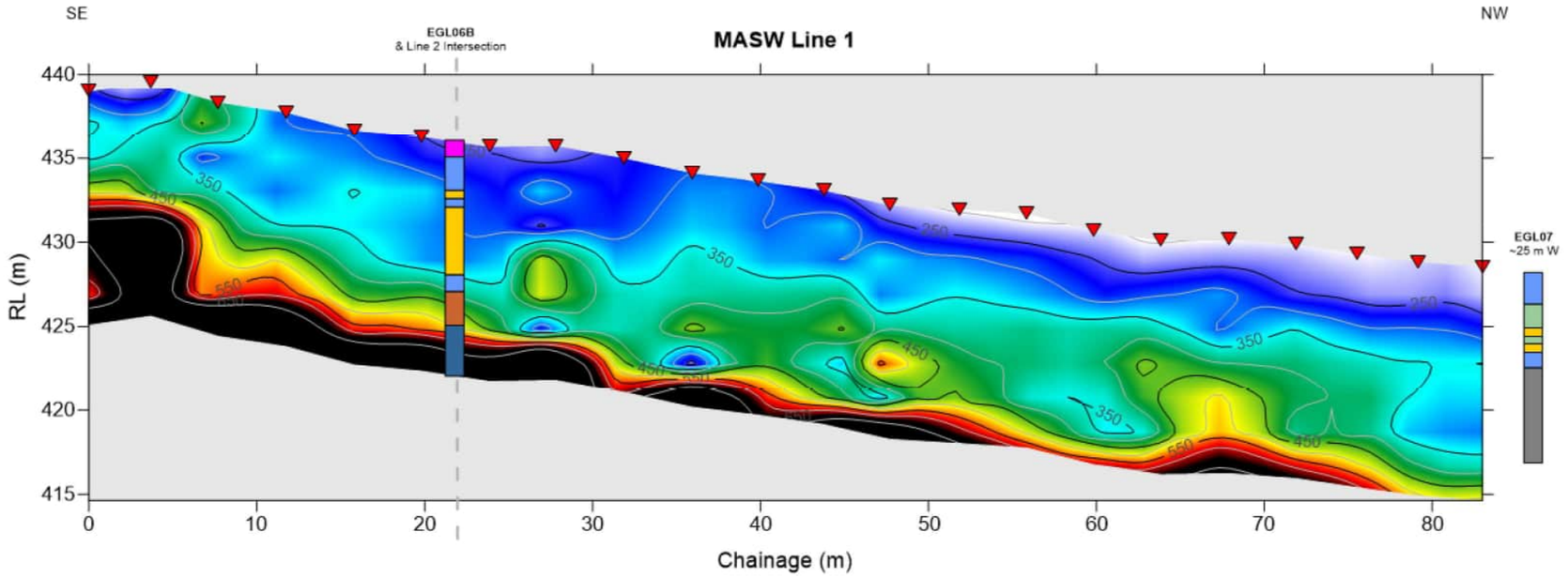
Site Survey Map
Downhole Shear Wave & MASW Surveys
Bendigo-Ophir

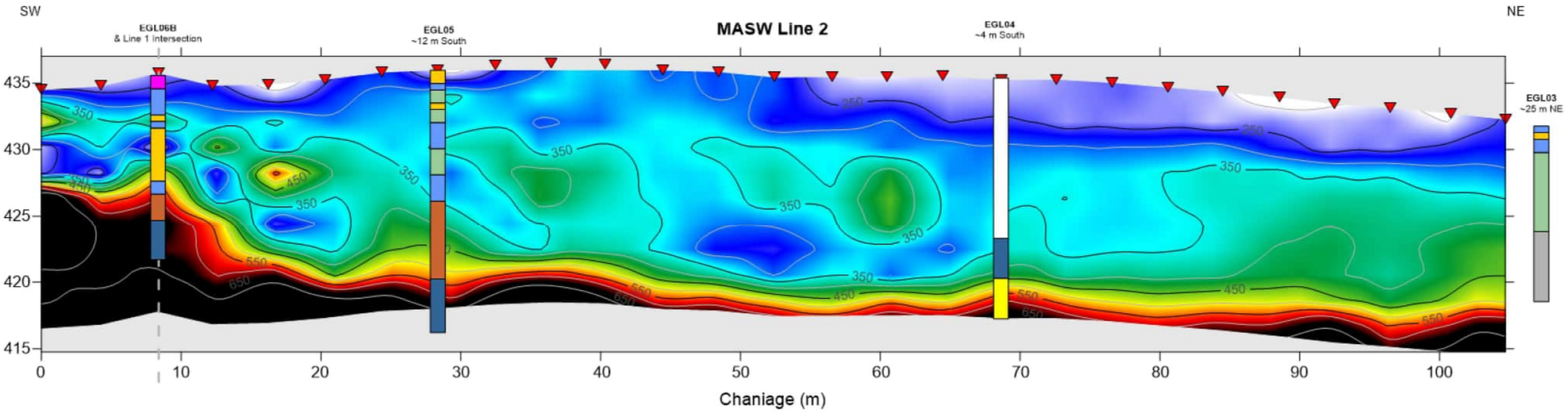
FIGURE 3

A4

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Vs (m/s)

200 250 300 350 400 450 500 550 600 650

Legend

MASW data collection point (centre of array)

Unit	Materials		Unit	Materials	
Fill/Slucing	Clay/Silt/Sand		Schist	Clay (Faulted)	
Alluvium	Caly/ Silt Sand Gravel			Gravel / Crush Schist	
Colluvium	Gravel			No Recovery	
				TBC	
				Unknown	

REV. HISTORY			
DRAWN BY	MH	DATE	04/03/2026
CHECKED BY	JF	DATE	13/03/2026

Notes:

MASW V_S profile has contour intervals of 50 m/s.

MASW profile scale is 1:1.

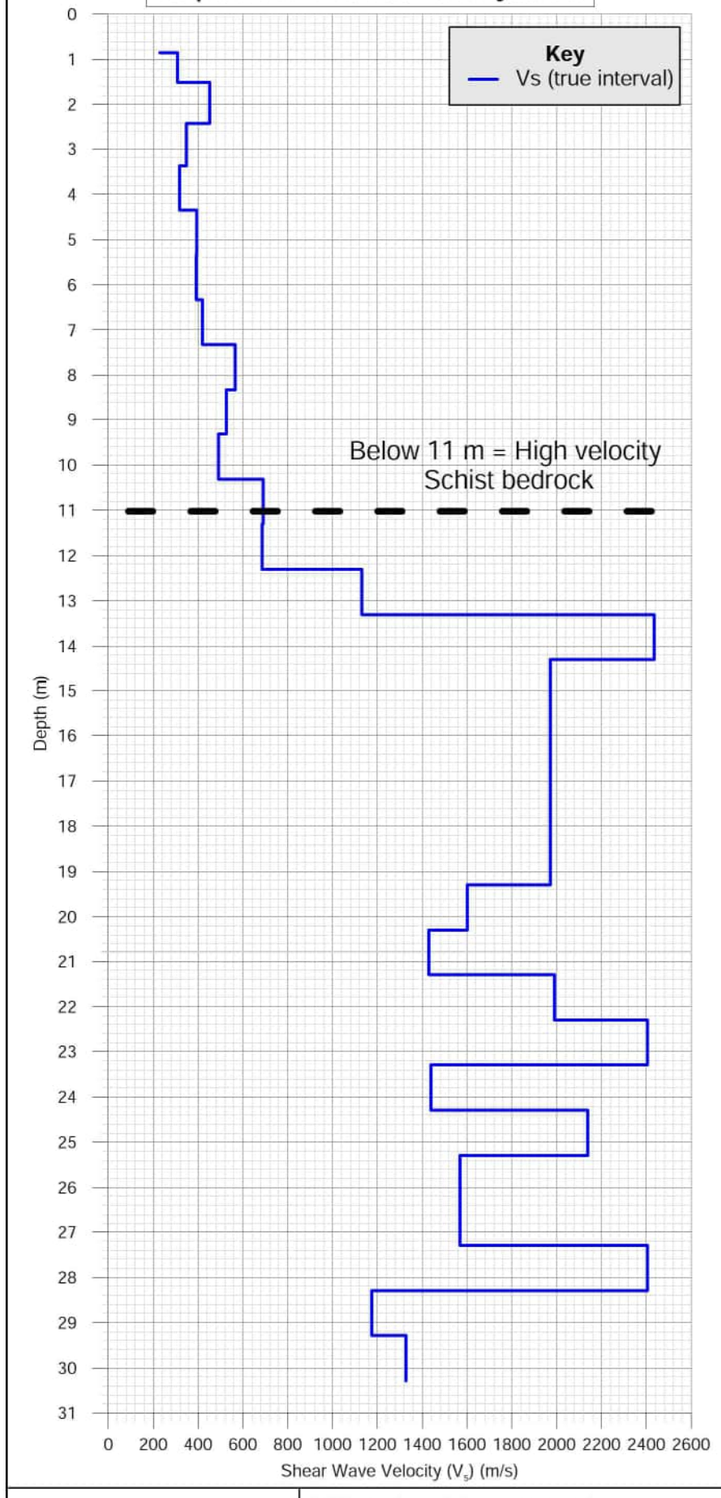
See site map for location of points and boreholes.

MASW Lines 1 & 2 - RL
Topographically Corrected
Downhole Shear Wave & MASW Surveys
Bendigo-Ophir

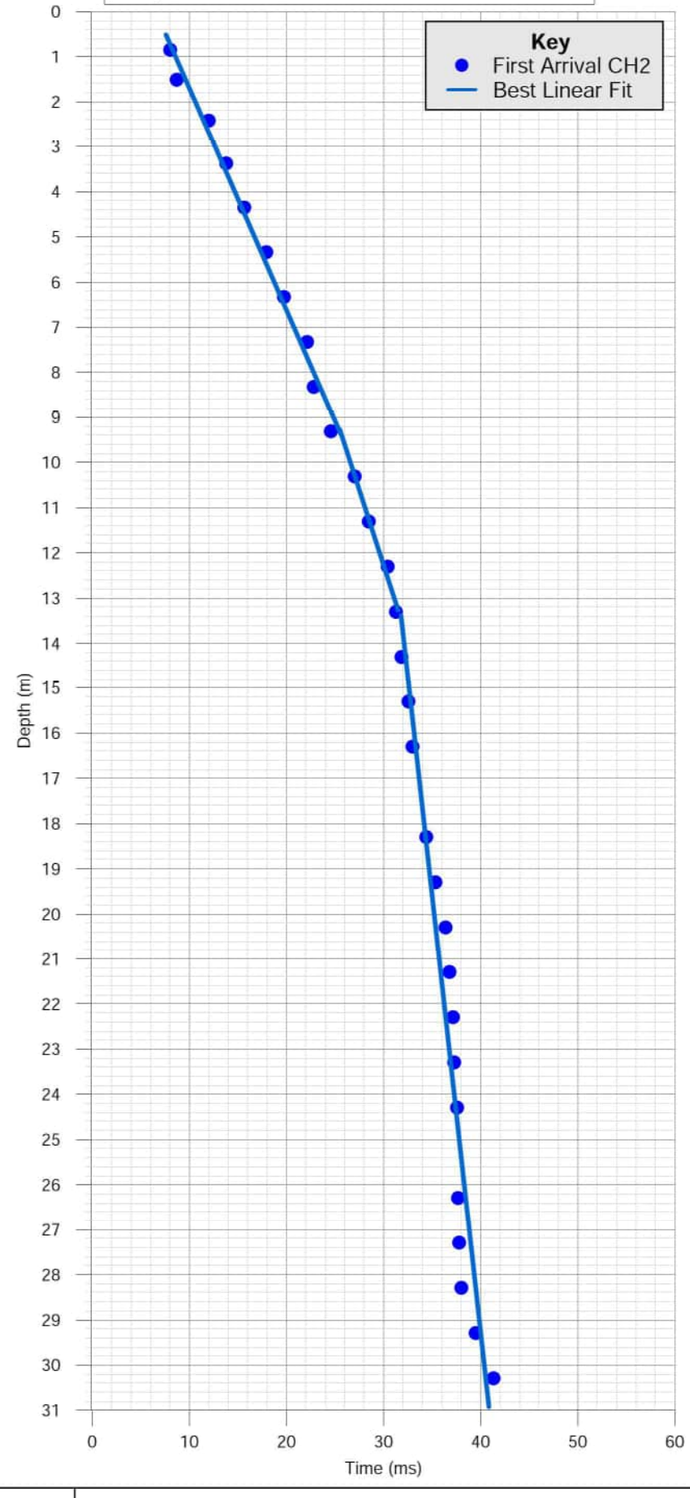
FIGURE
4
A4

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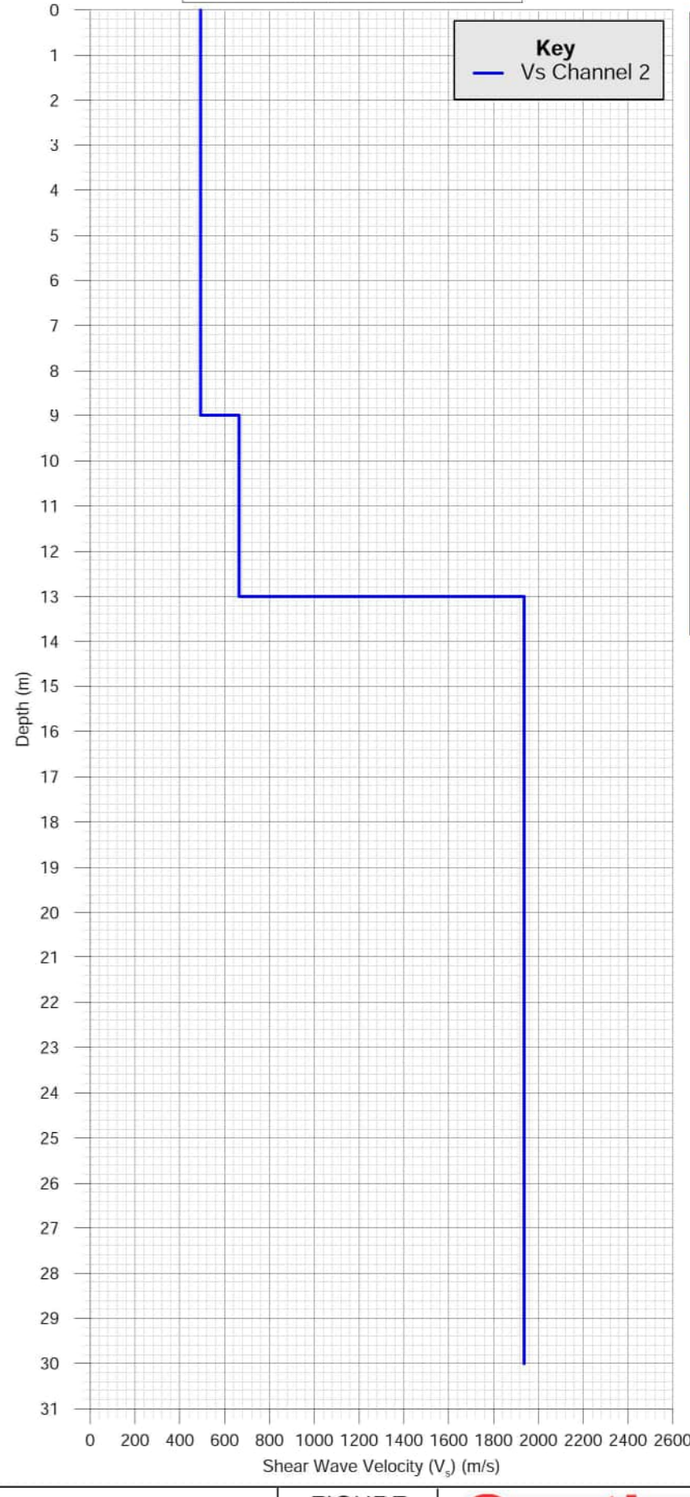
Graph A: True Interval Vs Velocity Profile



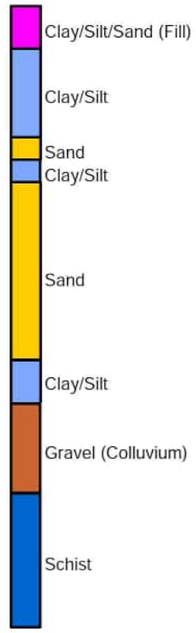
Graph B Corrected Shear Wave Arrival Times



Graph C: Simplified Vs Profile Indicating Major Velocity Units



Simplified Borehole Log



REV. HISTORY			
DRAWN BY	NH	DATE	06/03/2026
CHECKED BY	MF	DATE	13/03/2026

NOTES: See site map for location of the borehole.

Downhole Shear Wave Vs Profiles
BH EGL06B
Bendigo-Ophir

FIGURE 5

A3

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1. The client is advised that non-invasive geophysical testing has limitations and is not a complete source of testing. Often there is a need to couple non-invasive testing methods with invasive testing methods, such as drilling, especially in cases where the non-invasive testing results indicate anomalies.

2. This document has been prepared for the particular purpose outlined in the project proposal and Southern Geophysical Limited accepts no responsibility whatsoever for the use of this document and information contained therein, in whole or in part, in other contexts or for any other purpose.

3. This document and all information contained therein including graphics is provided for sole use by the client and is confidential to that client and its professional advisers. No responsibility whatsoever for the contents of this document will be accepted to any person other than the client. Any use which a third party makes of this document, or any reliance on or decisions to be made based on it, is the responsibility of such third parties. Southern Geophysical Limited accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this document.

4. Southern Geophysical Limited did not perform a complete assessment of all possible conditions or circumstances that may exist at the site. Conditions may exist which were undetectable given the limited nature of the enquiry Southern Geophysical Limited was retained to undertake with respect to the site. Variations in conditions often occur between investigatory locations, and there may be special conditions pertaining to the site which have not been revealed by the investigation and which, therefore, have not been considered. The client is advised that additional studies and actions may be required.

5. Southern Geophysical Limited collected the data and based the report on data and information which was collected at a specific point in time. The passage of time affects the information and assessment provided by Southern Geophysical Limited. The services provided allowed Southern Geophysical Limited to form no more than an opinion of the actual conditions of the site at the time the site was visited and investigated and cannot be used to assess the effect of any subsequent changes for whatever reason.

6. Where data is supplied by the client or other sources, including where previous site investigation data have been used, it has been assumed that the information is correct. No responsibility is accepted by Southern Geophysical Limited for incomplete, inaccurate or out-dated data supplied by others.

7. Best practice is applied to the collection and interpretation of data by Southern Geophysical Limited. No warranty is included, either express or implied, that the actual conditions will conform exactly to the assessments contained in this document.

Appendix A: Site Photographs



Figure A1: MASW data acquisition



Figure A2: MASW data acquisition

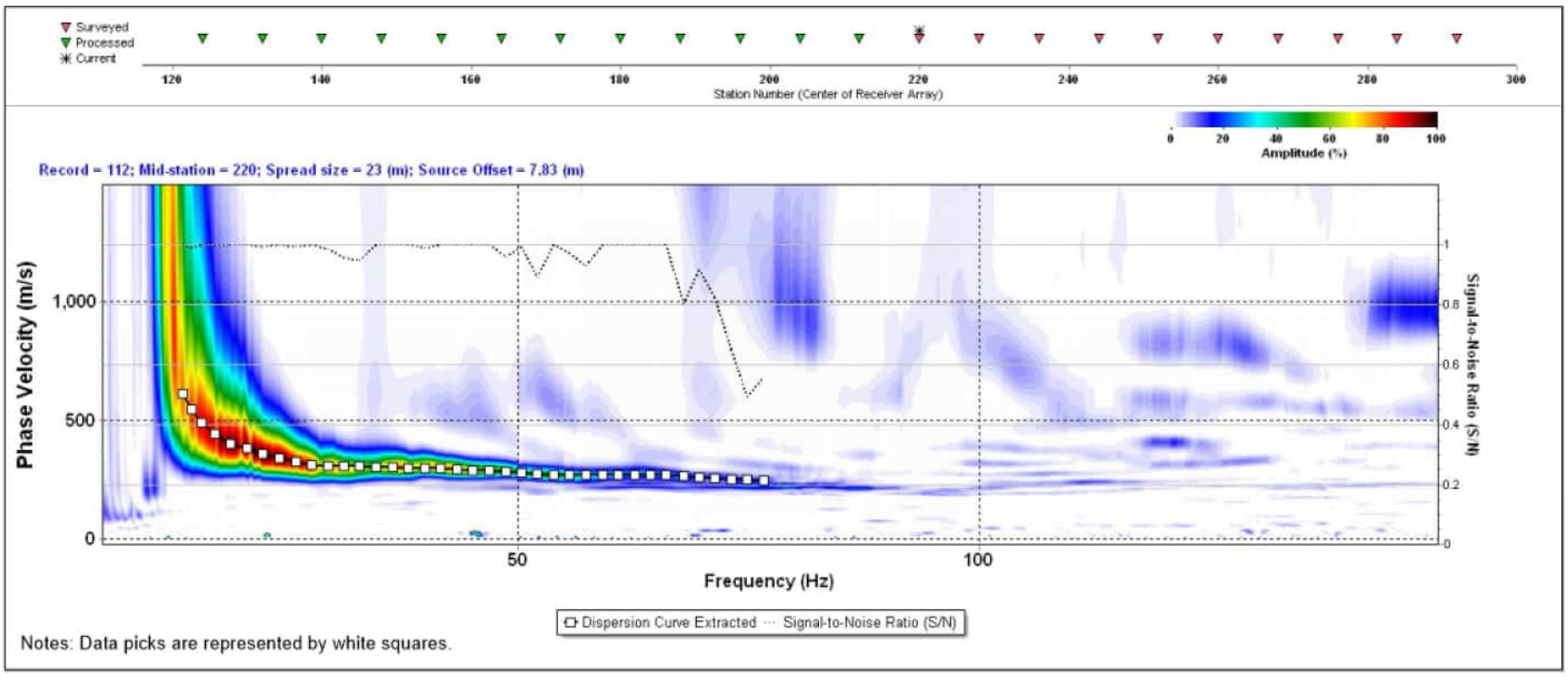


Figure A3: DHVs data acquisition



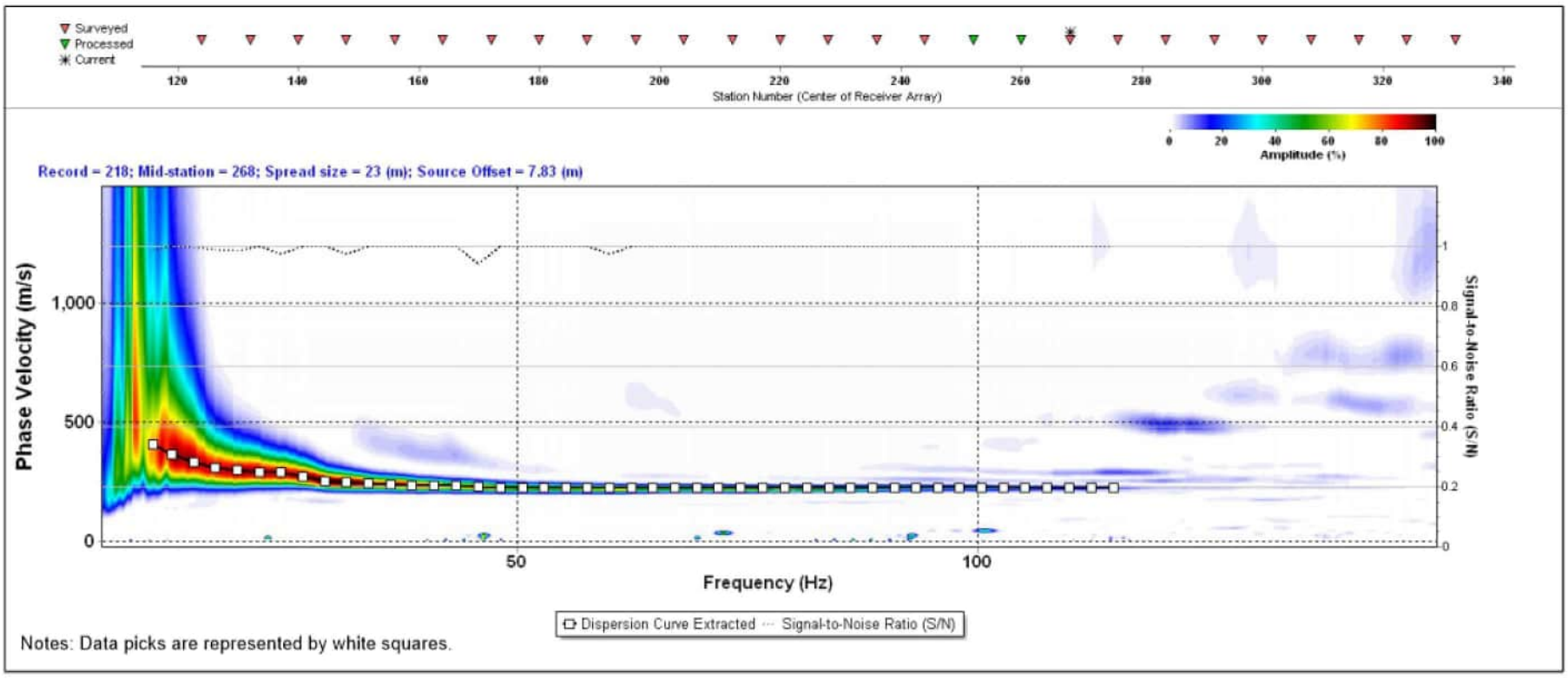
Figure A4: Borehole after data acquisition

Example One - Line 1 Dispersion Curve at 48 m



Notes: Data picks are represented by white squares.

Example Two - Line 2 Dispersion Curve at 72 m



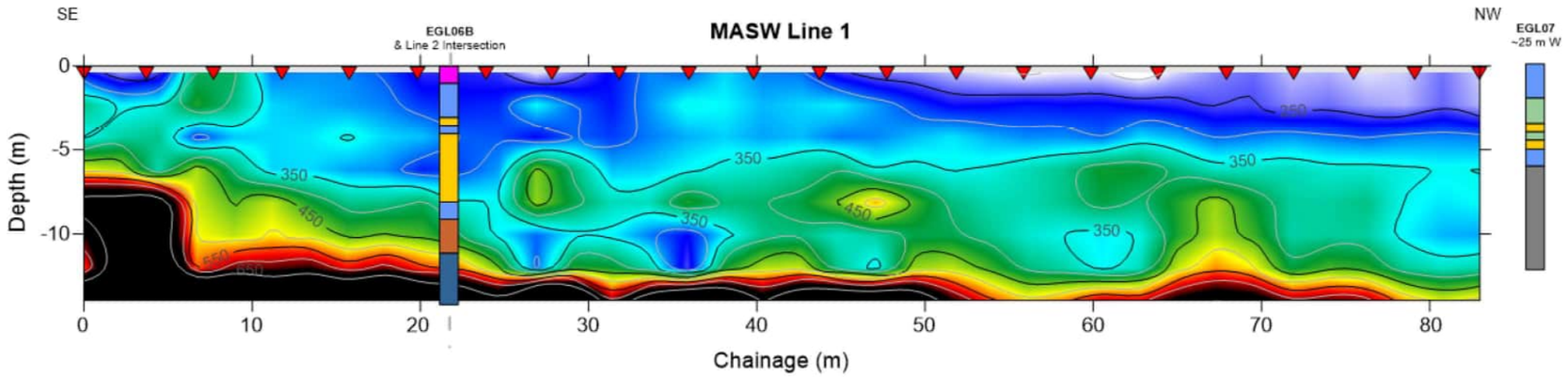
Notes: Data picks are represented by white squares.

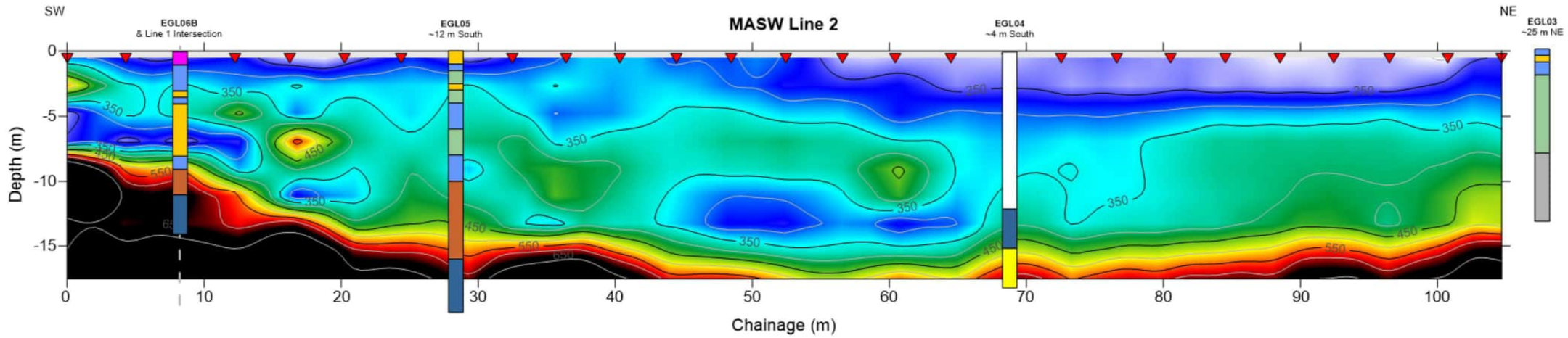
REV. HISTORY			
DRAWN BY	MH	DATE	09/03/2026
CHECKED BY	JF	DATE	09/03/2026

Example MASW Dispersion Curves
Downhole Shear Wave & MASW Surveys
Bendigo-Ophir

APPENDIX
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Vs (m/s)

200 250 300 350 400 450 500 550 600 650

Legend

MASW data collection point (centre of array)

Unit	Materials		Unit	Materials	
Fill/Slucing	Clay/Silt/Sand		Schist	Clay (Faulted) Gravel / Crush Schist	
Alluvium	Caly/ Silt Sand Gravel			No Recovery TBC Unknown	
Colluvium	Gravel				

REV. HISTORY			
DRAWN BY	MH	DATE	04/03/2026
CHECKED BY	JF	DATE	13/03/2026

Notes:

MASW V_S profile has contour intervals of 50 m/s.

MASW profile scale is 1:1.

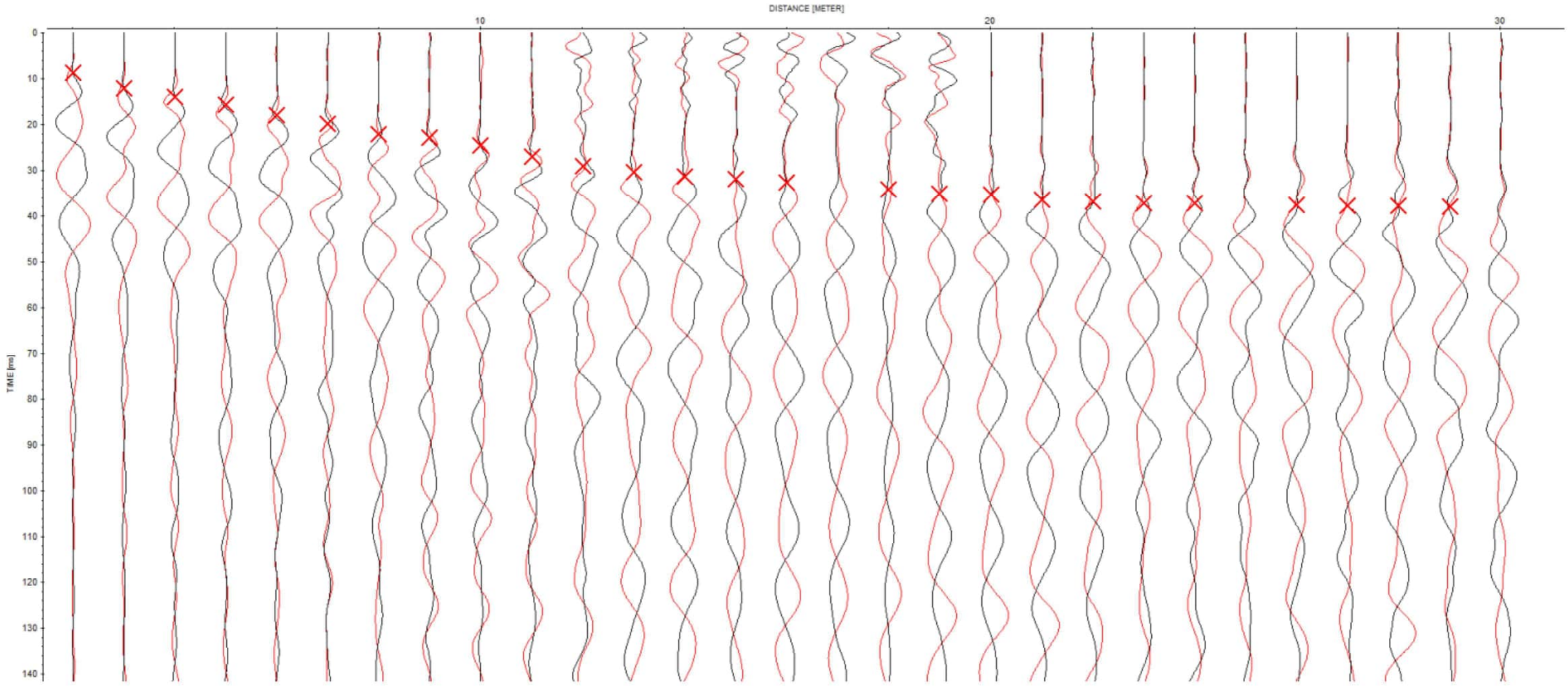
See site map for location of points and boreholes.

MASW Lines 1 & 2 - Depth
From Ground Surface
Downhole Shear Wave & MASW Surveys
Bendigo-Ophir

APPENDIX
C
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BHEGL06B - Channel 2 Middle Probe
Left and Right Overlaid



Notes: Data picks are represented by red crosses.
Low Pass filtering has been applied to the data.

REV. HISTORY			
DRAWN BY	NH	DATE	13/03/2026
CHECKED BY	MF	DATE	13/03/2026

Example Seismogram
Channel 2 Orthogonal Probe - First Positive Peak Arrival
Bendigo - Ophir

APPENDIX
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